

**NANYANG**  
**TECHNOLOGICAL**  
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**HYBRID TiO<sub>2</sub> PHOTOCATALYTIC CERAMIC  
MEMBRANES: FABRICATION,  
CHARACTERIZATION AND PERFORMANCE  
EVALUATION**

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**SCHOOL OF CIVIL AND ENVIRONMENTAL  
ENGINEERING**

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*<sup>23</sup> Whatever you do, work heartily, as for the Lord and not for men, <sup>24</sup> knowing that from the Lord you will receive the inheritance as your reward. You are serving the Lord Christ.  
(Colossians 3:23-24, ESV)*

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## SUMMARY

Titanium dioxide ( $\text{TiO}_2$ ) photocatalyst has been used extensively in many environmentally-sustainable applications owing to its sterling characteristics such as its excellent chemical and thermal stability, low toxicity, low cost and high quantum yield. The most photoactive polymorph of  $\text{TiO}_2$ , anatase, would initiate photocatalytic degradation of many noxious environmental pollutants upon the generation of the electron-hole ( $e^-$ - $h^+$ ) pairs under ultraviolet (UV) irradiation. The photocatalytic activity of  $\text{TiO}_2$  is highly dependent on its physico-chemical characteristics such as crystal structure, crystallite size, surface area, pore volume, and porosity. The integration of  $\text{TiO}_2$  photocatalysis and membrane separation process in a hybrid treatment system could be achieved either by a tandem operation of sequential photoreactor and membrane reactor or by operating a hybrid photocatalytic membrane reactor (PMR) in which the photocatalyst was anchored onto the membrane support. The PMR system allows simultaneous photocatalytic degradation and membrane separation of the pollutants in the feed water without the need of catalyst recovery at the end of each treatment process. This study aims to fabricate a hybrid  $\text{TiO}_2$  photocatalytic membrane to be used in the PMR treatment system. Thin layers of  $\text{TiO}_2$  photocatalyst were coated onto the macroporous alumina membrane support to obtain a dual-functional membrane that exhibits high water permeability, good photocatalytic degradation and good membrane separation performances.

In the first part of this study, Pluronic P-123, a tri-block copolymer, was used as the structure directing agent (SDA) in the preparation of  $\text{TiO}_2$  sols via acid-catalyzed sol-gel method. The mesoporosity of the resulting  $\text{TiO}_2$  layer was formed by the spontaneous self-assembly of the SDA. The SDA was subsequently removed during the calcination process

leaving behind a porous architecture of mesoporous TiO<sub>2</sub> layer. Generally, an increase in the amount of SDA added during the preparation of the TiO<sub>2</sub> sol would result in TiO<sub>2</sub> layer with higher overall surface area, larger porosity and pore sizes. A hierarchically porous hybrid photocatalytic membrane was fabricated via layer-by-layer coating of different TiO<sub>2</sub> layers formed with sols of varying SDA contents onto the macroporous alumina ceramic membrane support, starting from the TiO<sub>2</sub> layer of largest porosity and pore size on the support-TiO<sub>2</sub> interface followed by subsequent TiO<sub>2</sub> layers of decreasing porosity and pore size. Different hierarchical architectures of the P-123-based TiO<sub>2</sub> hybrid photocatalytic ceramic membranes were fabricated to obtain the optimum membrane performance. Various characterization techniques were employed to elucidate the physico-chemical and morphological characteristics of the resulting TiO<sub>2</sub> layer. The performance of the membrane was evaluated both in the batch photoreactor and continuous flow PMR operated in the dead-end filtration mode. All membranes exhibited a photo-induced super-hydrophilicity which was important for the photocatalytic degradation of the target pollutant. The membrane (Plu D) that consists of 3 sub-layers of P-123-10wt% TiO<sub>2</sub>, 2 sub-layers of P-123-5wt% TiO<sub>2</sub>, and a thin P-123-2wt% TiO<sub>2</sub> top layer exhibited the optimum membrane performance. The result suggested that the performance of the TiO<sub>2</sub> membrane could be optimized by tailoring the hierarchical architecture of the membrane.

In the second part of this study, various types of SDAs (i.e. Pluronic P-123, Triton X-100, Tween 20 and Tween 80) were used to prepare different TiO<sub>2</sub> sols. Four specimens of the TiO<sub>2</sub> photocatalytic membranes were prepared by multilayer coating of different TiO<sub>2</sub> sols prepared with single SDA. Two of the membrane specimens were prepared by coating TiO<sub>2</sub> sub-layers prepared with different SDAs. The TiO<sub>2</sub> sols prepared using different SDAs exhibited a good compatibility between the sub-layers, allowing flexibility of fabricating the

TiO<sub>2</sub> membrane that exhibited favorable operating parameters, i.e., high permeability, good photocatalytic performances or good membrane retention.

Finally, different types of Ag-decorated TiO<sub>2</sub> (Ag-TiO<sub>2</sub>) membranes were fabricated. The incorporation of Ag nanoparticles (Ag NPs) into the TiO<sub>2</sub> matrix enhanced the photocatalytic activity of TiO<sub>2</sub> and added an additional anti-bacterial functionality. The porous characteristics of the resulting Ag-TiO<sub>2</sub> layer could be fine-tuned by altering the amount of Ag and/or P-123 added into the sols. The Ag-TiO<sub>2</sub> membrane displayed a good chemical stability, leaching out 9.5 µg L<sup>-1</sup> of Ag after 6 h operation in the PMR and 27 µg L<sup>-1</sup> of Ag after 168 h of immersion in deionized (DI) water. The anti-bacterial property of the Ag-TiO<sub>2</sub> membrane was evaluated through the diffusion inhibition zone test and experiments using both batch reactor and PMR. In the batch reactor operated in dark, the membrane was able to remove a minimum of 5-logs of *Escherichia coli* (*E. coli*), a common water-borne pathogen. The membrane with the highest amount of incorporated Ag was able to remove close to 7-logs of *E. coli* when operated in the PMR.

The integration of the TiO<sub>2</sub> heterogeneous photocatalysis and membrane process in the membrane photoreactor offers simultaneous photodegradation and membrane separation, simpler system configuration with less mechanical and hydraulic fittings, and smaller overall footprint. The hierarchically porous TiO<sub>2</sub> photocatalytic membrane shows a great potential for use in water and wastewater treatment owing to its anti-fouling capability, high-flux performance, good photocatalytic activity, good anti-bacterial activity and reusability.

# TABLE OF CONTENT

ACKNOWLEDGEMENT.....	i
SUMMARY.....	iii
TABLE OF CONTENT .....	vi
LIST OF TABLES .....	ix
LIST OF FIGURES .....	xi
LIST OF SYMBOLS AND ABBREVIATIONS .....	xvii
LIST OF PUBLICATIONS.....	xx
CHAPTER 1 INTRODUCTION .....	1
1.1 Background .....	1
1.2 Motivation and knowledge gap.....	3
1.3 Objectives and scopes.....	5
1.4 The organization of Thesis .....	7
CHAPTER 2 LITERATURE REVIEW .....	9
2.1 Fundamental of heterogeneous photocatalysis .....	9
2.2 TiO <sub>2</sub> -assisted heterogeneous photocatalysis .....	13
2.2.1 Semiconductor photocatalysis.....	13
2.2.2 TiO <sub>2</sub> : structures, properties and syntheses.....	19
2.2.3 Improving photocatalytic activity and functionality of TiO <sub>2</sub> .....	28
2.2.3.1 Metal doped TiO <sub>2</sub> .....	28
2.2.3.2 Structure directing agent (SDA)-modified TiO <sub>2</sub> .....	30
2.3 TiO <sub>2</sub> -based hybrid photocatalytic ceramic membrane .....	33
2.4 Conclusion .....	55
CHAPTER 3 MATERIALS AND METHODS .....	56
3.1 Materials and synthesis techniques .....	56
3.1.1 Chemicals and materials .....	56
3.1.2 Preparation of macroporous alumina ceramic support .....	57
3.1.3 Preparation of TiO <sub>2</sub> sols.....	58
3.1.4 Preparation of Ag-TiO <sub>2</sub> sols.....	59
3.1.5 Fabrication of hierarchically porous TiO <sub>2</sub> photocatalytic ceramic membrane .....	60
3.1.6 Preparation of microbial strain.....	62

3.2 Photocatalytic membrane reactor (PMR) setup .....	62
3.3 Characterization techniques and analytical methods.....	65
3.4 Experimental procedures .....	67
3.4.1 Determination of photo-induced super-hydrophilicity .....	67
3.4.2 Photocatalytic degradation experiments using batch photoreactors.....	67
3.4.3 Photocatalytic degradation experiments using PMR.....	68
3.4.4 Silver leaching experiments .....	69
3.4.5 Diffusion inhibition zone experiments .....	70
3.4.6 Photocatalytic disinfection experiments using batch reactor .....	70
3.4.7 Photocatalytic disinfection experiments using PMR.....	71
3.4.8 Bacterial repair .....	71
<b>CHAPTER 4 HIGH PERMEABILITY TiO<sub>2</sub> PHOTOCATALYTIC MEMBRANE WITH HIERARCHICAL POROSITY: FABRICATION, CHARACTERIZATIONS, AND PERFORMANCES .....</b>	<b>72</b>
4.1 Introductions .....	72
4.2 Experimental procedures .....	74
4.2.1 Membrane fabrication.....	74
4.2.2 Characterization techniques .....	76
4.2.3 Evaluation of membrane performance.....	76
4.3 Results and discussion .....	78
4.3.1 Physico-chemical characteristics of sols.....	78
4.3.2 Characteristics of TiO <sub>2</sub> layers .....	82
4.3.3 Pure water permeability of P-123-based TiO <sub>2</sub> photocatalytic membrane.....	85
4.3.4 P-123-based TiO <sub>2</sub> photocatalytic membrane performances.....	89
4.3.4.1 Photocatalytic activity using batch photoreactor .....	89
4.3.4.2 Photocatalytic activity and flux performance using PMR .....	92
4.4 Conclusions.....	97
<b>CHAPTER 5 EFFECT OF DIFFERENT STRUCTURE DIRECTING AGENTS ON THE PERFORMANCES OF THE HIERARCHICALLY POROUS TiO<sub>2</sub> PHOTOCATALYTIC CERAMIC MEMBRANES.....</b>	<b>98</b>
5.1 Introductions .....	98
5.2 Experimental procedures .....	100

5.2.1 Membrane fabrication.....	100
5.2.2 Characterization techniques .....	102
5.2.3 Evaluation of membrane performance.....	102
5.3 Results and discussion .....	103
5.3.1 Physico-chemical characteristics of TiO <sub>2</sub> layers.....	103
5.3.2 Characteristics of TiO <sub>2</sub> photocatalytic ceramic membranes .....	111
5.3.3 Photocatalytic degradation of RhB using batch photoreactor.....	115
5.3.4 Photocatalytic degradation of RhB using PMR. ....	116
5.4 Conclusions.....	122
<b>CHAPTER 6 SILVER-DECORATED TiO<sub>2</sub> PHOOCATALYTIC CERAMIC MEMBRANE WITH HIERARCHICAL ARCHITECTURE: PHOTOCATALYTIC AND ANTIBACTERIAL ACTIVITIES.....</b>	
	123
6.1 Introductions .....	123
6.2 Experimental procedures .....	125
6.2.1 Membrane fabrication.....	125
6.2.3 Evaluation of membrane performance.....	127
6.3 Results and discussion .....	128
6.3.1 Characterization of Ag-TiO <sub>2</sub> layers.....	128
6.3.2 Characteristics of Ag-TiO <sub>2</sub> membranes.....	132
6.3.3 Photocatalytic degradation of RhB in the PMR reactor .....	137
6.3.4 Total Ag leaching of Ag-TiO <sub>2</sub> membranes .....	139
6.3.5 Anti-bacterial performance of Ag-TiO <sub>2</sub> membranes .....	141
6.3.5.1 Diffusion inhibition zone test .....	141
6.3.5.2 Anti-bacterial performance using batch reactor .....	143
6.3.5.3 Anti-bacterial performance using PMR .....	144
6.3.5.4 Anti-bacterial mechanisms of Ag-TiO <sub>2</sub> membranes .....	147
6.4 Conclusions.....	150
<b>CHAPTER 7 CONCLUSIONS AND RECOMMENDATIONS.....</b>	
	151
7.1 Conclusions.....	151
7.2 Recommendations for future research.....	152
REFERENCES .....	155

## LIST OF TABLES

<b>Table 2.1</b>	Fundamental processes of heterogeneous photocatalysis and its characteristic timescale (Hoffmann et al. 1995, Mills and Le Hunte 1997)	<b>13</b>
<b>Table 2.2</b>	Band gap energy of various common semiconductor materials (summarized from Linsebigler et al.(1995), Vinod and Anirudhan (2002), Kabra et al. (2004), Gaya and Abdullah (2008), and Thiruvengkatachari et al. (2008))	<b>14</b>
<b>Table 2.3</b>	Characterization tools for the determination of the extent of TiO <sub>2</sub> -assisted PCD reaction	<b>17</b>
<b>Table 2.4</b>	Characterization tools for TiO <sub>2</sub> materials	<b>24</b>
<b>Table 2.5</b>	Common types of SDA used in the preparation of mesoporous TiO <sub>2</sub>	<b>31</b>
<b>Table 2.6</b>	Characterization of ceramic membranes	<b>38</b>
<b>Table 2.7</b>	TiO <sub>2</sub> -based thin film and photocatalytic ceramic membrane: preparation, properties and performances	<b>41</b>
<b>Table 2.8</b>	Ag-decorated TiO <sub>2</sub> -based thin film and photocatalytic ceramic membrane: preparation, properties and performances	<b>47</b>
<b>Table 4.1</b>	Types of P-123-based membrane fabricated	<b>75</b>
<b>Table 4.2</b>	Physico-chemical characteristics of the as-synthesized TiO <sub>2</sub> layers	<b>78</b>
<b>Table 4.3</b>	Membrane performance in terms of its photocatalytic activity (PCA) and adsorptive-membrane retention (Ads-MR) after 8 h of operation	<b>94</b>
<b>Table 5.1</b>	Properties of different SDAs used	<b>99</b>
<b>Table 5.2</b>	Types of TiO <sub>2</sub> photocatalytic ceramic membranes fabricated	<b>101</b>
<b>Table 5.3</b>	Physico-chemical characteristics of the as-prepared TiO <sub>2</sub> layers	<b>103</b>
<b>Table 5.4</b>	Performance of TiO <sub>2</sub> photocatalytic ceramic membrane in terms of its photocatalytic activity (PCA) and adsorptive-membrane retention	<b>119</b>

	(Ads-MR) and percentage of initial flux retained after 8 h of operation	
<b>Table 6.1</b>	Types of Ag-TiO <sub>2</sub> photocatalytic membrane fabricated	<b>126</b>
<b>Table 6.2</b>	Physico-chemical characteristics of synthesized Ag-TiO <sub>2</sub> materials: (a) TiO <sub>2</sub> crystallite size, (b) BET surface area, and (c) BET porosity	<b>130</b>
<b>Table 6.3</b>	Performance of Ag-TiO <sub>2</sub> membrane in terms of its photocatalytic activity (PCA) and adsorptive-membrane retention (Ads-MR) and percentage of flux decline after 8 h of operation	<b>139</b>
<b>Table 6.4</b>	Time-dependent total-Ag leaching of Ag-TiO <sub>2</sub> membrane reported in (a) % of initial Ag loading and (b) in $\mu\text{g L}^{-1}$	<b>141</b>

## LIST OF FIGURES

<b>Figure 2.1</b>	Schematic of the PCD mechanism: (i) generation of charge carriers, (ii) reduction reaction involving photo-generated electrons, (iii) oxidation reaction involving photo-generated holes, (iv) recombination of charge carriers at the surface of photocatalyst, and (v) recombination of charge carriers in the bulk (modified from Mills and Le Hunte (1997)).	<b>10</b>
<b>Figure 2.2</b>	Energy level diagrams of various semiconductor materials with selected redox potential. The energy scales is referenced against vacuum and the normal hydrogen electrode (NHE) (taken from Choi et al.(2006a)).	<b>15</b>
<b>Figure 2.3</b>	Properties of different naturally-occurred TiO <sub>2</sub> polymorphs (summarized from Linsebigler et al. (1995), Di Paola et al. (2009), Park et al. (2009), and Smyth (2009)).	<b>19</b>
<b>Figure 2.4</b>	Colloidal and polymeric route of sol-gel synthesis using metal alkoxide as precursor (modified from Tsuru (2001)).	<b>22</b>
<b>Figure 2.5</b>	Metal-semiconductor (Ag-TiO <sub>2</sub> ) complexes that would prolong the life-time of photogenerated e <sup>-</sup> and h <sup>+</sup> pairs (taken from Zhao and Chen (2011)).	<b>28</b>
<b>Figure 2.6</b>	Flow diagram to prepare micro-/meso-porous ceramic membranes via the sol-gel technique (modified from Hsieh (1996)).	<b>35</b>
<b>Figure 3.1</b>	Molecular structure of Rhodamine B.	<b>57</b>
<b>Figure 3.2</b>	Photograph of alumina ceramic membrane support.	<b>57</b>
<b>Figure 3.3</b>	Schematic of preparation of the TiO <sub>2</sub> sol using sol-gel method.	<b>58</b>
<b>Figure 3.4</b>	Schematic of preparation of the Ag-decorated TiO <sub>2</sub> sol using sol-gel method.	<b>59</b>
<b>Figure 3.5</b>	Fabrication of hierarchically porous TiO <sub>2</sub> photocatalytic ceramic membrane.	<b>61</b>

<b>Figure 3.6</b>	Schematic diagram of the membrane cell module.	<b>63</b>
<b>Figure 3.7</b>	Schematic diagram of the PMR setup operating under dead-end filtration mode.	<b>64</b>
<b>Figure 3.8</b>	UV Labino 135 midlight lamp as the source of UV irradiation.	<b>64</b>
<b>Figure 4.1</b>	Image of the PMR reactor.	<b>77</b>
<b>Figure 4.2</b>	(a) N <sub>2</sub> adsorption/desorption curves and (b) pore size distribution of the pulverized TiO <sub>2</sub> layers with different amounts of P-123 added.	<b>80</b>
<b>Figure 4.3</b>	XRD spectra of the pulverized TiO <sub>2</sub> layers with different amounts of P-123 added.	<b>81</b>
<b>Figure 4.4</b>	SEM micrograph of surface of (a) alumina substrate, (b) Plu C, (c) Plu B, and Plu A membrane at (d) low and (e) high magnification (the inset in (d) depicts cross-sectional view of Plu A membrane).	<b>83</b>
<b>Figure 4.5</b>	Photoinduced super-hydrophilicity behavior of Plu A film coated on a borosilicate glass as shown on (a) as-coated sample, (b) upon 1 h of UV irradiation, and after (c) 8 h, (d) 24 h, and (e) 48 h left in the dark.	<b>84</b>
<b>Figure 4.6</b>	TiO <sub>2</sub> layer thickness and the resulting pure water flux of Plu A membrane with respect to the different sub-layers coated.	<b>86</b>
<b>Figure 4.7</b>	(a) PEG retention and (b) pure water permeability of P-123-based TiO <sub>2</sub> photocatalytic membrane.	<b>87</b>
<b>Figure 4.8</b>	Batch result of photocatalytic activity of (a) different configurations of TiO <sub>2</sub> photocatalytic membrane and (b) Plu A membrane at different initial concentrations of RhB (the inset depicts the linear plot of Langmuir-Hinshelwood model).	<b>90</b>
<b>Figure 4.9</b>	Shift of RhB maximum light absorption peak over the duration of the	<b>91</b>

photocatalytic degradation process.

