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Effect of Electromigration on Interfacial Reactions between Electroless Ni-P and Sn-3.5%Ag Solder

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Abstract

Effect of electromigration on interfacial reactions between electroless Ni-P (EL-Ni) and eutectic Sn-3.5% Ag solder has been investigated. Sandwich-type reaction couples, Cu/EL-Ni/Sn-3.5% Ag/EL-Ni/Cu, having two EL-Ni/Sn-3.5% Ag interfaces were prepared with the help of reflow process. During reflow, Ni₃Sn₄ intermetallic formed at the EL-Ni/Sn-3.5% Ag interfaces with a dark thin Ni₃P layer underneath it. The reaction couples were annealed at 160°C and 180°C for various durations with and without the passage of DC current of 1 × 10³ A/cm² density. It was found that current does not affect the stoichiometry of the intermetallics formed at the EL-Ni/Sn-3.5% Ag interfaces. The same Ni₃Sn₄ intermetallic formed in the samples annealed at both the temperatures with and without current. Formation of Kirkendall voids in the Ni₃P layer showed that Ni diffused from EL-Ni through the grain boundaries of Ni₃P to form Ni₃Sn₄. It was observed that current retards the Ni₃Sn₄ growth at both the anode and cathode side interfaces at 180°C, while no significant retardation was observed at 160°C. This effect of electromigration on the EL-Ni/Sn-3.5% Ag interfacial reactions was due to the presence of Ni₃P layer in between EL-Ni and Ni₃Sn₄.

Keywords: Electromigration, Interfacial reactions, Electroless Ni-P, Solder

1. Introduction

Electromigration, which is a transport phenomenon caused by the passage of electric current through a conductor, results in change of atomic distribution in the conductor. Driving force for this migration is the momentum exchange force, which arises from collision of charge carrier with the conductor atoms [1, 2]. In heterogeneous materials system, atomic transport phenomenon also occurs due to the concentration gradient wherein atoms diffuse and form intermetallic compounds (IMC) to obtain the equilibrium situation. The electromigration flux caused by the passage of electric current in the heterogeneous materials system, influences the atomic flux that occurs due to the concentration gradient [4-9]. This electromigration flux is given by the following equation:

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$$j_{em} = \frac{CDZ^*e\rho j}{kT} \tag{1}$$

where C is the concentration of moving atoms, D is the diffusivity, k is Boltzmann's constant, T is the absolute temperature, e is the electron charge, Z^* is the effective charge number, ρ is resistivity and j is current density.

Both the mass transport phenomena, electromigration and migration due to the concentration gradient, are very common in interconnects of electronic devices, which carry high current density and have interfaces between different materials such as solder/under bump metallization (UBM) interface. During soldering, initial formation of IMC at the solder/UBM interface ensures a good metallurgical bond. However, growth of these IMC affects the mechanical reliability of the interface [3]. Most of the interfacial studies between solder and UBM are based on annealing effect. However, a few investigations have shown that electromigration influences the interfacial reactions in most of the metallic systems [4-9]. Thus, it is significant to investigate the electromigration effect on the interfacial reactions between solder and UBM.

In recent years, electroless Ni-P (EL-Ni) is considered as a promising UBM due to its many advantages such as excellent solderability, good corrosion resistivity, selective deposition, strong adhesion, ease of processing, and low cost process as compared to thin-film vacuum processes [10-12]. The interfacial reactions, between EL-Ni and solder alloys, have been studied by number of researchers [11-16]. However, no literature has been found on the effect of electromigration on the EL-Ni/Sn-3.5% Ag interfacial reactions. The present study involves the investigation of electromigration effect on the phase formation and growth of IMC in the EL-Ni/Sn-3.5% Ag system at different temperatures.

