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Self-imaging generation of plasmonic void arrays

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A plasmonic device is proposed to produce a self-imaging surface plasmon void array (2D surface bottle beam array) by the interference of two nondiffracting surface beams, namely, cosine-Gauss beams. The self-imaging surface voids are shown by full-wave calculations and then verified experimentally with an aperture-type near-field scanning optical microscope. We also demonstrate that the void array can be adjusted with flexibility in terms of the pattern and the number of voids. © 2013 Optical Society of America

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Optical voids, that is, low or null intensity regions in an optical field enclosed by higher intensity, have found numerous applications in recent years; for example intensity minima in a focused optical field were used to trap microparticles with low refractive indices in optical tweezers [1,2]. In a trap of atoms (laser cooling), if the trapping beam is blue-detuned from the resonant transition of the atoms, they will be confined by repulsive forces in the dark region [3,4]. A popular choice for the generation of optical voids is to use vortex beams that have a two-dimensional (2D) on-axis intensity minimum in the transverse plane throughout propagation [5]. Bottles waves, on the other hand, offer three-dimensional (3D) voids with additional intensity variation in the propagating direction [6]. A Gord and Padgett first constructed a bottle beam with a 3D intensity void from the interference of two phase Laguerre–Gaussian modes, LG00 and LG20, by using a computer-generated hologram [7]. Recently, various other types of bottle beams have been explored, for instance, a 3D dark focus [8], bottle beams with long nondiffracting distance [9], holographic optical bottle beams [9], and vortex bottle beams carrying orbital angular momentum [10]. It is noted, however, that all these bottle beams were generated for free-space applications. In this Letter, we extend the concept of bottle beams to surface waves by introducing a plasmonic device that generates an array of surface plasmon (SP) voids (2D bottle beams) tightly bound to an air–metal interface by the use of the self-imaging effect. In addition, we show that both the patterns and the number of SP voids are adjustable by varying the design of this plasmonic device.

The Talbot effect, that is, the self-imaging effect, was first observed in the study of transmission gratings and arrays of holes perforated in metal films [11]. With the self-imaging effect, an optical field repeats at a regular interval known as the Talbot length. However, it has been shown that the self-imaging effect can be created by the superposition of a proper set of nondiffracting beams in free-space without periodic structures like gratings [12]. A nondiffracting beam maintains its transverse profile as it propagates in free space. In this case, the self-imaging effect occurs when the propagation constants of the constituent nondiffracting beams are different. So the beating among different propagation constants results in periodically constructive interference and destructive interference forming the repeated optical field along the propagating direction [13]. In our study, this phenomenon is used to ensure that all the constituent SP voids in the near-field array have comparable sizes. In particular, the superposition of two nondiffracting surface waves, namely cosine-Gauss beams (CGB) [14], is employed to produce the self-imaging void arrays. A nondiffracting CGB can be generated by interfering two SP plane waves at half-intersecting angle $\theta$ shown in Fig. 1(a). The resultant 2D nondiffracting surface wave is characterized by

$$E_z(x; y) = E_0 \cos(k_x y) \exp(-y^2/w_0^2) \exp(ik_x x).$$

where $E_0$ is a complex constant, and $w_0$ denotes the beam waist in the $y$ direction. $k_x$ and $k_y$ are the $x$ and $y$ components of the SP plane wave propagation constant $k_{sp}$, respectively.

Two collinear CGBs with different half-intersecting angles $\theta_1$ and $\theta_2$ are generated simultaneously to create the self-imaging SP void array at the region where the two beams overlap with each other. The design scheme is shown in Fig. 1(b). Two SP line sources (solid red) with
intersecting angle \( \theta_1 \) on the left-hand side generates a CGB with the propagation constant labeled \( k_{x1} \), while the other two SP line sources (solid blue) on the right-hand side generated another CGB with a different propagation constant \( k_{x2} \). It is noted that, ideally, \( k_{x1} = k_{y0} \cos(\theta_1) \) and \( k_{x2} = k_{y0} \cos(\theta_2) \). The resultant 2D amplitude distribution of the superposition can thus be expressed as

\[
E^s_{x}(x, y) = E_{x1}(x, y) + E_{x2}(x, y) = E_{1} \cos(k_{y0} y) \exp(-y^2/w^2_y) \exp(ik_{x1} x) + E_{2} \cos(k_{y0} y) \exp(-y^2/w^2_y) \exp(ik_{x2} x). \tag{2}
\]

We show the self-imaging property (periodicity in the propagation direction) of the field by considering the variation of the on-axis \((y = 0)\) intensity. Also, the propagation constant of SP waves can be expressed in terms of its real and imaginary components as \( k_{sp} = k_{y0} + ik_{sp}' \). The approximation \( E_{1} \approx E_{2} = E_{0} \) is used in Eq. \((2)\), while the half-intersecting angles \( \theta_1 \) and \( \theta_2 \) are small. Therefore we have the on-axis intensity component distribution of SP waves expressed as

\[
I(x, 0) = |E^s_{x}(x, 0)|^2 = |E_{0}|^2 \{\exp(-2k_{sp}' x) + \exp(-2k_{sp}' x) + 2 \cos[(k_{x1} - k_{x2}) x] \exp[-(k_{x1} + k_{x2}) x]\}. \tag{3}
\]