- Figure 4.10** Specific RhB removal of Pluronic-based TiO<sub>2</sub> photocatalytic membrane **92**  
(the numerical values depict kinetic value based on initial RhB removal rate within 1<sup>st</sup> hour in mg m<sup>-2</sup> h<sup>-1</sup>).
- Figure 4.11** Anti-fouling property of TiO<sub>2</sub> photocatalytic membrane. **95**
- Figure 4.12** Reusability potential of the TiO<sub>2</sub> photocatalytic membrane: (a) specific RhB removal and flux performance with inter-cycles cleaning in the presence of UV irradiation; comparison of the effect of UV irradiation during inter-cycles cleaning in terms of (b) % flux recovery and (c) % RhB removal retained. **96**
- Figure 5.1** XRD spectra of the pulverized T80-1.0 TiO<sub>2</sub> layers calcined at different temperatures. **104**
- Figure 5.2** XRD spectra of the pulverized TiO<sub>2</sub> layers prepared with different SDAs. **106**
- Figure 5.3** FTIR spectra of the pulverized TiO<sub>2</sub> layers prepared with T80. **107**
- Figure 5.4** Raman spectra of the pulverized TiO<sub>2</sub> layers prepared with T80. **108**
- Figure 5.5** (a) N<sub>2</sub> adsorption/desorption isotherms and (b) pore size distributions of the pulverized TiO<sub>2</sub> layers prepared with different SDAs. **110**
- Figure 5.6** FESEM micrographs of the surface of: (a) Plu, (b) X, (c) T20, (d) T80, (e) M1 and (f) M2 membrane. (g) A high magnification FESEM micrograph of Plu membrane (the inset depicts cross-sectional view of Plu membrane). **111**
- Figure 5.7** Photoinduced super-hydrophilicity (PSH) property of TiO<sub>2</sub> thin films prepared using different SDAs. **112**
- Figure 5.8** Pure water permeability of different types of TiO<sub>2</sub> photocatalytic ceramic **113**

membranes (the numerical values depict average pure water permeance in  $\text{L m}^{-2} \text{h}^{-1} \text{Bar}^{-1}$ ).

- Figure 5.9** Performances of different types of  $\text{TiO}_2$  photocatalytic ceramic membranes in the batch photoreactor. **115**
- Figure 5.10** Performances of different types of  $\text{TiO}_2$  photocatalytic ceramic membrane in the PMR (the numerical values depict kinetic value based on initial RhB removal rate within 1<sup>st</sup> hour in  $\text{mg m}^{-2} \text{h}^{-1}$ ). **117**
- Figure 5.11** Reusability potential of the  $\text{TiO}_2$  photocatalytic ceramic membrane in terms of flux and specific RhB removal performance with UV-assisted inter-cycle cleaning. **120**
- Figure 5.12** Reusability potential of different types of  $\text{TiO}_2$  photocatalytic ceramic membranes in terms of (a) specific RhB removal retained and (b) flux retained after each UV-assisted inter-cycles cleaning (8h for each cycle). **121**
- Figure 6.1** (a) XRD spectra, (b)  $\text{N}_2$  adsorption/desorption curves, and (c) pore size distribution of the pulverized Ag- $\text{TiO}_2$  layers with different amounts of Ag added. **128**
- Figure 6.2** High resolution XPS spectra of (a) C 1s, (b) O 1s, (c) Ti 2p and (d) Ag 3d regions of the pulverized Ag- $\text{TiO}_2$  layers. **132**
- Figure 6.3** FESEM micrographs of Ag- $\text{TiO}_2$  photocatalytic membrane at (a) low and (b) high magnifications. (c) TEM and (d) HRTEM micrographs of R2 membrane (the inset depicts the corresponding SAED pattern). (e) EDX of the surface of R2 membrane. **133**
- Figure 6.4** Pure water permeability of Ag- $\text{TiO}_2$  photocatalytic membrane (The numerical values depict average pure water permeance in  $\text{L m}^{-2} \text{h}^{-1}$ ) **135**

Bar<sup>-1</sup>).

- Figure 6.5** Photo-induced super-hydrophilicity of R6-like thin film coated on a borosilicate glass as shown on (a) as coated thin film, (b) upon 1 h of UV irradiation, and after (c) 8 hr, (d) 24 h, and (e) 48 h left in the dark. **136**
- Figure 6.6** Specific RhB removal of Ag-TiO<sub>2</sub> photocatalytic membrane (the numerical values depict kinetic value based on initial RhB removal rate within 1<sup>st</sup> hour in mg m<sup>-2</sup> h<sup>-1</sup>). **138**
- Figure 6.7** Cumulative total-Ag leached from Ag-TiO<sub>2</sub> membrane operated in the PMR. **140**
- Figure 6.8** Diffusion inhibition zones of Ag-TiO<sub>2</sub> photocatalytic membrane against *E. coli* after 24 h incubation. **142**
- Figure 6.9** *E. coli* log reduction value of Ag-TiO<sub>2</sub> photocatalytic membrane showing its reusability over 4 cycles (duration of 8 h each cycle) of operation in a batch reactor. Error bars represent one standard deviation of at least three replicates of experimental runs. **143**
- Figure 6.10** Flux performance of Ag-TiO<sub>2</sub> photocatalytic membrane in the dead-end filtration mode of PMR with inter-cycle cleaning operating (a) with UV and (b) without UV. Percent flux recovery after each cleaning cycles when operating (c) with UV and (d) without UV. **145**
- Figure 6.11** *E. coli* log reduction values of Ag-TiO<sub>2</sub> photocatalytic membrane operating in a photocatalytic membrane reactor: at sampling point (2) when operating (a) with and (b) without UV. Error bars represent one standard deviation of at least three replicates of experimental runs. **146**
- Figure 6.12** *E. coli* log reduction values of Ag-TiO<sub>2</sub> photocatalytic membrane **147**

operating in a photocatalytic membrane reactor: at sampling point (3) after each cross-flow cleaning cycles when operating (a) with and (b) without UV. Error bars represent one standard deviation of at least three replicates of experimental runs.

**Figure 6.13** Log reduction values of *E. coli* at sampling point 3 after cross-flow cleaning cycle for various membranes. Error bars represent one standard deviation of at least three replicates of experimental runs. **148**

**Figure 6.14** (a) Possible mechanisms of anti-bacterial action inside the photocatalytic membrane reactor: direct UV disinfection (when subjected to a high UV intensity), membrane rejection, interaction with  $\text{Ag}^+$  ions, interaction with Ag nanoparticles, and bactericidal action of  $\text{TiO}_2$  and (b) Summary of different actions of bacteria inactivation. **149**

## LIST OF SYMBOLS AND ABBREVIATIONS

Ads-MR	Adsorptive-membrane retention
Ag NPs	Silver nanoparticles
Ag-TiO <sub>2</sub>	Silver-decorated titanium dioxide
AOPs	Advanced oxidation processes
BET	Brunauer-Emmett-Teller
BJH	Barrett-Joyner-Halenda
CB	Conduction band
CMC	Critical micelle concentration
CS	Crystallite size
DI H <sub>2</sub> O	Deionized water
DRS	Diffuse reflectance spectra
EDX	Energy dispersive x-rays
E <sub>g</sub>	Band-gap energy
EtOH	Ethanol
FESEM	Field emission scanning electron microscopy
FTIR	Fourier transform infrared
FWHM	Full width at half maximum
HLB	Hydrophile-lipophile balance
HAP	hydroxyapatite
hν	photon energy
HPC	Hydroxypropyl cellulose
HRTEM	High-resolution transmission electron microscopy
ICP-MS	Inductively coupled plasma-mass spectroscopy
ICP-OES	Inductively coupled plasma-optical emission spectroscopy
IPA	Isopropanol

$K_{ads}$	Langmuir adsorption constant
$k_{app}$	Pseudo first-order rate constant
$\lambda$	Wavelength
MB	Methylene blue
MF	Microfiltration
MW	Molecular weight
MWCO	Molecular weight cut-off
NF	Nanofiltration
NHE	Normal hydrogen electrode
NOM	Natural organic matter
P25	Degussa/Evonik P25 (TiO <sub>2</sub> )
PCA	Photocatalytic activity
PCD	Photocatalytic degradation
PCO	Photocatalytic oxidation
PEG	Polyethylene glycol
PL	Photoluminescence
P-123	Pluronic P-123
PMR	Photocatalytic membrane reactor
PSH	Photo-induced super-hydrophilicity
PVA	Polyvinyl alcohol
PWP	Pure water permeability
RhB	Rhodamine B
RO	Reverse osmosis
ROS	Reactive oxygen species
rpm	Rotation per minute
SAED	Selected area electron diffraction
SDA	Structure directing agent
T20	Tween 20

T80	Tween 80
TGA	Thermogravimetric analysis
TMP	Trans-membrane pressure
TOC	Total organic carbon
TTIP	Titanium tetraisopropoxide
UF	Ultrafiltration
UV	Ultraviolet
UV-LED	Ultraviolet light emitting diode
VB	Valence band
VCA	Video contact angle
Vis	Visible light
$V_p$	Pore volume
X100	Triton X-100
XPS	X-rays photoelectrons spectroscopy
XRD	X-rays diffraction
$\rho$	Density

## LIST OF PUBLICATIONS

### Parts of the findings presented in this thesis have been published in the following journal papers:

**R. Goei**, and T.-T. Lim. Ag-decorated TiO<sub>2</sub> photocatalytic membrane with hierarchical architecture: Photocatalytic and anti-bacterial activities. *Water Research*. 59 (2014) 207-218.

**R. Goei**, and T.-T. Lim. Asymmetric TiO<sub>2</sub> hybrid photocatalytic ceramic membrane with porosity gradient: Effect of structure directing agent on the resulting membranes architecture and performances. *Ceramics International*. 40 (2014) 6747-6757.

**R. Goei**, Z. Dong, T. -T. Lim, High-permeability pluronic-based TiO<sub>2</sub> hybrid photocatalytic membrane with hierarchical porosity: Fabrication, characterizations and performances. *Chemical Engineering Journal*. 228 (2013) 1030-1039.

### Co-authorship in others' work:

D. Hou, **R. Goei**, X. Wang, P. Wang, T. -T. Lim, Preparation of carbon-sensitized and Fe-Er codoped TiO<sub>2</sub> with response surface methodology for bisphenol A photocatalytic degradation under visible-light irradiation. *Applied Catalysis B: Environmental*. 126 (2012) 121-133.

T. -T. Lim, K. H. Goh, **R. Goei**, Z. Dong, Mechanistic and thermodynamic studies of oxyanion sorption by various synthetic Mg/Al layered double hydroxides. *Water Science & Technology*. 59 (2009) 1011-1017.

# CHAPTER 1 INTRODUCTION

## 1.1 Background

Water shortage is one of the major issues faced both by the developed as well as the developing countries. Clean water is needed for domestic usage, agricultural development, and industrial processes. Water reclamation has been considered as an alternative source of water and its potential usage in a land scarce country like Singapore has preceded over other traditional sources of water supply to overcome the problem of water shortage (PUB 2014). In order to fully realize the potential of water reclamation, the removal of different types of water-borne pollutants from domestic and industrial wastewater needs to be considered. A novel and robust wastewater treatment is required to overcome the problem caused by different emerging contaminants. Commonly used water treatment processes include chemical and physical treatment and biological treatment (Aksu 2005, Appels et al. 2008, Bailey et al. 1999, Chen 2004, Chong et al. 2010, Gogate and Pandit 2004, Haritash and Kaushik 2009, Malato et al. 2009). Some of these treatments would introduce various types of chemicals into the treatment system or produce some secondary pollutants, which maybe more toxic than the primary pollutants (Magdeburg et al. 2014, Malato et al. 2003, Xiao et al. 2014, Zong et al. 2013).

The use of membrane separation for water purification has gained much interest in the last decades. Microporous membrane was first used to pre-treat drinking water supply during World War II in Europe (Baker 2004). Industrial scale wastewater reclamation using reverse osmosis (RO) membrane was triggered by the work of Loeb and Sourirajan (1963) who fabricated a defect free, high flux anisotropic RO membrane. Since then, membrane separation has been used widely in water filtration, medical separation process, gas separation, chemical purification and many other applications. The advantages of membrane technology

are low energy consumption, allowing continuous operation, easy to upscale and combine with other processes, good effluent quality and adjustable membrane properties (Baker 2004, Mulder 1996). However, inherent drawback of membrane fouling has led to higher operational and overall energy consumption in the treatment process (Gander et al. 2000, Le-Clech et al. 2006, Seidel and Elimelech 2002).

On the other hand, heterogeneous photocatalysis is deemed as an environmental friendly method to degrade many types of noxious and recalcitrant pollutants (Fox and Dulay 1993, Herrmann 1999, 2005). Heterogeneous photocatalysis is characterized by the formation of highly reactive radicals that are able to oxidize and degrade by mineralizing various recalcitrant contaminants (Herrmann 1999). These radicals include hydroxyl, superoxide and hydroperoxyl radicals. Characteristic features of the hydroxyl radical are highly reactive, powerful oxidant, easy to produce, ubiquitous in nature, possessing electrophilic property, non-selective reagent, relatively short lifespan, and its reaction with appropriate substrate molecules are kinetically controlled (Oppenländer 2003). Various advantages of heterogeneous photocatalysis over other advanced oxidation processes are zero/minimum usage and production of hazardous chemicals, and the opportunity to tap into abundant solar irradiation as the source of energy for the treatment process (Gaya and Abdullah 2008, Liu et al. 2006, Pirkanniemi and Sillanpää 2002, Rajeshwar et al. 2008). This is despite the possible limitation arising from the large scale applications.

The interest to couple photocatalytic processes and membrane separation has started with the introduction of photocatalytic oxidation treatment in tandem with a membrane separation treatment (Azrague et al. 2005, Molinari et al. 2004, Rivero et al. 2006). In this process configuration, the photocatalyst was introduced in the suspension prior to the membrane reactor. The main disadvantage of photocatalyst in suspension system is the need to recover

the photocatalyst after the treatment process. The integration of photocatalytic oxidation and membrane separation in a single hybrid treatment system was advocated.

Polymeric membranes have been used extensively in water/wastewater treatment process. However the disadvantages of the polymeric membrane are its poor chemical, thermal and photo-stability under UV irradiation which limits its used for the hybrid photocatalytic membrane process (Artale et al. 2001). The need to fabricate membrane that is chemically stable and able to withstand UV irradiation had brought interest to the usage of ceramic membrane. Ozdemir et al. (2006) reported that inorganic membrane (ceramic and metal) are used extensively in the study that combine membrane and catalyst, most of which involve gas phase reaction at elevated temperature. Ceramic membrane has shown superior quality in terms of its heat stability, mechanical properties, biological stability, easy to clean, stability to UV light irradiation and chemical stability in different corrosive environments (Anderson et al. 1988, Buekenhoudt 2008). Other advantages are its high selectivity, longer life span and therefore long term cost competitiveness.

## **1.2 Motivation and knowledge gap**

TiO<sub>2</sub> photocatalyst has been used extensively in many environmentally-sustainable applications owing to its sterling characteristics such as its excellent chemical and thermal stability, low toxicity, low cost and high quantum yield. The integration of the TiO<sub>2</sub> photocatalysis and membrane separation process in a hybrid treatment system could be achieved either by the operation of separate photo- and membrane reactor in succession or by the operation of hybrid photoreactor that carry out simultaneous photocatalytic degradation reaction and membrane separation (Lim et al. 2011). The former requires photocatalyst

recovery from the treated water. The latter could suffer from possible mass transfer limitation and lower photocatalytic degradation efficiency due to its smaller number of active sites.

Immobilizing  $\text{TiO}_2$  photocatalyst onto the membrane support could overcome the requirement of catalyst recovery for the separate reactor system. Besides, the immobilization of  $\text{TiO}_2$  may overcome the issue of mass transfer limitation through the forced permeation of pollutants across the photocatalytic layers of the membrane activated by UV irradiation.

However, the synergistic coupling of the hybrid photocatalytic membrane has long standing operational issues that need to be addressed: low water permeability and adverse loss of permeation over a prolonged usage period caused by membrane fouling. In order to address the above-mentioned issues and to fabricate an effective hybrid photocatalytic membrane, the following strategies could be adopted:

- The membrane support should be chemically stable under UV irradiation.
- The membrane should be as thin as possible to minimize the intrinsic resistance of the membrane without compromising the integrity of the membrane during operation.
- The hybrid membrane should possess a hierarchically porous architecture which can improve the water permeation through the membrane. The hierarchical architecture can be achieved through coating of multiple  $\text{TiO}_2$  sub-layers of different porous structures.
- The microstructural of the  $\text{TiO}_2$  photocatalytic sub-layer must be controllable during the fabrication process. This would allow easy fine-tuning of fabrication parameters in order to achieve an optimum membrane performance.
- The coated photocatalytic  $\text{TiO}_2$  sub-layers must be of uniform thickness with minimal presence of cracks, pinholes, or other defects.
- A flow-through membrane reactor should be setup to carry out simultaneous photocatalytic degradation reaction and membrane separation.

- The pollutant should be photocatalytically degraded when they travel through the hierarchically porous membrane.
- The membrane reactor setup should be able to treat various types of environmental noxious micropollutants.

Therefore, it is important to develop a TiO<sub>2</sub> hybrid photocatalytic membrane which allows effective removal of environmental pollutants through simultaneous degradation and separation process. The membrane system should operate in the high flux condition and allow re-utilization after appropriate cleaning. The flexibility to optimize the resulting membrane performance by controlling various membrane fabrication parameters is desirable.

### **1.3 Objectives and scopes**

This research aimed to fabricate, characterize, and evaluate the performances of a hierarchically porous TiO<sub>2</sub> hybrid photocatalytic ceramic membrane. Different structure directing agents (SDAs) were employed to achieve the hierarchical architecture. At the later stage, this study also aimed to further enhance the functionality of the TiO<sub>2</sub> membrane by the addition of Ag in the TiO<sub>2</sub> photocatalytic layers. The Ag-decorated TiO<sub>2</sub> (Ag-TiO<sub>2</sub>) membrane could effectively inactivate bacterial cells through different anti-bacterial actions. The performances of membranes are to be tested both in the batch photoreactor and the flow-through PMR.