2. Experimental Procedure

In order to investigate the electromigration effect upon EL-Ni/Sn-3.5%Ag interfacial reactions, Cu/EL-Ni/Sn-3.5%Ag/EL-Ni/Cu reaction couples having two EL-Ni/Sn-3.5%Ag interfaces were prepared as follows. First, a piece of commercial copper plate of the size 7 mm × 2.5 mm and 3.0 mm in thickness was ultrasonically cleaned in acetone for 20 min to remove the organic impurities. The plate was then etched with 30 vol% HNO₃ solution for 2 min at room temperature to remove inorganic impurities and surface oxide. Surface cleaned

Cu plate was coated by EL-Ni in two steps. In the first step, Cu surface was activated using the ruthenium-based commercial pre-initiator. Then, EL-Ni was coated on the activated Cu surface using commercial electroless nickel solution. Thin layer (~200 Å) of non-cyanide immersion gold was also deposited on EL-Ni surface to protect the surface from oxidation.

EL-Ni coated Cu plate was cut into two pieces of size 4.5 mm \times 2.5 mm and 2.5 mm \times 2.5 mm. They were then joined with each other using Sn-3.5% Ag solder with the help of reflow process. The reflow was carried out at 245 °C for 60 sec. Figure 1 shows the schematic diagram of setup by which solder joint was formed in between the two EL-Ni coated Cu plates. The joint was formed during the reflow process by placing a number of small pieces of Sn-3.5% Ag solder wires on the small EL-Ni coated Cu plate and pressing them by the big plate. Glass spacers of thickness 450 μ m were used to maintain the uniform thickness of Sn-3.5% Ag solder in between the EL-Ni coated Cu plates. The joined plates were cut into 450 μ m \times 650 μ m \times 6 mm reaction couples with the help of diamond saw. Figure 2 shows the schematic diagram of as-prepared EL-Ni/Sn-3.5% Ag reaction couple.

Experimental setup used to pass the electric current through the couple is shown in Figure 3. As-prepared couple was connected to current source with the help of a specially designed sample holder, which had a ceramic base and two Cu electrodes to hold Cu part of the reaction couple. Upper surface of Cu electrodes was coated with high temperature polymer film to disconnect them electrically from the sample holder body. These Cu electrodes were directly connected to a current source and a thermocouple was kept at the centre of reaction couple using the high temperature thermo-tape to monitor the reaction temperature.

As-prepared reaction couples were annealed at $160~^{\circ}\text{C}$ and 180°C for various durations from 48 h to 400 h. DC current of about $1\times10^3~\text{A/cm}^2$ density was also passed through the couple connected to the power source. After annealing with and without the passage of current, the couples were removed from the oven and cooled in air. Scanning electron microscopy (SEM) was used to observe the morphology and to measure the thickness of IMC layer. The thickness was calculated by dividing the IMC's area at the interface with associated interface length. For SEM observation, the couples were cold mounted in epoxy and polished down to 1 μ m finish. After polishing, etching was carried out

using 4 vol% hydrochloric acid to reveal the microstructure at the interface. Energy dispersive X-ray (EDX) was performed in the SEM to analyse the chemical composition of EL-Ni and IMC.