The three exponents in Eq. \((3)\) indicate the inherent Ohmic propagation loss of SP waves. The sinusoidal intensity variation represented by the third term of Eq. \((3)\) is the result of the beating of two different propagation constants of CGBs in the \( x \) axis. Therefore, the period of the SP bottle array, depending on the cosine function in Eq. \((3)\), is given by \( T = \lambda_{sp}/(\cos \theta_1 - \cos \theta_2) \) within the overlapped region along the \( x \) axis, where

\[
\lambda_{sp} = \lambda_{0} \sqrt{\varepsilon_{d} + \varepsilon_{m}}/\varepsilon_{d}\varepsilon_{m} \tag{4}
\]

is the wavelength of SP waves. \( \lambda_{0} \) is the wavelength (633 nm) of the incident light. \( \varepsilon_{d} \) and \( \varepsilon_{m} \) are dielectric constants of the metal (Ag) and the medium (air), respectively.

Two pairs of grooves [Fig. 2(a)] with different half-intersecting angles were fabricated in a silver film on a glass substrate by focused ion beam milling to generate two CGBs with different propagating constants. The optically opaque silver film is 300 nm thick to avoid the interference caused by the directly transmitted incident light and the SP waves. In the example illustrated in Fig. 2, the half-angles \( \theta \) were chosen to be 5° and 20°, respectively, and the length of grooves \( D \) was set to be 10 \( \mu \text{m} \) for both constituent CGBs.

One can see that an array of self-imaging voids [two of them are isolated by the blue boxes and are shown in Figs. 2(c) and 2(e)] is obtained because of the self-imaging effect as a result of the interference of two nondiffracting CGBs. As a \( \pi \) phase jump exists between adjacent transverse intensity maxima of a CGB, there is half-period shift in the propagation direction for the intensity pattern across the \( y \) axis, which results in an intensity variation in the transverse direction. Numerical modeling of the near-field intensity distribution of the SP void array was performed with full-wave calculations based on the finite-difference time-domain (FDTD) method. The experimentally observed near-field intensity distribution [Figs. 2(d) and 2(e)] are in good agreement with the numerical calculations [Figs. 2(b) and 2(c)].

We further demonstrate that both the patterns and the number of voids can be controlled by varying the design of the plasmonic device. In Fig. 3, we give two designs \([D = 15 \mu \text{m}, \theta_1 = 10^\circ, \theta_2 = 20^\circ], \text{shown in Figs. 3(b) and 3(c)}, \theta_1 = 5^\circ, \theta_2 = 30^\circ] \text{shown in Figs. 3(d) and 3(e)}, \text{in which the length of grooves and the half-intersecting angles are different from those in the previous example (Fig. 2)} \text{while the rest of the parameters remain the same}. \text{The distance of the self-imaging area (area of array voids) depends on the minimum nondiffracting distance of the two CGBs. In our case, the distance of the}
self-imaging area is $x = D / \sin(\theta_2)$. Taking the periodicity of the plasmonic voids propagating in the $x$ direction, $\lambda_{SP} / (\cos \theta_1 - \cos \theta_2)$, into consideration, the number of on-axis plasmonic voids is $N = D (\cos \theta_1 - \cos \theta_2) / (\lambda_{SP} \sin \theta_2)$. In the simulations and the experiments, shown in Figs. 3(b), 3(e) and 3(c), 3(f), both the periodicity and the number of voids are determined by the half-intersecting angles $\theta_1$ and $\theta_2$. The theoretical periodicities of the plasmonic voids shown in Figs. 3(a) and 3(b) are 13.6 and 4.7 μm, which are close to the experimentally measured 13.9 and 4.9 μm.

In conclusion, we have shown that plasmonic voids can be generated by the self-imaging effect with a plasmonic device consisting of two pairs of intersecting grooves fabricated by focused ion beam milling on the surface of silver film. This phenomenon is based on the superposition of two nondiffraction CGBs generated by two pairs of grooves. The full-wave simulation and experimental results obtained by NSOM are in good agreement, and the results indicated that all the constituent SP voids in the near-field array had comparable sizes. Furthermore, we verified that both the pattern and the number of voids could be adjusted by simply varying the intersecting angles and the length of SP sources. This controllable property of SP void patterns could be useful toward developing plasmonic-based nanophotonics devices and planar plasmonic circuits. The 2D arrays of SP voids have great potential in the applications of near field optical trapping in terms of noninvasive manipulation [15,16], sorting 2D near-field particles [17,18], and laser cooling techniques [19,20].

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