The detailed scope of works for this study is as follows:

1. Designing and commissioning of photocatalytic membrane reactor (PMR)
  - i. To design and commission a hybrid PMR system comprising an UV irradiation source, pumps, valves, and monitoring system;

- ii. To design and fabricate a membrane cell module to allow performance evaluation of the  $\text{TiO}_2$  / Ag- $\text{TiO}_2$  membranes in the PMR;
  - iii. To establish performance evaluation protocol using the PMR both for PCD and anti bacterial experiments.
2. Fabrication and performance evaluation of the hierarchically porous  $\text{TiO}_2$  photocatalytic ceramic membrane
  - i. To synthesize and characterize  $\text{TiO}_2$  membrane layers prepared by sol-gel method using Pluronic P-123 (P-123) as the SDA;
  - ii. To fabricate a hierarchically porous  $\text{TiO}_2$  photocatalytic ceramic membrane via layer-by-layer coating of the different  $\text{TiO}_2$  sub-layers;
  - iii. To characterize photo-induced super-hydrophilicity (PSH) of the  $\text{TiO}_2$  membrane;
  - iv. To evaluate pure water permeability and membrane retention capability of the  $\text{TiO}_2$  membrane;
  - v. To evaluate photocatalytic degradation (PCD) performance of the  $\text{TiO}_2$  membrane both in the batch photoreactor and PMR;
  - vi. To evaluate reusability potential of the  $\text{TiO}_2$  membrane.
3. Fabrication and performance evaluation of various hierarchically porous  $\text{TiO}_2$  photocatalytic ceramic membranes which were prepared using different types of SDAs
  - i. To synthesize and characterize  $\text{TiO}_2$  membrane layers prepared by sol-gel method using different types of SDAs;

- ii. To fabricate different types of hierarchically porous TiO<sub>2</sub> photocatalytic ceramic membranes with the photocatalytic TiO<sub>2</sub> sub-layers prepared using different SDAs;
  - iii. To evaluate the PCD performance of the composite membranes both in the batch photoreactor and PMR;
  - iv. To evaluate the reusability potential of the composite membrane.
4. Fabrication and performance evaluation of Ag-TiO<sub>2</sub> membrane
- i. To prepare various types of Ag-TiO<sub>2</sub> sols;
  - ii. To fabricate different types of the Ag-TiO<sub>2</sub> membranes;
  - iii. To evaluate the PCD performance of the Ag-TiO<sub>2</sub> membranes in the PMR;
  - iv. To quantify the amount of total-Ag leaching from the Ag-TiO<sub>2</sub> membranes;
  - v. To evaluate the diffusion inhibition zone of the Ag-TiO<sub>2</sub> membranes;
  - vi. To evaluate the anti-bacterial performance of the Ag-TiO<sub>2</sub> membranes both in the batch reactor and PMR based on *Escherichia coli* (*E. coli*) inactivation.

## **1.4 The organization of Thesis**

This thesis comprises seven chapters. Chapter 1 presents the background, motivation, knowledge gap, objectives, scope of works of this study and the organization of this thesis. Chapter 2 provides a review of the fundamentals of heterogeneous photocatalysis, the usage of TiO<sub>2</sub> as efficient photocatalyst, as well as brief introduction to the ceramic membrane and its usage as the support in a hybrid treatment system utilizing TiO<sub>2</sub> as the photocatalysis. Chapter 2 also discusses the recent findings in the research area of the TiO<sub>2</sub> hybrid photocatalytic ceramic membrane. Chapter 3 describes the materials and methods used in this study, including the experimental procedures adopted to fabricate, characterize and evaluate the performance of the TiO<sub>2</sub> hybrid photocatalytic ceramic membrane. Chapter 4 presents the

synthesis and characterization of high permeability TiO<sub>2</sub> hybrid photocatalytic ceramic membrane that possesses a hierarchical porous architecture. Chapter 5 presents the studies on the effect of different SDAs in tailoring the resulting performance of TiO<sub>2</sub> hybrid photocatalytic ceramic membrane. Chapter 6 elucidates the facile preparations of Ag-TiO<sub>2</sub> hybrid photocatalytic ceramic membrane and their physico-chemical characteristics, pollutant removal capabilities and the anti-bacterial functionality of the Ag-TiO<sub>2</sub> membrane against *E. coli*. Chapter 7 presents a summary of important conclusions derived from this study and also several recommendations for the future work.

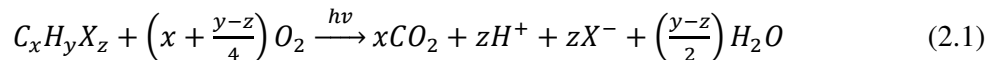
## CHAPTER 2 LITERATURE REVIEW

### 2.1 Fundamental of heterogeneous photocatalysis

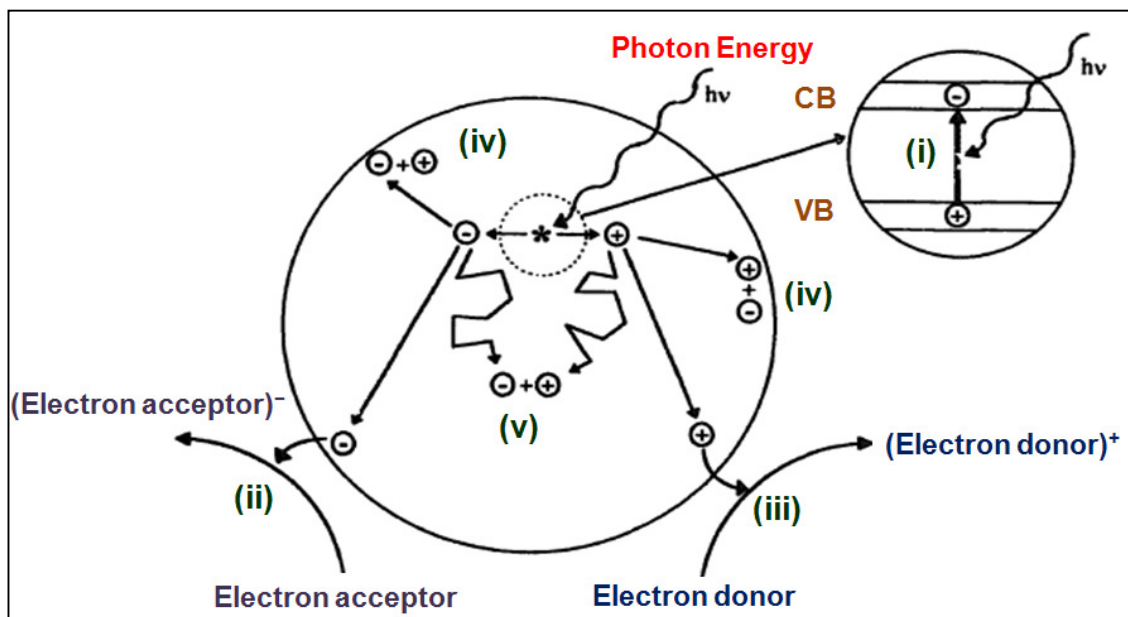
Heterogeneous photocatalysis is a subset of advanced oxidation processes (AOPs) in which the catalyst used and the reactants are of different phases. Heterogeneous photocatalysis could be carried out either in the aqueous solution, pure organic liquid phase, or in the gas phase. Fujishima and Honda (1972) through their pioneering discovery of water splitting in the irradiated TiO<sub>2</sub> electrode without any externally applied voltage, has triggered a worldwide intensive researches on the heterogeneous photocatalysis. The detailed studies of heterogeneous photocatalysis have been widely discussed in the literature (Carp et al. 2004, Fujishima and Zhang 2006, Herrmann 1999, 2005, Hoffmann et al. 1995, Linsebigler et al. 1995, Ollis and Al-Ekabi 1993). Photocatalytic degradation (PCD) reaction of pollutant in water consists of 5 major sequential steps (Herrmann 1999): (1) transfer of reactants from the bulk fluid phase to the surface of the catalyst, (2) adsorption of the reactants, (3) reaction in the adsorbed phase, (4) desorption of the products, and lastly (5) removal of the products from the interface region.

PCD of organic pollutants, microorganisms and other recalcitrant environmental pollutants was caused by the attack of the non-selective radicals generated on the surface of the photocatalyst via a photonic activation. The main advantage of the PCD reaction is the possibility of the complete mineralization of the pollutants resulting in an efficient treatment process with minimal handling of the secondary pollutants. Furthermore, PCD process can be carried out in a very mild operating temperature and pressure condition. Complete degradation occurred when all chemical constituents of the pollutant are mineralized into its inorganic forms i.e. carbon to carbon dioxide (CO<sub>2</sub>), hydrogen to water (H<sub>2</sub>O), nitrogen to

nitrate ( $\text{NO}_3^-$ ), halogen to halide ions ( $\text{X}^-$ ), sulfur to sulfates ( $\text{SO}_4^{2-}$ ), and phosphorus to phosphate ( $\text{PO}_4^{3-}$ ) (Carp et al. 2004). PCD reaction of an organic compound can be generalized as follows (Hoffmann et al. 1995):

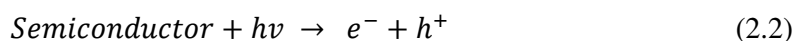


Characteristics of a good photocatalyst are high photo-reactivity, efficient utilization of visible or near UV irradiation, biologically and chemically inert, good photo-stability, low toxicity, and low production cost (Gaya and Abdullah 2008, Vinod and Anirudhan 2002). Semiconductor materials possess a unique electronic structure which consists of valence band (VB) and conduction band (CB) separated by an energy gap known as band gap. This unique characteristic allowed effective utilization of photonic energy to produce the reactive non-selective agents for PCD reaction.



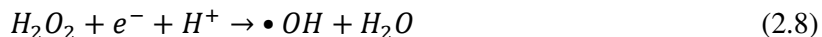
**Figure 2.1** Schematic of the PCD mechanism: (i) generation of charge carriers, (ii) reduction reaction involving photo-generated electrons, (iii) oxidation reaction involving photo-generated holes, (iv) recombination of charge carriers at the surface of photocatalyst, and (v) recombination of charge carriers in the bulk (modified from Mills and Le Hunte (1997)).

A graphical illustration of the photocatalytic processes in the semiconductor materials is presented in Fig 2.1. The photocatalytic process starts with the absorption of photonic energy that is equal or greater than the prescribed intrinsic band gap energy of the semiconductor materials. The absorbed energy is utilized to excite a photo-generated electron ( $e^-$ ) overcoming the band gap energy to the CB, leaving behind a photo-generated hole ( $h^+$ ) in its VB (Eq. 2.2). A reduction reaction (Eq. 2.3) between the  $e^-$  and electron acceptors (e.g. dissolved  $O_2$ ) produces superoxide radicals ( $\bullet O_2^-$ ). On the other hand, an oxidation reaction (Eq. 2.4) occurred between  $h^+$  with electron donors (e.g. adsorbed  $H_2O$  or hydroxide ions ( $OH^-$ )) produces hydroxyl radicals ( $\bullet OH$ ). These radicals are the non-selective reagents that would react and mineralize the target pollutants.



The  $\bullet O_2^-$  would trigger the formation of other chemical species (Eq. 2.5 - 2.8) in water such as hydroperoxyl radicals ( $\bullet OOH$ ), hydrogen peroxide ( $H_2O_2$ ), singlet oxygen species ( $^1O_2$ ) and eventually form the  $\bullet OH$ . The hydroperoxyl radicals would further prolong the life time of  $h^+$  by acting as an electron scavenger (Gaya and Abdullah 2008). The formation of  $\bullet OH$  is essential to ensure non-selective oxidation of the target pollutants. The  $\bullet OH$  radical possesses a very high standard redox potential of +2.8 V vs NHE (normal hydrogen electrode), second only to fluorine (of +3.03 V vs NHE) (Egerton and Christensen 2004). All the reactive oxygen species (ROS) generated (Eq. 2.5 – 2.8) holds a significant role in the PCD of the target pollutants depending on the exact experimental condition (Fujishima and Zhang 2006).

In the acidic condition:



Besides the above mentioned mechanisms, the photogenerated  $e^-$ - $h^+$  pairs could recombine either at the surface of the photocatalyst or in the bulk. The recombination steps could hinder the efficiency of the photocatalytic process (Herrmann 1999). Additionally, the charge carriers could be trapped in the meta-stable surface state of the dopant element in the case of metal/non-metal decorated photocatalyst (Hoffmann et al. 1995).

The general scheme of PCD reaction can be classified into 4 fundamental processes: generation of the charge carriers, trapping of the charge carriers, recombination process, and the interfacial charge transfer. The characteristic timescales for each fundamental process are delineated in Table 2.1. The efficiency of PCD reaction is limited by the recombination of the photogenerated  $e^-$ - $h^+$  pairs prior to the important activation of the superoxide species (Gerischer and Heller 1991). The recombination of  $e^-$ - $h^+$  pairs occur rapidly with the timescale in the order of nanoseconds (Rothenberger et al. 1985). It would result in overall lower quantum efficiency. It is generally accepted that the target pollutant undergo oxidation reaction by the surface-bound  $\bullet OH$ , although a direct oxidation via direct  $h^+$  transfer is also plausible (Turchi and Ollis 1989). Thus, it is vital that the target pollutants are in the vicinity of the photocatalyst surface and the electron donor or acceptor are presence sufficiently in the

aqueous reactor for the generation of  $\bullet OH$  to ensure effective PCD reaction with high quantum efficiency (Jing et al. 2006).

**Table 2.1** Fundamental processes of heterogeneous photocatalysis and its characteristic timescale (Hoffmann et al. 1995, Mills and Le Hunte 1997)

<b>Fundamental Processes</b>	<b>Characteristic Timescale</b>	
<b>Charge-carrier Generation</b>		
$TiO_2 + h\nu \rightarrow e^- + h^+$	fs (very fast)	(2.9)
<b>Charge-carrier Trapping</b>		
$h^+ + >Ti^{IV}OH \rightarrow (>Ti^{IV}OH^{\bullet+})$	10 ns (fast)	(2.10)
$e^- + >Ti^{IV}OH \leftrightarrow (>Ti^{III}OH)$	100 ps (shallow trap, dynamic equilibrium)	(2.11a)
$e^- + >Ti^{IV} \rightarrow >Ti^{III}$	10 ns (deep trap, irreversible)	(2.11b)
<b>Charge-carrier Recombination</b>		
$e^- + (Ti^{IV}OH\bullet)^+ \rightarrow >Ti^{IV}OH$	100 ns (slow)	(2.12)
$h^+ + (>Ti^{III}OH) \rightarrow >Ti^{IV}OH$	10 ns (fast)	(2.13)
<b>Interfacial Charge Transfer</b>		
$(Ti^{IV}OH\bullet)^+ + Red \rightarrow >Ti^{IV}OH + Red^{\bullet+}$	100 ns (slow)	(2.14)
$e_{trap}^- + Ox \rightarrow >Ti^{IV}OH + Ox^{\bullet-}$	ms (very slow)	(2.15)

Note:  $>TiOH$  = primary hydrated surface functionality of  $TiO_2$ ;  $e^-$  = conduction band electron;  $h^+$  = valence band hole;  $e_{trap}^-$  = trapped conduction band electron; **Red** = electron donor; **Ox** = electron acceptor;  $(Ti^{IV}OH\bullet)^+$  = surface trapped valence band hole and  $(>Ti^{III}OH)$  = surface trapped conduction band electron

## 2.2 $TiO_2$ -assisted heterogeneous photocatalysis

### 2.2.1 Semiconductor photocatalysis

Semiconductor materials with its unique electronic states are appraised as suitable candidates for a good photocatalyst. Unlike the continuum electronic state of metallic materials, semiconductor materials have an energy band gap. Band gap values signify the

amount of energy to be supplied for photo excitation process to take place. The band-gap energy of some common semiconductor materials is summarized in Table 2.2.

The relation between band gap and energy of radiation required to excite the  $e^-$ - $h^+$  pairs is governed by classical physics law (Eq. 2.16):

$$E = h\nu \quad (2.16)$$

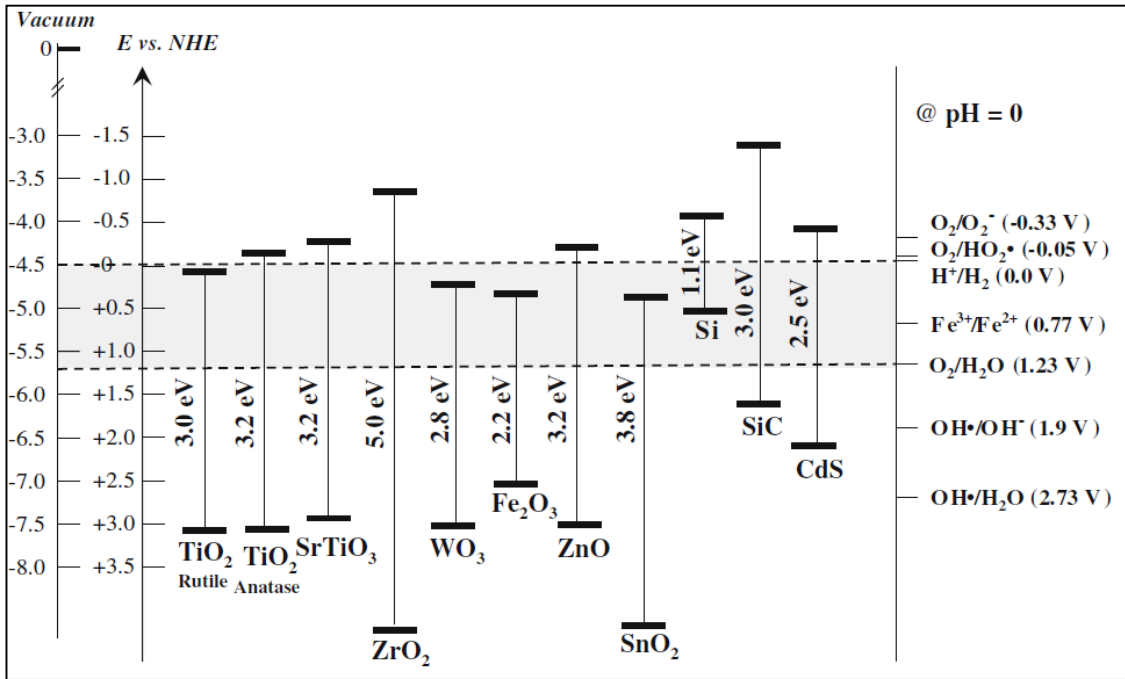
$$\lambda = \frac{1237}{E_g} \quad (2.17)$$

where E is the photon energy, h is Planck's constant of  $6.626 \times 10^{-34} \text{ m}^2 \text{ kg s}^{-1}$ , and  $\nu$  is the frequency of the electromagnetic wave oscillation contained in the incoming photon. Photon frequency can be further expanded as the ratio of speed of light with respect to the photon energy wavelength. The minimum wavelength (nm) of the photon required for the photo-generation of the  $e^-$  and  $h^+$  pairs for a given band-gap energy of the semiconductor material is delineated in Eq. 2.17.