3. Results and Discussion

3.1 As-prepared Reaction Couple

Figure 4(a) shows the cross-sectional view of as-prepared reaction couple. The measured thickness of the solder layer was around 425 µm. Figure 4(b) is the micrograph of EL-Ni/Sn-3.5% Ag interface in as-prepared couple. It shows that IMC with needle and chunky-type morphologies formed at the EL-Ni/Sn-3.5% Ag interface during the reflow. A dark thin layer also formed in EL-Ni layer underneath the IMC. Some voids were observed at the Cu/EL-Ni interface, which formed due to the etching during the surface preparation of the Cu plate. The thickness of EL-Ni and IMC layers was measured to be around 6.5 µm and 2.5 μm, respectively. EDX analysis showed that the Au layer completely dissolved in the solder during the reflow, as apparent with the absence of Au or Au-Sn IMC at the interface. Figures 5 (a), (b) and (c) show the EDX analysis of IMC, EL-Ni layer, and dark thin layer underneath the IMC, respectively. Quantitative EDX analysis showed that IMC had 43.39 at. % Ni and 56.61 at. % Sn, EL-Ni layer had 9.23 at. % P and 90.77 at. % Ni and dark thin layer had 20.85 at. % P and 79.15 at. % Ni. The compositions of the IMC and dark thin layer are close to Ni₃Sn₄ and Ni₃P, respectively. Thus, during the reflow needle and chunky-type Ni₃Sn₄ formed at the EL-Ni/Sn-3.5% Ag interface with a P rich Ni₃P layer underneath the Ni₃Sn₄. These results are in agreement with the previous interfacial studies between EL-Ni and Sn-3.5% Ag solder. [11-13]

3.2 Growth Mechanisms of IMC and Ni₃P Layers

Electromigration influences the interfacial reaction in most of the metallic system in terms of phase formation and growth [4-9]. Therefore, the growth mechanisms of IMC and Ni₃P layers in the EL-Ni/Sn-3.5% Ag system have to be understood first. The interfacial reaction between EL-Ni and Sn-3.5% Ag is highly complicated due to the presence of P in EL-Ni. According to the binary phase diagram, the thermodynamic equilibrium phases near the compositions of EL-Ni are Ni₃P and Ni [17], which form in the case of self-crystallization of amorphous EL-Ni at temperatures only above 250°C [18,19]. However, in soldering reaction-assisted crystallization, Ni₃P forms well below 250°C, along with the formation of

Ni₃Sn₄ as a result of reaction between Ni and Sn [11]. The interfacial reaction between EL-Ni and solder alloy during reflow could be written as

$$Ni_{x}P_{y} + \frac{4(x-3y)}{3}Sn \rightarrow yNi_{3}P + \frac{(x-3y)}{3}Ni_{3}Sn_{4}$$
 (2)

Further growth of Ni₃Sn₄ during annealing requires Ni that comes from the EL-Ni layer thereby increasing the Ni₃P layer thickness. Jang et al. [11] proposed that during Ni₃Sn₄ growth either Ni diffuses out of EL-Ni to Ni₃P/Ni₃Sn₄ through the grain boundaries of Ni₃P or Ni₃P decomposes into P and Ni at the Ni₃P/Ni₃Sn₄ interface and the P diffuses interstitially back to grow Ni₃P at the Ni₃P/EL-Ni interface. However, they supported the later mechanism as grain boundary diffusion of Ni must be accompanied by back diffusion of vacancies and they did not find any Kirkendall voids in the Ni₃P layer.

In this investigation, it was observed that Ni₃P layer has small Kirkendall voids, whose size and number increase with the duration of annealing. Figures 4 (c) and (d), respectively are the micrographs of EL-Ni/Sn-3.5% Ag interface in the couples annealed for 400 hr at 160°C and 180°C without current, showing the formation of large number of voids in the Ni₃P layer. Thus, during solid-state annealing Ni diffuses from EL-Ni to Ni₃P/Ni₃Sn₄ interface through the grain boundaries of Ni₃P layer. This Ni diffusion from EL-Ni layer, results in a counter diffusion of vacancies, which accumulate and form voids in the Ni₃P layer. The depletion of Ni from EL-Ni/Ni₃P interface assists the EL-Ni to crystallize into Ni₃P and increases the Ni₃P layer thickness. The reason behind the invisibility of the voids in the Ni₃P layer in the work of Jang et al. [11] could be the insufficient accumulation time for the vacancies during the brief annealing duration of up to 40 min.

3.3 Effect of Electromigration on the Interfacial Reactions

It was observed that electromigration does not affect the phase formation in EL-Ni/Sn-3.5%Ag system. Ni₃Sn₄ was the only phase formed in all the reaction couples annealed at 160°C and 180°C for various durations, with and without the passage of current. Figures 6 and 7 are the plots showing the variation in thickness of Ni₃Sn₄ with time in the reaction couples annealed at 160°C and 180°C, respectively, with and without current. In the couple with current, thickness was measured at both the anode side interface, where electrons flew from Sn-3.5%Ag solder to EL-Ni, and cathode side interface, where they flew from EL-Ni to

solder. In the couple without current, Ni_3Sn_4 thicknesses at both the interfaces were nearly the same, therefore only one value was reported for each measurement. Electromigration influenced the growth of Ni_3Sn_4 at both the interfaces by retarding it and this effect was visible at $180^{\circ}C$ (Fig. 7) but negligible at $160^{\circ}C$ (Fig. 6). The absence of electromigration effect at $160^{\circ}C$ was due to the fact that the Ni_3Sn_4 growth was low at $160^{\circ}C$ (at which thickness varied from $2.6~\mu m$ to $3.3~\mu m$) as compared to $180^{\circ}C$ (at which thickness varied from $2.9~\mu m$ to $5.3~\mu m$). The lower growth at $160^{\circ}C$ is understood to be due to the lower diffusivity at $160^{\circ}C$ than at $180^{\circ}C$.

The growth of IMC in reaction couple depends upon the direction of mass fluxes at the reaction-interface. If fluxes flowing toward the reaction-interface are larger than the fluxes flowing outward, the IMC grow, whereas in the opposite case, they shrink. As mentioned previously, electromigration influences the atomic fluxes in heterogeneous materials system. In most of the systems, it enhances the atomic flux of species when electrons flow in the direction of species diffusion driven by the concentration gradient, whereas retards when electrons flow in the opposite direction. This electromigration effect was investigated in Ni/Sn and Ni/Sn-3.5%Ag systems [4,6,9]. It was observed that electromigration accelerates the Ni₃Sn₄ growth when electrons flow in the direction of Sn diffusion and when they flow in the opposite direction it retards the Ni₃Sn₄ growth [4]. It was found that electromigration influenced the Sn flux through Ni₃Sn₄, whereas it did not have significant affect on the Ni flux through Ni₃Sn₄. Similar explanation was reported for the electromigration effect in the Ni/Sn-3.5%Ag system [6].

In EL-Ni/Sn-3.5% Ag system, as mentioned in the previous section for Ni₃Sn₄ growth Ni comes from EL-Ni layer to Ni₃P/Ni₃Sn₄ interface through Ni₃P layer, which plays an important role in the electromigration effect upon the EL-Ni/Sn-3.5% Ag interfacial reactions. Figure 8 illustrates the electromigration effect on Ni₃Sn₄ growth in the EL-Ni/Sn-3.5% Ag system. When current passes through the Cu/EL-Ni/Sn-3.5% Ag/EL-Ni/Cu reaction couple, at the anode side interface, electromigration retards the Ni flux through the Ni₃P towards the Ni₃P/Ni₃Sn₄ interface, whereas at the cathode side interface, it retards the Sn flux through the Ni₃Sn₄ towards the Ni₃Sn₄/Ni₃P interface. As a result the Ni₃Sn₄ growth is less at both the interfaces, compared with the couple without the passage of current. Significant effect of electromigration on the Ni flux in the EL-Ni/Sn-3.5% Ag system, unlike in the Ni/Sn and

Ni/Sn-3.5% Ag systems, is expected due to the high resistivity of EL-Ni, which is one order of magnitude higher than that of pure Ni [20, 21].