**Table 2.2** Band gap energy of various common semiconductor materials (summarized from Linsebigler et al.(1995), Vinod and Anirudhan (2002), Kabra et al. (2004), Gaya and Abdullah (2008), and Thiruvengkatachari et al. (2008))

Types	$E_g$ (eV)	$\lambda$ (nm)	Types	$E_g$ (eV)	$\lambda$ (nm)
CdS	2.30-2.50	538 - 495	SiC	3.00	412
CdSe	1.70	728	SnO <sub>2</sub>	3.50-3.80	353 - 326
Cu <sub>2</sub> O	3.90	317	SrTiO <sub>3</sub>	2.40-3.20	515 - 387
Fe <sub>2</sub> O <sub>3</sub>	2.20-2.80	562 - 442	TiO <sub>2</sub> (Rutile)	3.00	412
$\alpha$ -Fe <sub>2</sub> O <sub>3</sub>	3.10-3.50	399 - 353	TiO <sub>2</sub> (Anatase)	3.20	387
GaAs	1.40	884	WO <sub>3</sub>	2.80-3.40	442 - 364
GaP	2.25	550	WSe <sub>2</sub>	1.20	1030
PbS	2.20	562	ZnO	3.20-3.40	387 - 364
PbSe	0.20-0.30	6200	ZnS	3.10-3.70	400 - 334
Si (metal)	1.10	1125	ZrO <sub>3</sub>	5.00	25

From the Equation 2.17 and Table 2.2, it can be deduced that the range of electromagnetic spectrum that could be utilized for the photo-excitation process falls between 170 nm to 1000 nm. The range could be classified into different sub-bands of the electromagnetic spectrum i.e. vacuum UV, visible light (760-380 nm/ 1.63-3.26 eV), UVA (400-315 nm/ 3.10-3.94 eV), UVB (315-280 nm / 3.94-4.43 eV), and UVC (280-100 nm/ 4.43-12.4 eV). (Oppenländer 2003).



**Figure 2.2** Energy level diagrams of various semiconductor materials with selected redox potential. The energy scales is referenced against vacuum and the normal hydrogen electrode (NHE) (taken from Choi et al.(2006a)).

Among the chalcogenides (metal oxide/selenide/sulfide) semiconductor, CdS, TiO<sub>2</sub> and ZnO have been found to exhibit high photocatalytic activity (Hoffmann et al. 1995, Klavarioti et al. 2009, Thiruvengkatachari et al. 2008) . However, not all semiconductor materials are suitable to be used as photocatalyst. ZnO and CdS have a low solubility in the

aqueous media. ZnO in the aqueous system would produce  $\text{Zn(OH)}_2$  on the ZnO surface that could inactivate the photocatalyst over a prolonged usage. CdS, similar to the majority of the metal sulfides, undergo the photoanodic corrosion. Furthermore, Cd is a very toxic metal, second only to mercury (Hg).  $\alpha\text{-Fe}_2\text{O}_3$  experiences photocathodic corrosion (Fox and Dulay 1993).

It has been proposed that the band-gap energy of the semiconductor photocatalyst must extend through the redox potential of  $\text{H}_2\text{O}/\bullet\text{OH}$  and  $\text{O}_2/\text{HO}_2\bullet$  couple to allow efficient generation of the reactive radicals. Energy level diagram of various semiconductor materials is shown in Fig 2.2. As can be observed from Fig. 2.2, not all semiconductor materials satisfy the band-gap span requirement (e.g.  $\text{Fe}_2\text{O}_3$ ,  $\text{SnO}_2$ , rutile  $\text{TiO}_2$ , and  $\text{WO}_3$ ).

$\text{TiO}_2$  has received much attention as an ideal photocatalyst due to its high oxidation potential of VB holes ( $E_{\text{vb}} = + 2.7 \text{ V}_{\text{NHE}}$  at pH 7) (Choi 2006b). Besides,  $\text{TiO}_2$  possesses high surface activity, good biocompatibility, high chemical stability, high photo-stability, low cost, and low toxicity (Chen et al. 2009, Habibi et al. 2007a, Thiruvengkatachari et al. 2008). The first attempt of using  $\text{TiO}_2$  for the PCD application was by Frank and Bard for the decomposition of cyanide and sulfite (Frank and Bard 1977b, a). Since then,  $\text{TiO}_2$  photocatalyst has been used extensively in many environmental applications.

Types of pollutants which could be effectively mineralized in the  $\text{TiO}_2$  photocatalysis system are aliphatic compounds, aromatic compounds, detergents, dyes, polymers, pharmaceuticals, pesticides, and herbicides (Byrappa et al. 2000, Haque et al. 2006, Haque and Muneer 2007, Horikoshi et al. 2001, Lim et al. 2011, Molinari et al. 2006, Vinod and Anirudhan 2002). Table 2.3 summarizes different characterization techniques that can be used to monitor the extent of PCD reaction of various types of pollutants. These techniques

can be combined with total organic carbon (TOC) measurement to determine the overall extent of mineralization of organic pollutants.

The PCD reaction can happen only if the molecules of target pollutant are adsorbed to the surface of the photocatalyst. The adsorption of the pollutant to the photocatalyst can be modeled by the Langmuir adsorption isotherm (Langmuir 1932) as follow:

$$\theta = \frac{K_{ads} C_{eq}}{1 + K_{ads} C_{eq}} \quad (2.18)$$

The adsorbed target pollutant would then be degraded following the Langmuir-Hinshelwood (L-H) model (Houas et al. 2001, Xu and Langford 2001) as follow:

$$r = k\theta = k \left( \frac{K_{ads} C_{eq}}{1 + K_{ads} C_{eq}} \right) \quad (2.19)$$

where  $\theta$  = the fraction coverage of the photocatalyst surface by pollutant,  $C_{eq}$  = the concentration of the pollutant at equilibrium,  $K_{ads}$  = Langmuir adsorption constant, and  $k$  = reaction rate constant.

**Table 2.3** Characterization tools for the determination of the extent of TiO<sub>2</sub>-assisted PCD reaction

<b>Techniques / instruments</b>	<b>Type of molecules/target pollutants/intermediates studied</b>	<b>Selected references</b>
Chemical Oxygen Demand (COD)	Organic compounds	(Ghanem et al. 2014, Giri and Golder 2014, Wu et al. 1998, Yuan et al. 2014)
UV-visible spectrophotometry (UV/Vis)	Dyes (e.g. methylene blue, Rhodamine B, methyl orange, etc) and other organic compounds	(Choi et al. 2006b, Goei et al. 2013, Konstantinou and Albanis 2004)


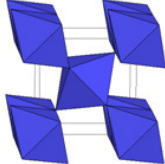

Gas chromatography (GC) / Gas chromatography-mass spectrometry (GC-MS)	Gas-phase pollutants (e.g. acetaldehyde, formaldehyde) and PCD end product (CO <sub>2</sub> )	(Jardim et al. 1997, Konstantinou and Albanis 2003, Sleiman et al. 2009, Stylidi et al. 2004, Zhao et al. 2008)
Gel filtration chromatography (GFC)	Molecular size distribution of NOM or other model pollutants and their intermediates with high MW (between 1 – 50 kDa)	(Amama et al. 2004, Syafei et al. 2008, Yu et al. 2009)
Ultra-filtration membrane fractionation	Molecular size of NOM or other pollutant with high MW (between 1 – 50 kDa)	(Syafei et al. 2008)
High performance liquid chromatography (HPLC)	Organic compounds	(Gao et al. 2010, Hou et al. 2012, Subagio et al. 2010, Zhao et al. 2008)
Specific ultraviolet absorbance (SUVA)	Fraction of unsaturated carbon bonds (degree of aromaticity) in the aromatic organic pollutant	(Abellán et al. 2007, Choo et al. 2008, Huang et al. 2008, Syafei et al. 2008, Yigit and Inan 2009)
Liquid chromatography-mass spectrometry (LC-MS/MS)	Organic compounds and its intermediates.	(Abellán et al. 2007, Antoniou et al. 2008, Calza et al. 2006, Konstantinou and Albanis 2003, Kouloumbos et al. 2003)
Excitation-emission matrix (EEM)	Changes in composition and reactivity of large organic compounds	(Bosco et al. 2006, Li and Sun 2014, Valencia et al. 2013, 2014)

The overall efficiency of the PCD of various organic pollutants was governed not only by inherent properties of the photocatalyst but also by operating parameters of the PCD experiment. The effect of different operating parameters such as light (energy) source, light intensity, photocatalyst dosage, concentration of target pollutants, operating pH, aqueous matrix species and various up-scaling parameters have been discussed in detail elsewhere

(Bhatkhande et al. 2002, 2003, Gaya and Abdullah 2008, Konstantinou and Albanis 2004, Sin et al. 2012).

### 2.2.2 TiO<sub>2</sub>: structures, properties and syntheses.

TiO<sub>2</sub> exist either in its natural polymorphs (i.e. anatase, brookite, or rutile) or in its artificial polymorphs (i.e. TiO<sub>2</sub>(B), TiO<sub>2</sub>(H), TiO<sub>2</sub>(R), etc) (Herrmann 1999). The properties of three different naturally-occurred TiO<sub>2</sub> polymorphs are summarized in Fig. 2.3.

Anatase	Rutile	Brookite
 <p><b>Tetragonal</b>  <b>Unit Cell:</b>  <math>a = 3.7842 \text{ \AA}</math>  <math>b = 3.7842 \text{ \AA}</math>  <math>c = 9.5146 \text{ \AA}</math></p>	 <p><b>Tetragonal</b>  <b>Unit Cell:</b>  <math>a = 4.5845 \text{ \AA}</math>  <math>b = 4.5845 \text{ \AA}</math>  <math>c = 2.9533 \text{ \AA}</math></p>	 <p><b>Orthorhombic</b>  <b>Unit Cell:</b>  <math>a = 9.184 \text{ \AA}</math>  <math>b = 5.447 \text{ \AA}</math>  <math>c = 5.145 \text{ \AA}</math></p>
<b>Z:</b> 4	<b>Z:</b> 2	<b>Z:</b> 8
<b>Point Group:</b> 4/mmm	<b>Point Group:</b> 4/mmm	<b>Point Group:</b> mmm
<b>Space Group:</b> I4 <sub>1</sub> /amd	<b>Space Group:</b> P4 <sub>2</sub> /mmm	<b>Space Group:</b> Pbca
<b>Density:</b> 3.895 g cm <sup>-3</sup>	<b>Density:</b> 4.274 g cm <sup>-3</sup>	<b>Density:</b> 4.123 g cm <sup>-3</sup>
<b>Molar Vol.:</b> 20.156 cm <sup>3</sup>	<b>Molar Vol.:</b> 18.693 cm <sup>3</sup>	<b>Molar Vol.:</b> 19.377 cm <sup>3</sup>
<b>E<sub>g</sub>:</b> 3.05 eV at pH 7	<b>E<sub>g</sub>:</b> 2.98 eV at pH 7	<b>E<sub>g</sub>:</b> 3.26 eV at pH 7
<b>d<sub>Ti-Ti</sub>:</b> 3.04 - 3.79 Å	<b>d<sub>Ti-Ti</sub>:</b> 2.96 - 3.57 Å	<b>d<sub>Ti-Ti</sub>:</b> 2.05 - 3.06 Å
<b>d<sub>Ti-O</sub>:</b> 1.93 - 1.98 Å	<b>d<sub>Ti-O</sub>:</b> 1.95 - 1.98 Å	<b>d<sub>Ti-O</sub>:</b> 1.87 - 2.04 Å
<b>d<sub>O-O</sub>:</b> 2.43 Å	<b>d<sub>O-O</sub>:</b> 2.43 Å	<b>d<sub>O-O</sub>:</b> 2.49 Å
<b>ΔG<sub>f</sub><sup>o</sup>:</b> -211.4 kcal mol <sup>-1</sup>	<b>ΔG<sub>f</sub><sup>o</sup>:</b> -212.6 kcal mol <sup>-1</sup>	<b>ΔG<sub>f</sub><sup>o</sup>:</b> -196.6 kcal mol <sup>-1</sup>

**Figure 2.3** Properties of different naturally-occurred TiO<sub>2</sub> polymorphs (summarized from Linsebigler et al. (1995), Di Paola et al. (2009), Park et al. (2009), and Smyth (2009)).

Anatase and rutile polymorphs of TiO<sub>2</sub> exist in the tetragonal structure, while brookite and TiO<sub>2</sub> (B) exist in the orthorhombic structure. The atoms in the anatase, brookite and rutile

were in the  $[\text{TiO}_2^{6-}]$  intrinsic octahedral arrangement (Fig. 2.3). The Ti-Ti distance in the anatase is wider than those in the  $[\text{TiO}_2^{6-}]$  octahedral arrangement of rutile. The number of neighboring octahedrons that are in contact with the octahedral structure of anatase and rutile are 8 (4 sharing a corner and 4 sharing an edge) and 10 (8 sharing a corner and 2 sharing an edge) respectively. This would lead to a denser rutile structure. The dense structure of rutile is able to withstand a high temperature and pressure up to 60 kBar (Jamieson and Olinger 1968, Navrotsky et al. 1967).

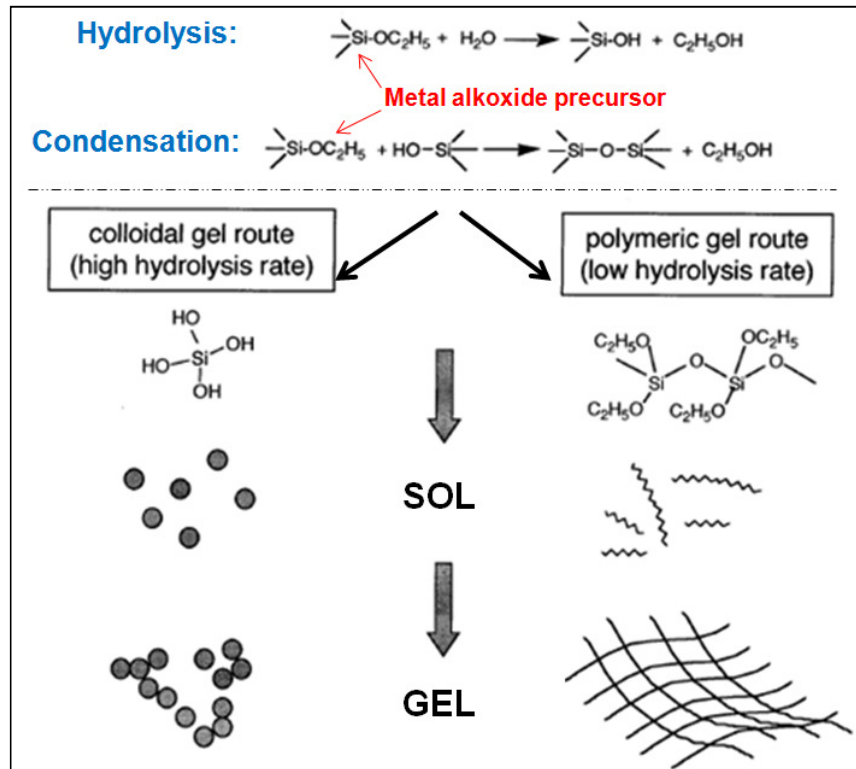
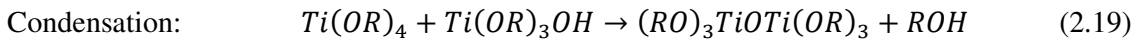
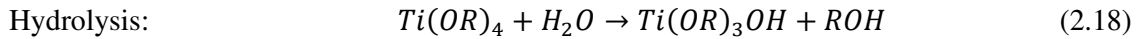
Although anatase is thermodynamically less stable than rutile, the formation of anatase is much favored at lower temperature ( $< 600^\circ\text{C}$ ) (Herrmann 1999). The formation of  $\text{TiO}_2$  crystals at a lower temperature would yield  $\text{TiO}_2$  with a higher surface area and hence, a higher surface density of the active sites for effective adsorption and photocatalytic degradation reaction. Therefore, anatase was found to be the most photocatalytically active polymorph of  $\text{TiO}_2$  (Gaya and Abdullah 2008, Schindler and Kunst 1990, Tanaka et al. 1993a). The high photocatalytic activity of anatase could be ascribed to its triangular atomic arrangement that allowed effective adsorption of pollutants (Di Valentin et al. 2007). Both anatase and brookite polymorph would be transformed to the rutile structure when subjected to a higher temperature (Linsebigler et al. 1995). The detailed review on the anatase to rutile transformation has been published elsewhere (Hanaor and Sorrell 2011). The differences in the electronic and optical responses of different  $\text{TiO}_2$  polymorphs are discussed in detail elsewhere (Landmann et al. 2012).  $\text{TiO}_2$  showed an amphoteric characteristic (i.e. its surface charge are pH dependent). The iso-electric point of  $\text{TiO}_2$  is in between pH 5 and 7. At acidic condition (pH  $< 5$ ), the surface charge of  $\text{TiO}_2$  will be positive ( $\equiv\text{Ti-OH}_2^+$ ); while in the alkaline condition (pH  $> 7$ ), the surface charge will turn negative ( $\equiv\text{Ti-OH}^-$ ) (Choi 2006a).

Surface defects of the TiO<sub>2</sub> crystals also play a critical role in the adsorption of reactive adsorbates (Nash 2008). For example, the presence of oxygen vacancy in the TiO<sub>2</sub> surface would allow the non-dissociative adsorption of O<sub>2</sub> molecules generating a superoxide radical upon reaction with the photogenerated electron. This phenomenon coupled with the high electron transfer rates from TiO<sub>2</sub> to the adsorbed molecule is responsible for the high photocatalytic activity of TiO<sub>2</sub>.

TiO<sub>2</sub> could be prepared in different shapes and morphologies such as nanocrystals/nanodots, nanowires/nanorods (when TiO<sub>2</sub> was synthesized with templating agent), nanosheets, or nanofilms. Nano-sized TiO<sub>2</sub> demonstrates unique optical, electronic, mechanical, thermal, and structural properties which are size-, shape-, and microstructure-dependent. Different techniques to prepare TiO<sub>2</sub> are aerogel method, chemical vapor deposition, direct oxidation method, electro-deposition, hydrothermal method, microwave irradiation method, micelles/inverse-micelles method, physical vapor deposition, sol method, sol-gel method, solvothermal method, and sonochemical method (Chen and Mao 2007).

Sol-gel technique has notable advantages such as high purity, good homogeneity of the film microstructure, low temperature synthesis, controlled reaction condition, low-cost and simple technology, low processing temperature for film densification, controllable properties and versatility for coating on large surface area (Chen et al. 2009, Răileanu et al. 2009, Sharma et al. 2009). Besides, sol-gel method allows a uniform mixing, even at molecular level, of different precursors resulting in a homogeneous multi-components ceramic materials (Vankelecom et al. 2005). Besides TiO<sub>2</sub>, sol-gel method has been used to prepare different types of ceramic materials such as silica (SiO<sub>2</sub>), yttria (Y<sub>2</sub>O<sub>3</sub>), zirconia (ZrO<sub>2</sub>), and many other composite ceramics (Van Gestel et al. 2010).

Sols is a stable dispersion of nanometer-sized colloidal particles in a liquid solution. Drying of the sol at the ambient pressure (thermal evaporation of the liquid) will cause shrinkage in the dispersion producing an intermediate xerogel phase. A final gel will be produced by the complete removal of the water/solvent at a higher temperature. The sol-gel preparation of TiO<sub>2</sub> could be divided into two major reaction steps i.e. hydrolysis and condensation (Eq 2.18 and 2.19).



**Figure 2.4** Colloidal and polymeric route of sol-gel synthesis using metal alkoxide as precursor (modified from Tsuru (2001)).

The formation of TiO<sub>2</sub> using sol-gel method could happen either through the particulate/colloidal sol route or a polymeric sol route (Anderson et al. 1988, Tsuru et al.

2001b). Fig. 2.4 illustrates sol-gel preparation routes. In the particulate sol, the hydrolysis reaction takes place in the condition of high water concentration followed by gelation of the titania network. The fast hydrolysis and condensation reaction would result in the formation of highly branched network. The size of primary colloidal particles is usually in the range of 5-15 nm. In the case of the polymeric sol, hydrolysis reaction occurs in the solvent (i.e. low water content) to form a soluble intermediate product before the condensation reaction to form a linear inorganic polymeric network. Polymeric sol route is preferred for the fabrication of mesoporous TiO<sub>2</sub> thin film due to the formation of smaller size gel network at the end of the synthesis process. This will result in the formation of micropores. It was suggested that the size of individual nanoparticles were to be less than 10 nm for the formation of a well connected microporous structure (De Lange et al. 1995). The hydrolysis rate can also be slowed down by the addition of chelating agent (e.g. acetylacetone) or the selection of precursor with slower hydrolysis rate (Cot et al. 2000, Vankelecom et al. 2005).

Sol-gel technique allows a one-pot synthesis by combining different types of precursors and solvent to yield a desired gel network. Different types of titanium precursors such as titanium alkoxides or non-alkoxide titanium source could be used to prepare the TiO<sub>2</sub> sol (Chen and Mao 2007, Guillén-Santiago et al. 2010, Raut et al. 2009). Different of organic solvents have been incorporated in the preparation of TiO<sub>2</sub> sol including ethanol, benzyl alcohol, butanol, ethylene glycol, 2-propanol, and 1-methoxy-2-propanol (Beyers et al. 2005, Han et al. 2014, Hung et al. 2010, Jiang et al. 2003, Niederberger et al. 2002, Zhong et al. 2005).

The final appearance of titania sol is highly dependent on two parameters: the initial hydrolysis ratio ( $r_w = [\text{H}_2\text{O}] / [\text{Ti}]$ ) and the inhibitor ratio ( $r_a = [\text{H}^+] / [\text{Ti}]$ ). A higher initial hydrolysis ratio  $r_w$  would give rise to a larger particle size and surface area. The  $r_w$  ratio has

to be kept below 2 to avoid early gelation of the sol. pH is an important parameter to control sol-gel process. A low pH is favorable for hydrolysis reaction (Sekulic et al. 2004). An optimum pH value of 2 is required to form a stable sol (Kermanpur et al. 2008). HCl (or other acids) could be incorporated in the sol preparation to control the condensation rate and to prevent fast gelation of the sol (Habibi et al. 2007a, Van Gestel et al. 2002). The final solid gel phase would be obtained upon the completion of polymerization reaction or due to the solvent vaporization.

Acetic-acid catalyzed sol-gel route was employed by Choi and coworkers (2006b) to prepare TiO<sub>2</sub> sol. In this route, the rate of hydrolysis was controlled by the slow release of H<sub>2</sub>O via the esterification reaction between alcohol and acetic acid (Barboux-Doeuff and Sanchez 1994, Sanchez et al. 1988). Chelating agent such as acetylacetone could be added to retard the hydrolysis and condensation reaction (Habibi et al. 2007a, Habibi and Nasr-Esfahani 2007, Habibi et al. 2007b).

The properties of TiO<sub>2</sub> can be elucidated using a wide range of characterization tools. The important characterization techniques employed are summarized in Table 2.4.

**Table 2.4** Characterization tools for TiO<sub>2</sub> materials

<b>Technique / instrument</b>	<b>Characteristic studied</b>	<b>Findings/characteristic peaks</b>
Atomic Force Microscope (AFM)	Surface morphology	The grain appear elongated along the direction of withdrawal of dip coating (Chryscopoulou et al. 1998). TiO <sub>2</sub> appear as uniform and dense spherical grain (Sun et al. 2009). Three important parameters to characterize the morphology of thin film from AFM image are the maximum height ( $R_{max}$ ), the average roughness value ( $R_a$ ) and the root mean square roughness ( $R_{rms}$ ) (Tsoukleris et al. 2007).

N <sub>2</sub> porosimetry analysis	Specific surface area and pore size distribution	Titania film shows good potential for composite membrane fabrication with low hydraulic resistance and effective organic retention (Choi et al. 2006a). N <sub>2</sub> adsorption at low relative pressure ( $P/P_0 < 0.4$ ) is accounted for monolayer adsorption of N <sub>2</sub> on the pore walls. The sharp inflection at $0.4 < P/P_0 < 0.75$ is characteristic of capillary condensation within uniform pores. The sharpness of the step indicates the uniformity of the pore size distribution (Zhao et al. 2005).
Fourier transformed Infra Red Spectroscopy (FTIR)	Chemical bonding	–O–H stretching @ 3450 cm <sup>-1</sup> ; Ti–O–Ti network absorption @ 450-700 cm <sup>-1</sup> ; rutile @ 650 cm <sup>-1</sup> ; 1634, 1638, 2360, 2922 cm <sup>-1</sup> due to stretching and bending of C=C, –C=O, –CH, and –CH <sub>2</sub> respectively (Wang et al. 2008). Ti(O–C) – stretching vibration @ 1100 cm <sup>-1</sup> (Zhang et al. 2006).
Laser Light Scattering / dynamic light scattering	Colloidal diameter, particle size distribution.	Colloidal diameter could be controlled by temperature of aging process (Tsuru et al. 2001b).
Mastersizer	Average particle size	Average size titania nanoparticles cluster on the suspension was found to be 65 nm (Ding et al. 2006).
<sup>1</sup> H / <sup>13</sup> C / <sup>17</sup> ONuclear magnetic resonance (NMR)	Chemical changes of Ti(IV) environment, chemical structure	Selected references (Almeida et al. 2014, Crepaldi et al. 2003, Sun et al. 2014a, Sun et al. 2014b, Wu et al. 1998)
Powder X-Ray Diffraction (XRD) with Rietveld Analysis	Crystal phase and composition	TiO <sub>2</sub> → <i>Anatase</i> [JCPDS 21-1272]: 25.28° (101), 48.05° (200), 37.80° (004), 53.89° (105), 55.06° (211), and 62.69° (204); <i>Brookite</i> [JCPDS 29-1360]: 25.34° (120), 30.81° (121), 25.69° (111), 48.01° (231), 55.23° (241); <i>Rutile</i> [JCPDS 21-1276]: 27.45° (110), 54.32° (211), 36.09° (101), 41.23° (111), 56.64° (220), 69.01° (301). Al <sub>2</sub> O <sub>3</sub> → <i>Corundum</i> [JCPDS 10-0173]: 43.36° (113), 35.13° (104), 57.52° (116), 25.58° (012), 68.19° (300), 52.55° (024), 37.78° (110). Ag → [JCPDS 74-1828]: 38.4° (111),

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		64.2° (220), and 77.4° (311).
Raman Spectroscopy	Structure of composites	<u>Anatase</u> : 143, 196, 395, 513, 519, and 638 cm <sup>-1</sup> ; <u>Rutile</u> : 611 cm <sup>-1</sup> (Bosc et al. 2003, Kment et al. 2010).
Rotary viscosimeter	Suspension viscosity and rheology	Viscosity of titania sol $5.45 \times 10^{-3}$ Pa s = 5.45 cP (Ding et al. 2006)
Scanning Electron Microscopy (SEM) with Energy Dispersive X-Rays (EDX)	Surface morphology and elemental composition	Coating of TiO <sub>2</sub> thin film supported on different ceramic substrate could be observed.
Scanning Tunneling Microscopy (STM)	Surface morphology	The morphology of TiO <sub>2</sub> thin film could be observed by STM.
Transmission Electron Microscopy (TEM)	Film thickness and coating inside the membrane pores	Highly porous titania film with distinct pore structure with mean diameter 3-7 nm was observed (Choi et al. 2006a).
Thermo-gravimetric Analysis (TGA) with differential thermal analysis (DTA)	Thermal stability	Weight loss: (1) < 200°C is due to water evaporation and thermal decomposition of the remnant organic solvent, (2) 200-280°C is due to carbonization / combustion of organic compounds in the composite and (3) > 280°C is due to evaporation of physically absorbed water and further combustion of organic additives (Habibi et al. 2007a).  DTA Analysis: endothermic: removal of water and alcohol. Exothermic: thermo-oxidative degradation of organics, crystallization process (Răileanu et al. 2009).
UV-Vis Diffuse Reflectance Spectrophotometer (UV-DRS)	UV-Vis light absorbance, bandgap and light utilization characteristic	$E_g=3.23$ eV ( $\lambda=385$ nm) for anatase; $E_g=3.34$ eV ( $\lambda=372.5$ nm) for titania catalyst (Choi et al. 2006a). Two main absorption bands at 233 and 304 nm assigned to titanium species in octahedral [TiO <sub>2</sub> <sup>6-</sup> ] environment signified the formation of anatase titania (Zhao et al. 2005).

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X-ray Photoelectron Spectroscopy (XPS)	Elemental surface chemistry	Ti <sup>4+</sup> is confirmed by Ti 2p <sub>3/2</sub> at binding energy of 453-460 eV with Ti 2p <sub>1/2</sub> peak at 458.8 eV (Choi et al. 2006a).
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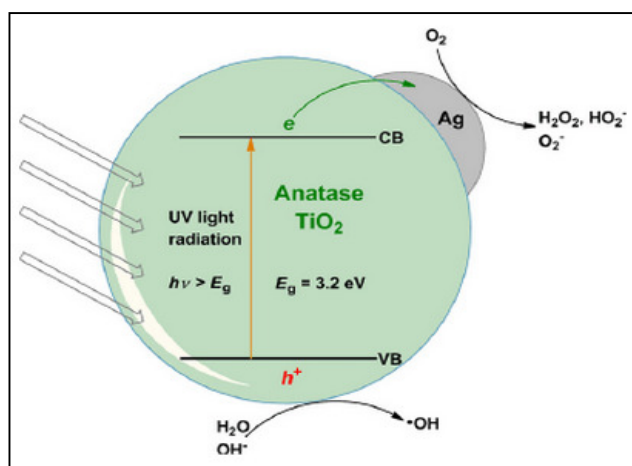
PCD performance of TiO<sub>2</sub> photocatalyst is strongly influenced by the crystal structure, lattice defects, particle size, porosity, overall surface area, and the density of hydroxyl group on the surface of the photocatalysts (Răileanu et al. 2009, Shankar et al. 2004). An optimum TiO<sub>2</sub> crystallite size in the range of 8-10 nm for efficient PCD reaction was postulated (Bosc et al. 2003). The crystallite size (CS) could also be estimated from the BET surface area by assuming spherical crystallite with no or minimal aggregation among the particles (Ivanda et al. 1999). Other method to estimate CS of TiO<sub>2</sub> is by using Scherrer's equation (Scherrer 1918) from the XRD peak broadening of (101) anatase crystal plane at 25.3°.

TiO<sub>2</sub> under UV irradiation displayed photocatalytic disinfection property (Fujishima et al. 2000). Matsunaga and co-workers (1985) was the first to report the anti-bacterial activity of UV-irradiated TiO<sub>2</sub>. Since then, large numbers of research works have been dedicated to study the disinfection capability of TiO<sub>2</sub> photocatalyst. Photocatalytic disinfection capability of TiO<sub>2</sub> has been tested against different types of microorganisms such as bacteria, fungi, algae, protozoa, and virus (Foster et al. 2011, Yao and Lun Yeung 2011). The mechanisms of photocatalytic disinfection capability of TiO<sub>2</sub> are direct oxidation of coenzymes in cells, destruction of cell structure and damaging the cell DNA (Hu et al. 2007, Matsunaga et al. 1985).

## 2.2.3 Improving photocatalytic activity and functionality of TiO<sub>2</sub>

### 2.2.3.1 Metal doped TiO<sub>2</sub>

Attempt to improve the photocatalytic activity of TiO<sub>2</sub> include synthesizing nano-sized TiO<sub>2</sub> in various shapes and morphologies (Joo et al. 2005, Wu 2007), doping with metal (Lahiri et al. 2006, Subramanian et al. 2004) and non-metal, coupling with other semiconductor materials, surface modification, etc. Different metals (e.g. Ag, Al, Au, Ce, Co, Cr, Cu, Fe, Mn, Nb, Ni, Pd, Pt, V, W), lanthanides (e.g. Ce, Eu, Nd, La) and non-metal (e.g. B, C, F, N, S) have been used as the dopant materials. Various co-doped TiO<sub>2</sub> have also been reported (Wang and Lim 2010, Wang et al. 2011a, Wang et al. 2011b).



**Figure 2.5** Metal-semiconductor (Ag-TiO<sub>2</sub>) complexes that would prolong the life-time of photogenerated  $e^-$  and  $h^+$  pairs (taken from Zhao and Chen (2011)).

The formation of metal cluster and semiconductor complex (Fig. 2.5) has been reported to enhance the PCD reaction efficiency by trapping the photo-generated charge carriers and improving overall charge transfer process (Subramanian et al. 2001). The dopant creates an additional intermediate energy level that prolongs the lifetime of the photogenerated  $e^-$ - $h^+$  pairs by acting as an electron traps. They also might introduce oxygen vacancies that would

improve the number of active sites thus improving overall PCD efficiency. Among the metallic materials, Ag provides the highest Schottky barrier which is important for effective inhibition of  $e^-h^+$  pairs recombination (Nasr-Esfahani and Habibi 2008). Ag-doping also allowed the PCD reaction to be carried out under visible light ( $\lambda > 400$  nm) irradiation. Besides, Ag is preferred as the metal dopant due to its excellent anti-bacterial properties that could reduce biofouling in the membrane separation process (Liu et al. 2013b, Yin et al. 2013).

Kubacka et al. (2008) have combined Ag and  $TiO_2$  via impregnation and photodeposition method. They found that combining Ag and  $TiO_2$  by photodeposition method displayed higher anti-bacteria performance over the impregnated Ag- $TiO_2$  composite. Photodeposition of Ag nanoparticles improved the PCD performance of  $TiO_2$  coating (Arabatzis et al. 2003). In other study, Ag-modified P25 coating displayed an improved PCD performance of o-cresol over the Ag-less coating (Liu et al. 2004). The incorporation of photoreduced Ag on mesoporous anatase has significantly enhanced the anti-bacterial activity (Liu et al. 2008).

The incorporation of Ag into the  $TiO_2$  matrix by direct photoreduction process has some disadvantages because of its poor adhesion, inability to yield uniform Ag nanoparticles distribution and the length of time required for effective photoreduction (Hou et al. 2009). A modified sol-gel method has been used instead to incorporate  $Ag^+$  in the preparation of  $TiO_2$ .  $Ag^+$  would be deposited on the surface of  $TiO_2$  during calcination while the remaining  $Ag^+$  would diffuse into the  $TiO_2$  lattice. The diffused  $Ag^+$  could be photoreduced during the post treatment.  $Ag^+$  ion could also be reduced to  $Ag^0$  during the calcination due to the high redox potential of Ag (Ao et al. 2008). Deposited Ag nanoparticles were found to agglomerate near the surface of the Ag- $TiO_2$  composite due to its high surface energy (Chao et al. 2003).

The need of anti-bacterial actions of Ag was aggravated by the evolution of new bacteria strains that are resistant to antibiotic (Kyriacou et al. 2004). The anti-bacterial properties of Ag-TiO<sub>2</sub> composite is mainly contributed by Ag<sup>+</sup> ions dissolving from the surface of Ag (Feng et al. 2000). Dissolved Ag<sup>+</sup> can be adsorbed onto the surface of the bacteria cells and damage the cell membrane and solid structures of its protein. Ag<sup>+</sup> can also permeate into bacteria cells, interacting with various enzymes within the cells and may interfere with the DNA (Feng et al. 2000, Li et al. 2008) .

The main drawback of the application of Ag as an anti-bacterial agent in the water-related application is the high rate of Ag<sup>+</sup> release. High Ag<sup>+</sup> release rate would shorten the lifespan of anti-bacterial activity (Wang et al. 1998). Besides, the stringent potable water standards have prescribed a maximum level of Ag in potable water supply as 100 µg L<sup>-1</sup> (USEPA 2009, WHO 2011). Therefore, the need to immobilize Ag nanoparticles in the mesoporous support matrix is imminent in order to delay the release of Ag<sup>+</sup>. The supported Ag composite could prolong the duration of anti-bacterial activity which would lower the overall treatment cost (Akhavan and Ghaderi 2010, Zhang et al. 2004).

### **2.2.3.2 Structure directing agent (SDA)-modified TiO<sub>2</sub>**

Ordered mesoporous TiO<sub>2</sub> can be prepared using a process known as evaporation-induced self-assembly. In this process, an SDA is added during the preparation of the TiO<sub>2</sub> sol. The SDA assembles to form a micellar structure that can be removed during calcination steps, leaving behind an ordered mesoporous TiO<sub>2</sub> structure. The addition of SDA in the sol preparation allows fine-tuning the porosity and porous structure of the resulting TiO<sub>2</sub>. Besides, the addition of SDA would increase the overall specific surface area of the TiO<sub>2</sub>. The increase of specific surface area of the TiO<sub>2</sub> would promote better adsorption of

pollutants onto photocatalyst resulting in higher overall PCD rate. Different types of SDAs that could be used to assist the pore formation are classified into block copolymers and cationic, anionic and nonionic surfactants. Table 2.5 summarizes common types of SDAs that have been used in the preparation of TiO<sub>2</sub>.