3.4 Conclusion

In EL-Ni/Sn-3.5%Ag system, only one Ni_3Sn_4 IMC formed at the interface during annealing at 160°C and 180°C with and without the passage of current of 1×10^3 A/cm² density. The electric current does not show significant affect on Ni_3Sn_4 growth at 160°C since the diffusion activity at this temperature is relatively low. However, at 180°C it retards the Ni_3Sn_4 growth at both the anode and cathode side interfaces. This effect of electromigration on the EL-Ni/Sn-3.5%Ag system is due to the Ni_3P layer present between the EL-Ni and Ni_3Sn_4 . During Ni_3Sn_4 growth, Ni diffuses from EL-Ni to Ni_3P/Ni_3Sn_4 interface through Ni_3P grain boundaries. Thus, at anode side interface, where electrons flow from solder to EL-Ni, current retards the Ni flux through the Ni_3P toward the Ni_3P/Ni_3Sn_4 interface, where as at cathode side interface, where electrons flow from EL-Ni to solder, it retards the Sn flux through the Ni_3Sn_4 towards the Ni_3Sn_4/Ni_3P interface.

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List of Figure Captions

- Fig. 1. Schematic illustration of preparation of Cu/EL-Ni/Sn-3.5% Ag/EL-Ni/Cu reaction couples.
- Fig. 2. Schematic diagram of as-prepared EL-Ni/Sn-3.5% Ag reaction couple.
- Fig. 3. Schematic diagram of experimental setup used for electromigration study on the EL-Ni/Sn-3.5% Ag reaction couple
- Fig. 4. SEM image of (a) as-prepared couple (b) EL-Ni/Sn-3.5% Ag interface in as-prepared couple (c) EL-Ni/Sn-3.5% Ag interface in the couple annealed at 160°C for 400 h without current (d) EL-Ni/Sn-3.5% Ag interface in the couple annealed at 180°C for 400 h without current.
- Fig. 5. EDX analysis of different layers formed at the EL-Ni/Sn-3.5% Ag interface of asprepared couple (a) IMC layer, (b) EL-Ni layer and (c) dark thin EL-Ni layer underneath the IMC.
- Fig. 6. The thickness of Ni_3Sn_4 as a function of time in the sample annealed at 160°C, with and without the passage of current 1×10^3 A/cm².
- Fig. 7. The thickness of Ni_3Sn_4 as a function of time in the sample annealed at 180°C, with and without the passage of current 1×10^3 A/cm².
- Fig 8. Schematic illustration for electromigration effect on Ni₃Sn₄ growth in EL-Ni/Sn-3.5%Ag system.

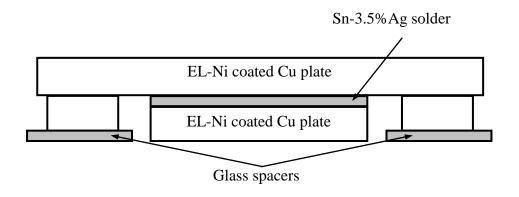


Fig. 1.

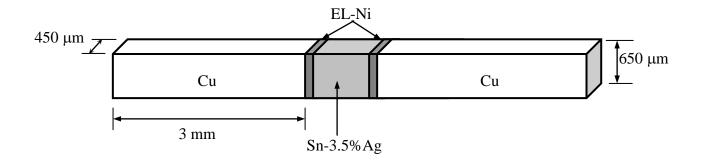


Fig. 2.

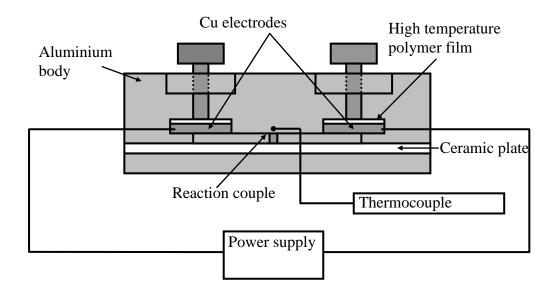


Fig. 3.