**Table 2.5** Common types of SDA used in the preparation of mesoporous TiO<sub>2</sub>

<b>Class</b>	<b>Examples (Scientific/Trade)</b>	<b>Selected references</b>
<b>Polymer</b>	Polyethylene glycol (PEG)	(Arconada et al. 2009, Chen and Dionysiou 2007, Jahromi et al. 2009)
<b>Di-block copolymer</b>	Poly(ethylene-co-butylene)-block-poly(ethylene oxide) / KLE	(Coquil et al. 2010, Fattakhova-Rohlfing et al. 2007, Ortel et al. 2012a)
	Poly(ethylene oxide)-block-polybutadiene-block-poly(ethylene oxide)/ PEO-PB-PEO	(Ortel et al. 2012b)
	Polystyrene-block-polybutadiene-block-polystyrene/ SBS	(Zakaria et al. 2013)
<b>Tri-block copolymer</b>	Poly(ethylene oxide)-block-poly(propylene oxide)-block-poly(ethylene oxide)/ Pluronic P-123	(Goei et al. 2013, Liu et al. 2009, Procházka et al. 2008, Sun et al. 2009, Wu and Rankin 2011)
	Poly(ethylene oxide)-block-poly(propylene oxide)-block-poly(ethylene oxide)/ Pluronic F-127	(Castro and Durán 2013, Rahimi et al. 2013, Wang et al. 2013)

<b>Cationic surfactant</b>	Cetyl trimethyl-ammonium bromide/ CTAB	(Lee et al. 2013, Rashad and Shalan 2013, Shao et al. 2013)
	Poly(ethyleneimine)/ PEI	(Chang and Hsiang 2010)
<b>Anionic surfactant</b>	Sodium dodecyl sulfate/ SDS	(Rashad and Shalan 2013)
<b>Nonionic surfactant</b>	Polyethylene glycol p-(1,1,3,3-tetramethylbutyl)-phenyl ether/ Triton X-100	(Li et al. 2011, Sanguanruang et al. 2011, Xu et al. 2013)
	Polyoxyethylene (20) sorbitan monolaurate/ Tween 20	(Chen and Dionysiou 2008, García-Benjume et al. 2009)
	Polyoxyethylene (20) sorbitan monooleate / Tween 80	(Choi et al. 2006c, Choi et al. 2006d, Han et al. 2011)
	Poly(ethylene glycol) hexadecyl ether/ Brij58	(Arconada et al. 2010, Castro and Durán 2013)

The usage of copolymer as SDA in the past has been limited due to the low thermal stability of the polymer, resulting in the amorphous TiO<sub>2</sub> at a low calcination temperature or TiO<sub>2</sub> with smaller surface area and pore volume due to the collapse of the SDA scaffolding at a higher calcination temperature (Shamaila et al. 2011). The possibility of the high temperature calcination while maintaining a high-porosity TiO<sub>2</sub> was demonstrated by Lee et al. (2008) using a mixture of soft and hard templates as the SDA. The materials were able to withstand a calcination temperature of 1000°C while maintaining a high porosity. Zhang and coworkers (2010) carbonized the copolymer template using H<sub>2</sub>SO<sub>4</sub> to yield amorphous carbon inside the mesoporous structure of TiO<sub>2</sub> that has strengthened TiO<sub>2</sub> framework during calcination. Other efforts were noted to improve the thermal stability of the template (Yoshitake et al. 2002).

Among different types of SDAs, a non-ionic SDA was generally preferred due to the weaker interactions between the SDA and the TiO<sub>2</sub> scaffold allowing easy removal of the SDA during calcination step. Besides, the use of non-ionic SDA would increase the structural stability of the meso-structure (Habibi et al. 2007a, Habibi and Nasr-Esfahani 2007, Habibi et al. 2007b). Generally, the increase in the SDA chain length would result in a structure with a larger porosity. The increase in the SDA concentration has the similar effect as the increase in the SDA chain length (Choi et al. 2006b, Zhang et al. 2003a). Zhang and coworkers (2003b) studied the effect of the molecular weight of polyethylene glycol (PEG) and the molar ratio of the SDA to the Ti content on the performances of the resulting TiO<sub>2</sub> photocatalytic film. The capping effect of SDA on the titanium precursor was found to reduce the hydrolysis and condensation reaction during the sol-gel synthesis (Dag et al. 2003, Stathatos et al. 2004).

During the preparation of the sol, the hydrated head group of the SDA (e.g. poly(ethylene oxide) of P-123 copolymer) interacts directly with the metal alkoxide precursor. This interaction promote the formation of a micellar structure even at a concentration lower than the critical micelle concentration (Wu and Rankin 2011). The resulting pore diameter is relatively uniform while the wall thickness of the resulting microstructure is solely dependent on the overall concentration of SDA in the sol (thicker wall for lower concentration of SDA).

### **2.3 TiO<sub>2</sub>-based hybrid photocatalytic ceramic membrane**

The integration of TiO<sub>2</sub> heterogeneous photocatalysis and membrane separation process in a hybrid treatment system is advocated in order to achieve effective water treatment solution. The integration could be achieved either using a separated membrane reactor with photoreactor in tandem as well as an integrated membrane photoreactor (Lim et al. 2011). In each case, TiO<sub>2</sub> photocatalyst could be either used in a suspension or in an immobilized

system. The former requires catalyst recovery after the photocatalytic treatment process. The latter suffers from mass transfer limitation and has a much smaller number of active sites compared to the former.

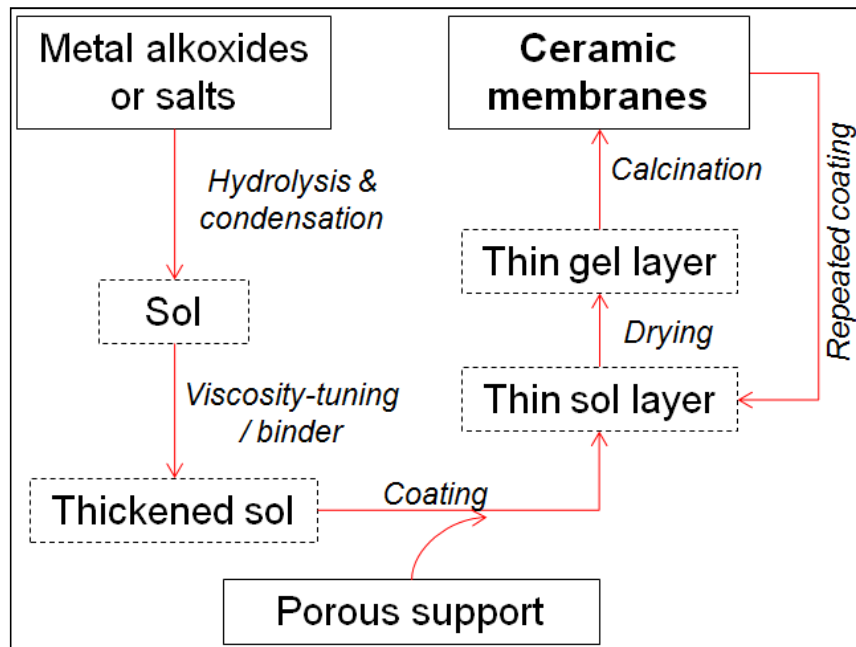
The usage of suspended  $\text{TiO}_2$  nanoparticles in a tandem photocatalyst-membrane reactor treatment system has been limited due to possible particles aggregation, possible membrane fouling and the need of particle recovery at the end of the treatment process (Linsebigler et al. 1995, Zhang et al. 1998). By anchoring the  $\text{TiO}_2$  photocatalyst onto a porous membrane support, the issue of catalyst recovery can be solved. In addition, it also allows the synergistic coupling of photocatalytic reaction and membrane filtration which promotes mass transfer process through forced permeation. In this context, the crystallite size of the anchored  $\text{TiO}_2$  photocatalyst must be optimized in order to achieve a high photocatalytic activity while not incurring a high membrane resistance. In addition, there is a need to produce a thin and uniform layer of nano-sized photocatalyst anchored on the highly porous membrane surface in order to maintain high water permeation through the  $\text{TiO}_2$  membrane.

$\text{TiO}_2$  nanoparticles can be anchored onto different types of supports such as polymeric and ceramic membrane. An attempt to anchor  $\text{TiO}_2$  nanoparticles on different types of flat-sheet polymeric membranes have resulted in partial membrane damage caused by radical attack triggered by UV-irradiation (Molinari et al. 2000). Photostable ceramic membrane has since been used for hybrid photocatalytic membrane application.

The ceramic membrane has many notable advantages such as its good permeability (due to good surface wettability and relatively uniform pore size), chemical stability (able to withstand organic solvents, chlorines, and extreme pH condition), thermal stability, mechanical stability, easy to clean, anti-fouling and anti-microbial property (Anderson et al. 1988, Bhave 1991, Burggraaf and Cot 1996, Chang et al. 1994, Guizard et al. 1992). Besides,

membrane process using ceramic membrane is cheaper over a long term application despite its high membrane cost compared to the polymeric membrane system. A comprehensive economic assessment of membrane process for water and wastewater treatment has been published elsewhere (Owen et al. 1995).

Ceramic membrane for water and wastewater treatment normally consists of an asymmetric structure coated on a macroporous support. The support provides a mechanical strength to the membrane. Among different types of ceramic porous support materials,  $\alpha$ - $\text{Al}_2\text{O}_3$  was commonly chosen due to its high chemical stability in extreme pH condition (Tsuru et al. 2001b).



**Figure 2.6** Flow diagram to prepare micro-/meso-porous ceramic membranes via the sol-gel technique (modified from Hsieh (1996)).

The flow diagram of the typical preparation steps of micro/mesoporous membranes via the sol-gel technique is presented in Fig. 2.6. In the typical preparation, a thickened sol is coated onto the porous support. The asymmetrical structure is obtained through coating of 2 or more layers with different porosities. Usually, more than 1 layer of coating is required for each type of the sol to ensure the smoothness and uniformity of the coating. A mesoporous intermediate layer is coated prior to the microporous top layer to reduce the surface roughness. This will result in a multi-layered ceramic membrane with a hierarchically porous architecture. The presence of porosity gradient is important to prevent early clogging of the composite membrane during the treatment process.

Leenaars and coworkers were the first to prepare an alumina ceramic membrane with ultrafine pores of diameter 3-5 nm by controlling the condition during sol-gel synthesis and the subsequent heat treatment (Keizer et al. 1984, Leenaars et al. 1984, Leenaars and Burggraaf 1985). Hashizume and Kunitake (2003) prepared a self-supporting ultrathin titania film by spin coating. They used different types and concentrations of spin-coating solutions to achieve a titania thin film with a controllable thickness. Meulenberg and coworkers (2006) produced a hybrid membrane with porosity gradient combining a stainless steel substrate, screen-printed ceramic layer, and a thick photoactive TiO<sub>2</sub> layer.

Coating of TiO<sub>2</sub> photocatalytic layers is an important step in the fabrication of the hybrid membrane. Delamination of TiO<sub>2</sub> layer from the support layer is to be avoided. Different coating techniques have been used to prepare and coat the TiO<sub>2</sub> thin film layer on the ceramic membrane support such as dip coating, spin coating (Fretwell and Douglas 2001, Pan and Lee 2006, Wang et al. 2002), slip casting (Alem et al. 2009b, Zaspalis et al. 1992), in-situ hydrothermal/solvothermal synthesis (Shen et al. 2014, Zhan et al. 2013), aerosol spraying (Cho and Yoon 2013, Kavan and Grätzel 1995, Kubo et al. 2013), chemical vapor deposition

(Diesen et al. 2013, Mills et al. 2002), physical vapor deposition (Moser et al. 2013, Weng and Huang 2013), radio-frequency magnetron sputtering (Dholam et al. 2008), spray pyrolysis (Ennaoui et al. 2006, Kavan and Grätzel 1995), reactive sputtering (Awitor et al. 2008), electrochemical deposition (Hepel and Kumarihamy 2007, Palmas et al. 2010), plasma spraying (Znamirovski et al. 2013, Zou et al. 2007), etc.

Different preparation and coating techniques used would result in the TiO<sub>2</sub> thin film of various thicknesses and morphologies. The final microstructure and the performance of the TiO<sub>2</sub> thin film is strongly dependent of the preparation condition. Zhao and coworkers (2004) investigated different preparation conditions that would affect the microstructure of the resulting TiO<sub>2</sub> thin film such as amount of SDA added, amount of the hydrolysis retardants added, aging time, pH, and calcination temperature. Liu and coworkers (2005) optimized the relative amount of the TiO<sub>2</sub> sol constituent to control the porosity of the resulting thin film.

Recurrently, binder such as hydroxypropyl cellulose (HPC) or polyvinyl alcohol (PVA) was added into the TiO<sub>2</sub> sol as a binder (Alem et al. 2009b). Binder could help to adjust the viscosity of the sol, lower the surface tension of the sol and increase the mechanical strength of the resulting membrane (Larbot et al. 1988, Sekulic-Kuzmanovic 2004).

Heat treatment plays an important role in the fabrication of crack-free membrane. A lower calcination temperature would yield membrane with a smaller pore and crystallite size. Also, the lower calcination temperature would prevent transformation of anatase to rutile. By controlling the heating rate during the calcination step, one can avoid the development of thermally induced stress possibly caused by unequal thermal expansion of the composite membrane or layer shrinkage due to thermal decomposition of organic additives. For the multi-layer coating process, the repeated thermal treatments performed after each coating could cause a partial collapse of the porous structure thus reducing its PCD efficiency

(Arconada et al. 2010). It was suggested that the calcination temperature is the ultimate control porosity structure of the resulting membrane (Puhlfürß et al. 2000).

It is important to ensure that the surface of the composite membrane is hydrophilic to allow easy access of the target organic pollutant to the catalytic sites (Hata et al. 2000). Surface of the TiO<sub>2</sub> exhibits photo-induced super-hydrophilicity (PSH) when irradiated with UV source (Irie et al. 2003, Watanabe et al. 1999). According to the Laplace equation, the wettability of porous materials is inversely proportional to the contact energy (surface energy) of the materials (Mulder 1996).

Table 2.6 summarizes different characterization techniques that can be used to study various characteristics of ceramic membrane composite.

**Table 2.6** Characterization of ceramic membranes

<b>Technique / instrument</b>	<b>Characteristic studied</b>	<b>Findings</b>
Gas bubble pressure (GBP) method (ASTM F316-80)	Mean pore size and pore size distribution	Pore size decreases or can be plugged as the deposition of TiO <sub>2</sub> increases (Ha et al. 1996).
ASTM F316	Pore size characteristic	Permeability of the TiO <sub>2</sub> composite membrane was evaluated (Alem et al. 2009b).
Nano-permporometry (humid gas permeation)	Pore size and pore size distribution	Nano-order pore size of silica-zirconia membrane is evaluated (Tsuru et al. 2001a).
Pencil hardness testing (ASTM D3363-92a) / Tensile testing (ASTM C633-01) / Scratch adhesion testing	Mechanical properties / coating strength	Pencil hardness testing is more suitable for porous film; porous film shows fair adhesion strength but relatively weak mechanical properties as compared to dense membrane (Ryu et al. 2010).
Static angle goniometer	Hydrophilicity /	Hydrophilic membrane is compatible with

	hydrophobicity	polar pollutant.
Spectral ellipsometry and environmental ellipsometric porosimetry	Thickness and porosity of the coating	Different information of TiO <sub>2</sub> film could be obtained via ellipsometry (Boissiere et al. 2005).
Three-points bend test	Mechanical strength	The mechanical strength of the composite membrane was reinforced by the alumina support (Alem et al. 2009b).
Water absorption method (ASTM C373-88)	Apparent porosity and bulk density	Apparent porosity of TiO <sub>2</sub> composite membrane was evaluated. Result was complimentary to BET porosimetry analysis (Alem et al. 2009b).
Zeta potential analyzer	Electrical potential difference (streaming potential)	Zeta potential depends of types of the electrolyte; titania shows amphoteric properties with isoelectric point of 6.5 (Tsuru et al. 2001b).

Table 2.7 summarizes selected works on the TiO<sub>2</sub>-based thin films and photocatalytic ceramic membranes. Majority of works listed on Table 2.7 mainly deal with TiO<sub>2</sub>-based thin films or TiO<sub>2</sub>-based membranes used to treat various types of pollutants in a batch photoreactor. In the batch reactor, the efficacy of supported-TiO<sub>2</sub> photocatalyst is limited to the mass-transfer limitation of the pollutants to the surface of the photocatalysts. A continuous flow treatment system can be achieved by coating TiO<sub>2</sub> onto a porous membrane support. The overall improvement on direct contact between target pollutants and photocatalysts due to the forced permeation through the membrane will result in an enhanced photocatalytic degradation efficiency of the treatment system.

The anti-bacterial application of traditional ceramic membrane treatment process was limited to the molecular sieve functionality. It does not inactivate bacteria cells. Bacteria cells

deposited on the membrane surface can grow into structured community known as bio-film which is more difficult to remove than individual bacteria cells in suspension (Costerton et al. 1999). The inclusions of Ag nanoparticles (Ag NPs) into TiO<sub>2</sub> photocatalytic ceramic membrane could enhance the anti-bacterial property and inhibit the growth of bio-film. Table 2.8 summarizes selected works on Ag-decorated TiO<sub>2</sub>-based thin films and photocatalytic ceramic membranes.