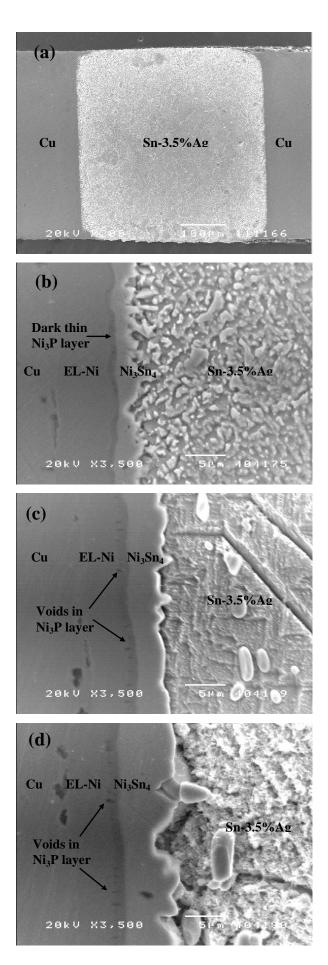
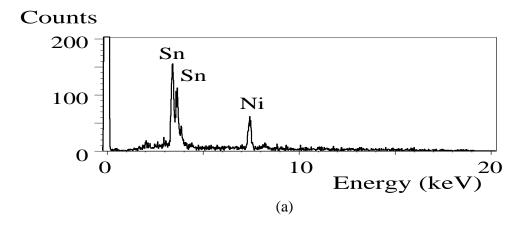
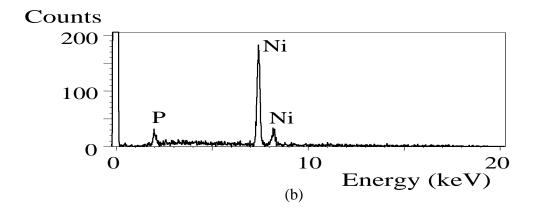


Fig. 4.





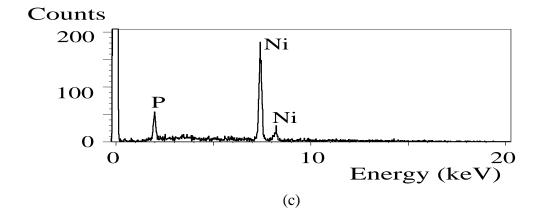


Fig. 5.

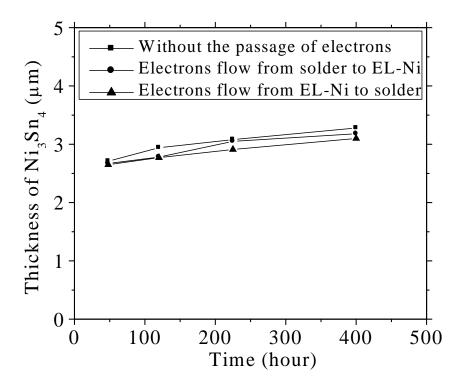


Fig. 6.

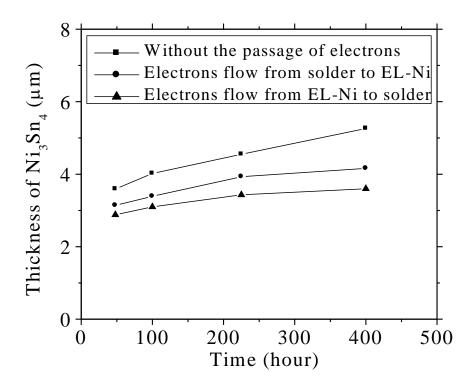
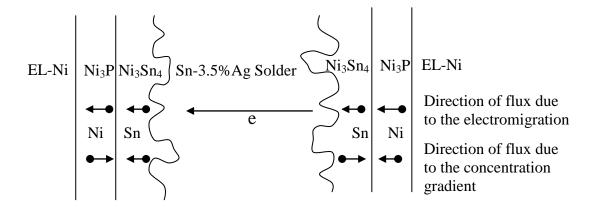


Fig. 7.



Anode side interface

Cathode side interface

Fig. 8.