**Table 2.7** TiO<sub>2</sub>-based thin film and photocatalytic ceramic membrane: preparation, properties and performances

References	Synthesis / fabrication highlights	Important physico-chemical properties	Photocatalytic and membrane performances
(Anderson et al. 1988)	<ul style="list-style-type: none"> <li>Two types of membrane were prepared: from particulate sols and polymeric sols.</li> </ul>	<ul style="list-style-type: none"> <li>The size of the particles in the particulate sols is strongly dependent on the pH condition (early precipitation and possible particle aggregation occurred respectively at low and high pH condition).</li> <li>For the polymeric sols, a transparent gel could only be obtained when <math>[H_2O]/[Ti] \leq 4</math>, acid do not significantly affect the properties of the polymeric gels.</li> </ul>	<ul style="list-style-type: none"> <li>The membrane pores whose diameter are in the 1.8 – 5.0 nm range.</li> </ul>
(Zhao et al. 2004, Zhao et al. 2005)	<ul style="list-style-type: none"> <li>TiO<sub>2</sub> mesoporous thin film was prepared using P-123 as the SDA.</li> <li>TiO<sub>2</sub> sol was dip-coated on glass slides and/or silicon wafer.</li> </ul>	<ul style="list-style-type: none"> <li>Optimum molar concentration of SDA was found to be 0.03 with respect to Ti.</li> <li>Different parameters (i.e. amount of SDA, aging time, pH, aging temperature, and amount of acetylacetone (chelating agent)) were investigated in relation to the properties of the final TiO<sub>2</sub> film.</li> <li>Template removal by solvent extraction</li> </ul>	<ul style="list-style-type: none"> <li>Thin film composite was tested against methylene blue.</li> <li>Ethanol-extracted membranes calcined at 350-400°C have the highest PCD efficiency due to its larger surface area.</li> </ul>

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(Zhang et al. 2006)	<ul style="list-style-type: none"> <li>• TiO<sub>2</sub>/Al<sub>2</sub>O<sub>3</sub> composite membranes were prepared from colloidal titania sols.</li> </ul>	<p>followed by calcination improved the overall structural stability of the TiO<sub>2</sub> scaffold.</p> <ul style="list-style-type: none"> <li>• TiO<sub>2</sub> crystallite size (CS) ranged between 5 and 30 nm for solvent-extracted samples.</li> <li>• Uniform pore size around 50-100 nm.</li> <li>• The dissolution of TiO<sub>2</sub> microstructure was observed after 6 times usage resulting in membrane with larger pore size.</li> <li>• Membrane consists of TiO<sub>2</sub> tubules with average thickness of 50 μm.</li> </ul>	<ul style="list-style-type: none"> <li>• Different retention rates were observed for model pollutant Direct Black168 when treated at different pH.</li> <li>• Immediate decline in flux was observed followed by a stable sustainable flux for the rest duration of the experimental run.</li> <li>• The presence of H<sub>2</sub>O<sub>2</sub> accelerates the PCD reaction of organic pollutant.</li> </ul>
(Choi et al. 2006b)	<ul style="list-style-type: none"> <li>• TiO<sub>2</sub> sol was prepared using acetic-acid based sol-gel route with non-ionic surfactant as SDA.</li> <li>• TiO<sub>2</sub> sol was dip-coated on borosilicate glass.</li> <li>• Among the non-ionic SDAs, Tween-80</li> </ul>	<ul style="list-style-type: none"> <li>• TiO<sub>2</sub> CS range between 8.3 and 15.6 nm.</li> <li>• Slow hydrolysis reaction enhanced the structure of the resulting TiO<sub>2</sub>.</li> <li>• Capping effect from the SDA reduce the hydrolysis and condensation reaction rate.</li> </ul>	<ul style="list-style-type: none"> <li>• Higher removal of methylene blue (MB) for higher loading of SDA up to 2.0 molar ratios (with respect to TiO<sub>2</sub>), above which the PCD efficiency was reversed.</li> </ul>

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	showed the best pore structure and film thickness controllability.		
(Habibi et al. 2007a, Habibi and Nasr-Esfahani 2007, Habibi et al. 2007b)	<ul style="list-style-type: none"> <li>• TiO<sub>2</sub> thin film composite was prepared by sol-gel method utilizing methylcellulose (MC, a non-ionic polymer) as the SDA.</li> <li>• TiO<sub>2</sub> sol was spin-coated onto borosilicate glass.</li> </ul>	<ul style="list-style-type: none"> <li>• The addition of MC improved the stability of the TiO<sub>2</sub> sol and the resulting coating quality.</li> <li>• The addition of MC improved the adhesion of the TiO<sub>2</sub> layer to the support.</li> <li>• TiO<sub>2</sub> CS of the composite film was 16.3 nm</li> </ul>	<ul style="list-style-type: none"> <li>• Thin film composite was tested against 3 types of diazo dyes.</li> <li>• First order kinetic of PCD of C.I. Reactive Yellow 2 dye was observed.</li> <li>• More efficient PCD was observed for thin film composite prepared with MC.</li> <li>• Photodecoloration was much faster than the photomineralization (which includes aromatic ring opening reaction).</li> </ul>
(Zhao et al. 2008)	<ul style="list-style-type: none"> <li>• A micro-nano hierarchical TiO<sub>2</sub> film was fabricated with Si-coated borosilicate glass as support.</li> <li>• Electro-hydrodynamic (EHD) coating technique (Zhao et al. 2006).</li> <li>• For comparison, nano-structured TiO<sub>2</sub> thin film was also prepared by spin coating.</li> </ul>	<ul style="list-style-type: none"> <li>• TiO<sub>2</sub> layer consist of array of TiO<sub>2</sub> nanoparticles.</li> <li>• TiO<sub>2</sub> loading of 12 ± 1 mg.</li> <li>• Pore size &lt; 100 nm.</li> <li>• Thickness of the hierarchically porous and nanoporous TiO<sub>2</sub> thin films were 2 and 1.5 μm respectively.</li> </ul>	<ul style="list-style-type: none"> <li>• PCD capability of the thin film was evaluated against liquid phenol and gaseous acetaldehyde.</li> <li>• Hierarchical porous thin film showed a better PCD performance (especially in treating phenol).</li> </ul>
(Syafei et al.	<ul style="list-style-type: none"> <li>• Commercial Degussa P25 suspended in</li> </ul>	<ul style="list-style-type: none"> <li>• Commercial membrane with MWCO 1,</li> </ul>	<ul style="list-style-type: none"> <li>• Higher flux decline for the TiO<sub>2</sub> coated</li> </ul>

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2008)	acetylacetone solution with Triton X-100 as the SDA.	15, and 30 kDa was used.	membrane which could be attributed to the adsorption of organic pollutant.
	<ul style="list-style-type: none"> <li>• Coating by immersing TAMI ATZ (alumina, titania, zirconia) ceramic membrane disk.</li> </ul>		<ul style="list-style-type: none"> <li>• Higher humic acid removal by the TiO<sub>2</sub> coated membrane which mainly was contributed by the membrane rejection.</li> </ul>
(Sun et al. 2009)	<ul style="list-style-type: none"> <li>• Usage of DoE (design of experiment) to find an optimal synthesis condition for maximum photocatalytic activity.</li> <li>• Factors considered: amount of acetic acid added, amount of ethanol added, amount of SDA (P-123) added, and calcination temperature.</li> <li>• TiO<sub>2</sub> film was coated on ITO glass.</li> </ul>	<ul style="list-style-type: none"> <li>• The presence of residual OH groups bonded with Ti was found in the FTIR spectrum of all samples.</li> <li>• TiO<sub>2</sub> CS range between 12.0 and 38.7 nm.</li> <li>• TiO<sub>2</sub> loading range between 33 and 211 μg cm<sup>-2</sup>.</li> <li>• TiO<sub>2</sub> exist as uniform and dense spherical grain.</li> </ul>	<ul style="list-style-type: none"> <li>• Calcination temperature has the most significant influence for the photocatalytic activity of both methyl orange and gaseous toluene.</li> </ul>
(Alem et al. 2009b)	<ul style="list-style-type: none"> <li>• TiO<sub>2</sub>/Al<sub>2</sub>O<sub>3</sub> composite membrane prepared from TiO<sub>2</sub> colloidal sol with HPC and PVA added as binder.</li> <li>• TiO<sub>2</sub> layer was coated using slip casting method.</li> </ul>	<ul style="list-style-type: none"> <li>• Optimum thickness of 1μm for membrane with good integrity.</li> <li>• Composite membrane with large surface area (75 m<sup>2</sup> g<sup>-1</sup>) and small pore size (4.7 nm) was fabricated.</li> </ul>	<ul style="list-style-type: none"> <li>• Membrane showed permeability of 30 mL min<sup>-1</sup> Bar<sup>-1</sup> cm<sup>-2</sup> with Knudsen diffusion observed at low TMP.</li> <li>• Removal of methyl orange in the batch photoreactor was observed despite the issue of mass transfer limitation.</li> </ul>

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(Alem et al. 2009a)	<ul style="list-style-type: none"> <li>• Multilayer TiO<sub>2</sub>/Al<sub>2</sub>O<sub>3</sub> composite membrane prepared using TiO<sub>2</sub> polymeric and TiO<sub>2</sub> colloidal sol as the top and intermediate layer respectively.</li> <li>• Aging to increase the viscosity of the sol and thus minimizing sol infiltration to the underlying layer.</li> </ul>	<ul style="list-style-type: none"> <li>• Composite membrane with improved surface area (83 m<sup>2</sup> g<sup>-1</sup>) and smaller pore size (4 nm) was fabricated.</li> </ul>	<ul style="list-style-type: none"> <li>• Addition of top TiO<sub>2</sub> layer had a minimum impact on the membrane permeability.</li> <li>• Improved PCD of methyl orange in the batch photoreactor due to the presence of top TiO<sub>2</sub> layer prepared from polymeric sol.</li> </ul>
(Arconada et al. 2010)	<ul style="list-style-type: none"> <li>• TiO<sub>2</sub> mesoporous thin film was prepared using different types of SDAs: Pluronic F-127, Brij56/58, CTAB and SDS.</li> <li>• Two types of chelating agents were used: acetylacetone and acetic acid.</li> <li>• TiO<sub>2</sub> was dip-coated to glass and silicon wafer substrate, prior SiO<sub>2</sub> coating was applied to the glass substrate to prevent diffusion of Na<sup>+</sup>.</li> </ul>	<ul style="list-style-type: none"> <li>• All sol displayed an excellent stability (a relatively constant viscosity of 2 mPa.s for more than 1 month).</li> <li>• Coating thickness was varied between 200 and 300 nm. Thickest coating was obtained for TiO<sub>2</sub>-acetic acid-F-127 combination.</li> <li>• Porosity profile of the film was determined using spectral ellipsometry.</li> <li>• Specific surface area range between 28 and 68 m<sup>2</sup> g<sup>-1</sup>.</li> </ul>	<ul style="list-style-type: none"> <li>• The efficacy of PCD reaction is highly dependent of the total surface area effectively irradiated with UV.</li> <li>• There exists an optimum coating thickness above which, the light shielding effect and higher material cost hinder the overall efficacy of the PCD reaction.</li> </ul>

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(Arconada et al. 2011)	<ul style="list-style-type: none"> <li>• TiO<sub>2</sub> mesoporous thin film was prepared using different types of SDAs: F-127, Brij58 and Triton X-100.</li> <li>• TiO<sub>2</sub> was dip-coated to glass in different relative humidity (RH) and withdrawn at different rate.</li> </ul>	<ul style="list-style-type: none"> <li>• TiO<sub>2</sub> CS range between 16 and 19 nm.</li> <li>• Total pore volume range between 30 and 45% with pore size distribution between 2.4 and 6.4 were obtained.</li> </ul>	<ul style="list-style-type: none"> <li>• TiO<sub>2</sub> film prepared with Brij58 at RH 50% displayed highest initial PCD rate while maximum amount of methylethyl ketones was degraded by Brij58, RH 20% TiO<sub>2</sub> film.</li> </ul>
(Wang et al. 2013)	<ul style="list-style-type: none"> <li>• TiO<sub>2</sub> mesoporous thin film was prepared using F-127 as the SDA.</li> <li>• TiO<sub>2</sub> sol was spin-coated onto ITO glass slides and/or silicon wafer.</li> </ul>	<ul style="list-style-type: none"> <li>• Highly ordered TiO<sub>2</sub> mesoporous framework was obtained after calcination at 350°C.</li> <li>• The mesoporous framework was stable even after calcination at 600°C.</li> <li>• TiO<sub>2</sub> CS ranged between 7.6 and 29.6 nm with pore walls ~13 nm.</li> </ul>	<ul style="list-style-type: none"> <li>• Thin film calcined at 350°C showed poor PCD of methyl orange due to the presence of amorphous TiO<sub>2</sub> and organic residues.</li> <li>• There exists an optimum calcination temperature 500°C for excellent PCD activity, above which the mesoporous structure collapsed.</li> </ul>
(Castro and Durán 2013)	<ul style="list-style-type: none"> <li>• TiO<sub>2</sub> mesoporous thin film was prepared using F-127 and Brij58 as the SDA.</li> <li>• TiO<sub>2</sub> sol was dip-coated to glass slides and/or silicon wafer, 6 mm s<sup>-1</sup> withdrawal rate. An intermediate SiO<sub>2</sub> layer was coated to prevent the diffusion of Na<sup>+</sup> from the glass substrate to the TiO<sub>2</sub> coating.</li> </ul>	<ul style="list-style-type: none"> <li>• TiO<sub>2</sub> CS ranged between 7 and 12 nm. TiO<sub>2</sub> layer prepared with F-127 showed larger pore sizes (6-10 nm).</li> <li>• TiO<sub>2</sub> layer prepared with F-127 showed highly ordered TiO<sub>2</sub> framework while the layer prepared with Brij58 showed a homogeneous mesoporous structure without pore ordering.</li> </ul>	<ul style="list-style-type: none"> <li>• TiO<sub>2</sub> layer prepared with Brij58 showed higher PCD efficiency when treating gaseous pollutants: TCE (trichloroethene), H<sub>2</sub>S (hydrogen sulfide) and methyl-ethyl-ketone.</li> <li>• TiO<sub>2</sub> layer prepared with Brij58 showed a higher PCD efficiency when treating aqueous methyl orange dye solution.</li> </ul>

**Table 2.8** Ag-decorated TiO<sub>2</sub>-based thin film and photocatalytic ceramic membrane: preparation, properties and performances

References	Synthesis / fabrication highlights	Important physico-chemical properties	Photocatalytic, anti-bacterial and membrane performances
(Page et al. 2007)	<ul style="list-style-type: none"> <li>• Ag-TiO<sub>2</sub> film was prepared by a modified sol-gel method. AgNO<sub>3</sub> was added in the preparation of TiO<sub>2</sub> sol.</li> <li>• Ag-TiO<sub>2</sub> sol was dip-coated to different types of substrates.</li> </ul>	<ul style="list-style-type: none"> <li>• Ag present in the Ag-TiO<sub>2</sub> films as Ag<sub>2</sub>O.</li> <li>• Ag-TiO<sub>2</sub> films displayed a photo-induced super-hydrophilicity property.</li> </ul>	<ul style="list-style-type: none"> <li>• Anti-bacteria property was tested against gram-positive (<i>B. cereus</i>, and <i>S. aureus</i>) and gram-negative bacteria (<i>E. coli</i>) using UV 365 nm as irradiation sources.</li> <li>• Gram-positive bacteria were more susceptible to the anti-bacterial activity of Ag-TiO<sub>2</sub> film mainly due to its more porous membrane structure.</li> </ul>
(Liu et al. 2008)	<ul style="list-style-type: none"> <li>• TiO<sub>2</sub> was prepared by sol-gel method using P-123 as SDA.</li> <li>• TiO<sub>2</sub> was spin-coated onto glass substrate.</li> <li>• Ag-doping was done by immersing coated substrate in the AgNO<sub>3</sub> solution.</li> </ul>	<ul style="list-style-type: none"> <li>• Concentration of Ag<sup>+</sup> released was determined using anodic stripping voltametry. Higher initial Ag<sup>+</sup> release rate was observed.</li> <li>• Homogeneous worm-like 3-dimensional pores were formed. Pore size was 5 nm in diameter. Ag NPs were incorporated in the TiO<sub>2</sub> mesopores.</li> <li>• Pore volume and surface area of the Ag-TiO<sub>2</sub> thin film was 0.26 cm<sup>3</sup> g<sup>-1</sup> and 157 m<sup>2</sup> g<sup>-1</sup>.</li> </ul>	<ul style="list-style-type: none"> <li>• Anti-bacterial activity of the Ag-TiO<sub>2</sub> composite was tested against <i>E. coli</i> and Ag-resistant <i>E. coli</i>.</li> <li>• Extent of anti-bacterial activity was determined by viable-bacteria cells imaging using epifluorescence microscopy.</li> <li>• Ag-TiO<sub>2</sub> composite was equally effective in killing both <i>E. coli</i> and Ag-resistant <i>E. coli</i>.</li> </ul>

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(Nasr-Esfahani and Habibi 2008)	<ul style="list-style-type: none"> <li>• Ag-TiO<sub>2</sub> materials were prepared by sol-gel method, using MC as SDA and TiO<sub>2</sub> nanoparticles (3 types) as fillers.</li> <li>• Ag was introduced by soaking of film in the AgNO<sub>3</sub> solution.</li> </ul>	<ul style="list-style-type: none"> <li>• TiO<sub>2</sub> CS was 10 nm.</li> <li>• TiO<sub>2</sub> nanoparticles filler aggregate and grow to form a larger TiO<sub>2</sub> crystal during calcination.</li> <li>• The addition of nanoparticles fillers enhances the growth of TiO<sub>2</sub> crystals.</li> </ul>	<ul style="list-style-type: none"> <li>• Improved photocatalytic activity as compared with the undoped TiO<sub>2</sub>.</li> </ul>
(Akhavan 2009)	<ul style="list-style-type: none"> <li>• TiO<sub>2</sub> thin film was prepared by dip-coating of TiO<sub>2</sub> sol on glass substrate.</li> <li>• Ag was introduced by soaking of film in the AgNO<sub>3</sub> solution.</li> <li>• Other type of Ag-TiO<sub>2</sub> thin film was prepared by a direct incorporation of Ag sol in the sol preparation.</li> </ul>	<ul style="list-style-type: none"> <li>• TiO<sub>2</sub> crystallite size (CS) was ~11 nm. The mean size of Ag NPs was ~12 nm.</li> <li>• Based on XPS analysis, Ag species exist as AgO, Ag<sub>2</sub>O and Ag<sup>0</sup>.</li> <li>• Ag was found to aggregate on the surface of Ag-TiO<sub>2</sub> film.</li> <li>• Surface Plasmon resonance phenomenon due to Ag NPs was observed at 412 nm.</li> </ul>	<ul style="list-style-type: none"> <li>• Anti-bacterial activity of the Ag-TiO<sub>2</sub> composite was tested against <i>E. coli</i> in the presence of visible light irradiation (425 nm).</li> <li>• Enhanced anti-bacterial activity was observed for Ag-TiO<sub>2</sub> thin film.</li> <li>• Ag-TiO<sub>2</sub> thin film prepared by a direct incorporation of Ag source in the sol preparation displayed a higher anti-bacteria activity.</li> </ul>

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(Krylova et al. 2009)	<ul style="list-style-type: none"> <li>• Ag NPs were incorporated in various ceramic-based thin films: SiO<sub>2</sub>, TiO<sub>2</sub>, and ZrO<sub>2</sub> prepared by sol-gel method. P-123 was incorporated as SDA.</li> <li>• Thin films were deposited onto different supports (i.e. glass, silicon wafer and aluminum) by dip-coating method.</li> </ul>	<ul style="list-style-type: none"> <li>• Ag inhibited the growth of TiO<sub>2</sub> crystals.</li> <li>• The mean pore size of TiO<sub>2</sub> was 12 nm with pore wall thickness of 5.5 nm.</li> <li>• Mixture of anatase and brookite phases was observed for Ag-TiO<sub>2</sub> thin film.</li> <li>• TiO<sub>2</sub> CS ranged between 15 and 25 nm. Average size of Ag NPs was 4-10 nm.</li> <li>• Surface Plasmon resonance phenomenon was observed at 400 nm.</li> </ul>	<ul style="list-style-type: none"> <li>• No performance evaluation was performed in this work.</li> </ul>
(Răileanu et al. 2009)	<ul style="list-style-type: none"> <li>• Ag-doped (2% wt) TiO<sub>2</sub> thin film supported on glass.</li> <li>• Two types of thin film: direct Ag doping (in-situ co-gelation) and addition of Ag into the TiO<sub>2</sub> sol.</li> </ul>	<ul style="list-style-type: none"> <li>• Smoother TiO<sub>2</sub> thin film was observed for film prepared by direct Ag doping</li> <li>• Ag was present as Ag<sup>+</sup>.</li> <li>• Ag inhibited the growth of TiO<sub>2</sub> crystals.</li> <li>• Ag was found to promote anatase-rutile transformation.</li> </ul>	<ul style="list-style-type: none"> <li>• Improved photocatalytic activity as compared with undoped TiO<sub>2</sub>.</li> <li>• Early anatase-rutile transformation decreases the overall PCD efficiency.</li> </ul>

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(Hou et al. 2009)	<ul style="list-style-type: none"> <li>• Ag-TiO<sub>2</sub> film was prepared by a modified sol-gel method. AgNO<sub>3</sub> was added in the preparation of TiO<sub>2</sub> sol.</li> <li>• Ag-TiO<sub>2</sub> sol was dip-coated 3 times to a glass substrate.</li> </ul>	<ul style="list-style-type: none"> <li>• TiO<sub>2</sub> CS ranged between 10 and 40 nm.</li> <li>• Formation of Ag cluster was observed for sample with Ag/Ti molar ratio = 0.48.</li> <li>• Based on XPS analysis, Ag species exist as AgO, Ag<sub>2</sub>O and Ag<sup>0</sup>.</li> <li>• Ag was found to aggregate on the surface of Ag-TiO<sub>2</sub> film.</li> </ul>	<ul style="list-style-type: none"> <li>• There exists an optimum level of Ag loading for maximum PCD performance both when irradiated with UV or visible light.</li> <li>• PCD performance of Ag/TiO<sub>2</sub> film was better under visible light irradiation.</li> </ul>
(Ma et al. 2009a)	<ul style="list-style-type: none"> <li>• Ag-TiO<sub>2</sub> sol was prepared by sol-gel method. Hydroxyapatite (HAP) sol was prepared by precipitation method.</li> <li>• Alumina support was coated with two-step approach: first with HAP sol and calcined followed by coating of Ag-TiO<sub>2</sub> sol and final calcination.</li> </ul>	<ul style="list-style-type: none"> <li>• Thickness of HAP/Ag-TiO<sub>2</sub> composite layer was ~10μm.</li> <li>• No Ag<sup>0</sup> phase was observed in XRD spectra due to small amount of Ag<sup>0</sup> present.</li> <li>• Amount of HAP deposited varied from 2.8 to 5.5 g m<sup>-2</sup> depending on the dip time. Amount of Ag-TiO<sub>2</sub> deposited ~49 g m<sup>-2</sup> (not affected by the dip-time).</li> <li>• Mean pore size ~790 nm.</li> </ul>	<ul style="list-style-type: none"> <li>• Ag-TiO<sub>2</sub> sol with 1wt% Ag exhibits higher photoactivity than the one with 5wt% Ag and pure TiO<sub>2</sub>.</li> <li>• Anti-bacterial activity of the Ag-TiO<sub>2</sub> composite was tested against <i>E. coli</i>.</li> <li>• HAP was found to increase bacterial adsorption capacity of the membrane.</li> <li>• The removals of <i>E. coli</i> were approximately 6 and 4-logs under UV Irradiation and in the dark respectively.</li> </ul>

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(Akhavan and Ghaderi 2010)	<ul style="list-style-type: none"> <li>• Ag-TiO<sub>2</sub> was prepared by sol-gel method.</li> <li>• Ag-TiO<sub>2</sub> was dip-coated to glass substrate.</li> </ul>	<ul style="list-style-type: none"> <li>• TiO<sub>2</sub> CS was ~11 nm. The mean size of Ag NPs was ~10 nm.</li> <li>• Majority of the Ag species were Ag<sup>0</sup>. Ag<sup>0</sup> were found to agglomerate on the surface of TiO<sub>2</sub>.</li> <li>• Pore volume and surface area of the Ag-TiO<sub>2</sub> thin film was 0.30 cm<sup>3</sup> g<sup>-1</sup> and 213 m<sup>2</sup> g<sup>-1</sup>.</li> <li>• Ag<sup>+</sup> release was found to reach saturation after 8 days.</li> </ul>	<ul style="list-style-type: none"> <li>• Enhanced anti-bacterial activity was observed for Ag-TiO<sub>2</sub> thin film mainly due to slow Ag<sup>+</sup> release and slower recombination rate of photo-generated e<sup>-</sup>-h<sup>+</sup> pairs.</li> <li>• Anti-bacterial activity of the Ag-TiO<sub>2</sub> composite was tested against <i>E. coli</i>.</li> </ul>
(Kment et al. 2010)	<ul style="list-style-type: none"> <li>• Ag acetylacetonate was added during the preparation of TiO<sub>2</sub> sol. Ag-TiO<sub>2</sub> sol was dip-coated to a glass slide.</li> <li>• Fe- and Zr-doped TiO<sub>2</sub>. Were also prepared/</li> </ul>	<ul style="list-style-type: none"> <li>• TiO<sub>2</sub> CS ranged between 10 and 14 nm.</li> <li>• Ag was found to suppress the growth of anatase crystals.</li> </ul>	<ul style="list-style-type: none"> <li>• Ag-TiO<sub>2</sub> film displayed a relatively high quantum high, second only to Zr-TiO<sub>2</sub> based on electrochemistry experiment.</li> <li>• Ag-TiO<sub>2</sub> film displayed the highest PCD activity among the metal-doped TiO<sub>2</sub> film.</li> </ul>
(Zhao and Chen 2011)	<ul style="list-style-type: none"> <li>• Ag-TiO<sub>2</sub> sol was prepared by sol-gel method utilizing H<sub>2</sub>O<sub>2</sub> as peptizing agent to allow preparation at neutral pH.</li> <li>• Ag-TiO<sub>2</sub> sol was dip-coated to a glass slide.</li> </ul>	<ul style="list-style-type: none"> <li>• Ag NPs were found deposited on the surface of TiO<sub>2</sub>.</li> <li>• Rhombus-shape TiO<sub>2</sub> were synthesized (diagonal lengths of 10 and 40 nm).</li> </ul>	<ul style="list-style-type: none"> <li>• Enhanced photocatalytic activity was observed for Ag-TiO<sub>2</sub> thin film even at low Ag loading (0.5 wt%).</li> </ul>

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(Yu et al. 2011)	<ul style="list-style-type: none"> <li>• Ag-TiO<sub>2</sub> was prepared by sol-gel method using P-123 as SDA and acetylacetone as chelating agent.</li> <li>• Ag-TiO<sub>2</sub> was spin-coated onto silicon wafer.</li> </ul>	<ul style="list-style-type: none"> <li>• Ag species exists as Ag<sup>0</sup>. After UV exposure, Ag<sub>2</sub>O was formed through oxidation.</li> <li>• Average size of TiO<sub>2</sub> range between 10 and 20 nm. Ag NPs of various sizes (range between 10 and 30 nm) exist as agglomerated granules. Ag NPs agglomeration could be avoided at higher Ag concentration. Ag NPs were concentrated on the surface of the TiO<sub>2</sub>.</li> </ul>	<ul style="list-style-type: none"> <li>• Anti-bacteria property was tested against <i>E. coli</i> using UV 365 nm as the irradiation sources.</li> <li>• Anti-bacterial activity of Ag-TiO<sub>2</sub> composites were studied by diffusion inhibition zone and batch reactor.</li> <li>• Anti-bacterial activity was proportional to the [Ag] on the TiO<sub>2</sub> surface.</li> </ul>
(Piwoński et al. 2011)	<ul style="list-style-type: none"> <li>• TiO<sub>2</sub> was dip-coated on silicon wafer.</li> <li>• TiO<sub>2</sub> thin film was immersed in the AgNO<sub>3</sub> solution (from 0.05 – 500 mM) followed by UV irradiation or irradiation with excimer laser.</li> </ul>	<ul style="list-style-type: none"> <li>• Three Ag- photodeposition parameters were studied: [AgNO<sub>3</sub>], irradiation time, and irradiation source.</li> <li>• Number of photodeposited Ag increase by 10 folds when [AgNO<sub>3</sub>] increased by 10,000. Prolonged irradiation time increase the size of deposited Ag.</li> <li>• UV-assisted photodeposition was more effective.</li> </ul>	<ul style="list-style-type: none"> <li>• TiO<sub>2</sub> film displayed a weak anti-bacterial activity in the dark.</li> <li>• Anti-bacterial activity is proportional to the [Ag] on the TiO<sub>2</sub> surface.</li> </ul>

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(Kubacka et al. 2011)	<ul style="list-style-type: none"> <li>• TiO<sub>2</sub> was prepared using a micro-emulsion synthetic route supported on ethylene-vinyl alcohol copolymer.</li> <li>• Ag was photodeposited up to 1% wt% with respect to Ti.</li> </ul>	<ul style="list-style-type: none"> <li>• Characteristic TiO<sub>2</sub> primary particle size was ~10 nm.</li> <li>• No structural changes were observed for Ag-decorated film. The inclusion of Ag only alters the optical property of the film.</li> </ul>	<ul style="list-style-type: none"> <li>• Anti-bacteria property was tested against <i>E. coli</i> and <i>S. aureus</i> using UV (280) nm and visible light (500 nm) as irradiation sources.</li> <li>• Ag decorated film remove up to 7 and 6 logs <i>E. coli</i> and <i>S. aureus</i> respectively when irradiated with UV.</li> <li>• Ag decorated film remove up to 3 logs <i>E. coli</i> and <i>S. aureus</i> when irradiated with visible light.</li> </ul>
(Emadi and Raeissi 2011)	<ul style="list-style-type: none"> <li>• TiO<sub>2</sub> layer was prepared by anodic oxidation of titanium plate support.</li> <li>• Ag was deposited by electro-deposition.</li> </ul>	<ul style="list-style-type: none"> <li>• Average size of electro-deposited Ag was 32 nm.</li> </ul>	<ul style="list-style-type: none"> <li>• Ag-TiO<sub>2</sub> effectively killed <i>E. coli</i> and <i>S. aureus</i> bacteria cells.</li> <li>• Bio-medical application.</li> </ul>
(Wu et al. 2011)	<ul style="list-style-type: none"> <li>• Microporous TiO<sub>2</sub> thin film was prepared by anodizing titanium plate.</li> <li>• Ag-doping was done by immersing anodized Ti plate in the AgNO<sub>3</sub> solution.</li> </ul>	<ul style="list-style-type: none"> <li>• The TiO<sub>2</sub> thin film consists of 80% anatase and 20% rutile.</li> <li>• The size of micropores range between 90 and 300 nm.</li> </ul>	<ul style="list-style-type: none"> <li>• Extent of PCD reaction was determined by measuring concentration of hydroxyl radical.</li> <li>• Disinfection capability of Ag-TiO<sub>2</sub> composite was determined by the level of lipid peroxidation, K<sup>+</sup> and protein leakage from the cells.</li> </ul>

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(Joya et al. 2012)	<ul style="list-style-type: none"> <li>• TiO<sub>2</sub> was dip-coated on glass substrate.</li> <li>• TiO<sub>2</sub> thin film was immersed in the AgNO<sub>3</sub> solution followed by irradiation with KrF excimer laser.</li> </ul>	<ul style="list-style-type: none"> <li>• Thin film thickness was in the range between 250-300 nm.</li> <li>• TiO<sub>2</sub> CS ranged between 38 and 43 nm.</li> <li>• Cubic and hexagonal Ag NPs size was ranged between 5 and 20 nm.</li> <li>• Surface Plasmon resonance phenomenon was observed at 516 nm (due to localized SPR of Ag NPs formed during the laser irradiation).</li> </ul>	<ul style="list-style-type: none"> <li>• Anti-bacteria property was tested against <i>E. coli</i> and <i>S. aureus</i> using normal daylight as the irradiation source.</li> <li>• The Ag-TiO<sub>2</sub> thin film composite completely eliminated <i>E. coli</i> and <i>S. aureus</i> (<math>4 \times 10^4</math> cfu mL<sup>-1</sup>) within 60 min.</li> </ul>
(Gutiérrez et al. 2013)	<ul style="list-style-type: none"> <li>• Ag-TiO<sub>2</sub> was prepared by sol-gel method.</li> <li>• Ag-TiO<sub>2</sub> was dip-coated to glass substrate.</li> </ul>	<ul style="list-style-type: none"> <li>• TiO<sub>2</sub> CS ranged between 13 and 18 nm.</li> <li>• There exists an optimum Ag loading for which the photocurrent would be maximized (indicating maximum PCD capability).</li> </ul>	<ul style="list-style-type: none"> <li>• Enhanced photocatalytic decomposition of methanol and Basic Orange II were observed for Ag-TiO<sub>2</sub> thin film.</li> </ul>
(Obalová et al. 2013)	<ul style="list-style-type: none"> <li>• Ag-TiO<sub>2</sub> was prepared by sol-gel method.</li> <li>• Ag-TiO<sub>2</sub> was dip-coated to glass substrate.</li> </ul>	<ul style="list-style-type: none"> <li>• Ag was found to improve crystallinity while suppressing crystal growth of TiO<sub>2</sub>.</li> </ul>	<ul style="list-style-type: none"> <li>• Enhanced photocatalytic decomposition of N<sub>2</sub>O was observed for Ag-TiO<sub>2</sub> thin film.</li> <li>• There exists an optimum amount of Ag-doping for efficient decomposition of N<sub>2</sub>O.</li> </ul>

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## 2.4 Conclusion

TiO<sub>2</sub> has been used extensively in the water and wastewater treatment due to its ability to generate electron and hole pairs when irradiated with UV. The photogenerated e<sup>-</sup> and h<sup>+</sup> pairs could generate different types of non-selective reactive radicals upon reaction with suitable electron and holes acceptor. These radicals are responsible for the decomposition and possible complete mineralization of wide range of environmental recalcitrant and noxious pollutants.

The need of post-separation of the powdered photocatalyst during application had prompted many research efforts on supported TiO<sub>2</sub>. Ceramic support has been used as an ideal support material due to its stability and potential long term application. The idea of supported TiO<sub>2</sub> on a ceramic membrane to allow continuous treatment processes has been explored extensively.

Different method can be employed to increase the PCD capability of TiO<sub>2</sub>. Among which are the usage of SDA and chelating agent during the preparation of the sol, and doping with various metal/non-metal elements. Ag has been an excellent dopant candidate due to its anti-bacterial activity and visible light responsiveness. Different aspects of incorporation of SDA and Ag dopant have been discussed in this chapter.

In the following chapters, effort to immobilized TiO<sub>2</sub> into a ceramic membrane support will be described. Different types of SDAs will be used to improve overall performance of the photocatalyst. Various preparation steps will be carefully considered in order to obtain a hybrid membrane that shows an optimum photocatalytic and membrane performance. Lastly, the addition of Ag is considered to improve the PCD capability as well as to introduce an additional anti-bacterial activity to the hybrid membrane.

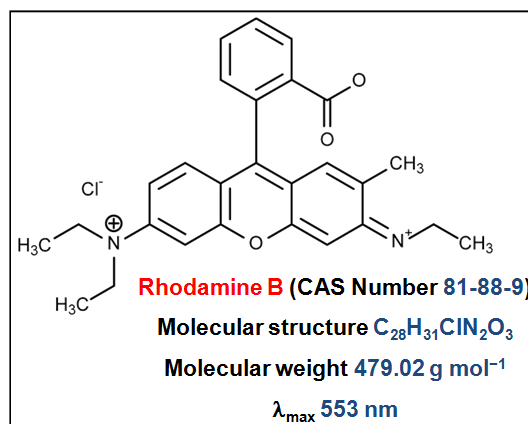
## CHAPTER 3 MATERIALS AND METHODS

### 3.1 Materials and synthesis techniques

#### 3.1.1 Chemicals and materials

All chemicals used in this study were of analytical grade. The following chemical were used in the preparation of TiO<sub>2</sub> sol without further purification unless it is stated otherwise: titanium tetraisopropoxide (TTIP, Merck), 2-propanol (IPA, Merck), hydrochloric acid 37% (HCl, Aldrich), and nitric acid 67% (HNO<sub>3</sub>, Merck). Silver nitrate  $\geq 98\%$  (AgNO<sub>3</sub>, Merck) was used as the Ag source for the Ag-decorated TiO<sub>2</sub> (Ag-TiO<sub>2</sub>). MilliQ water (18.2 M $\Omega$ .cm at 25°C) was used throughout in the sol preparation and other experiments in this study. Four types of structure directing agents (SDAs) were employed to produce mesoporous TiO<sub>2</sub> layer, i.e. poly(ethylene glycol)–block–poly(propylene glycol)–block–poly(ethylene glycol) (Pluronic<sup>®</sup> P-123, P-123, Aldrich), polyethylene glycol p-(1,1,3,3-tetramethylbutyl)-phenyl ether (Triton X-100<sup>TM</sup>, X100, Aldrich), Polyoxyethylene (20) sorbitan monolaurate (Tween<sup>®</sup> 20, T20, Aldrich), and Polyoxyethylene (20) sorbitan monooleate (Tween<sup>®</sup> 80, T80, Aldrich).

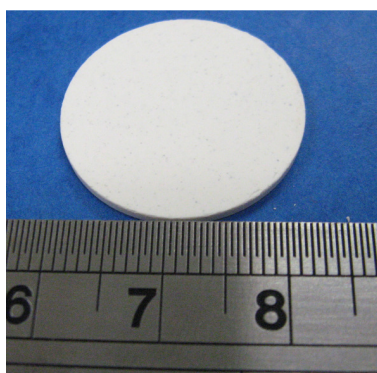
The macroporous alumina ceramic membrane support was prepared from aluminum oxide ( $\alpha$ -Al<sub>2</sub>O<sub>3</sub>, Aldrich) with a relative density of 4 g cm<sup>-3</sup> and average particle size of 0.05  $\mu$ m. Poly vinyl alcohol 88%-hydrolyzed (MW 88,000 g mol<sup>-1</sup>, PVA, Acros Organics) was used as pores filler during the coating of TiO<sub>2</sub> photocatalytic layers in the membrane fabrication. The membrane retention capability was evaluated using poly(ethylene glycol) (PEG, Alfa Aesar) of MW 1,500, 6,000, 10,000, and 20,000 g mol<sup>-1</sup>. Rhodamine B (Fig. 3.1) (MW 479.02 g mol<sup>-1</sup>,  $\lambda_{\max}$  553 nm, RhB, Merck), a common tracer dye and bio-marker, was used as the model organic pollutant without further purification.



**Figure 3.1** Molecular structure of Rhodamine B.

### 3.1.2 Preparation of macroporous alumina ceramic support

The macroporous alumina ceramic membrane support was fabricated by molding a predetermined amount of  $Al_2O_3$  powder on a custom-made pellet pounder assembly. The pellet pounder assembly was pressed at 50 kN for 3 min and 100 kN for the subsequent 3 min by the uni-axial hydraulic press (Perkin Elmer). The diameter and thickness of the resulting ceramic membrane support were 23 mm and 2 mm respectively.

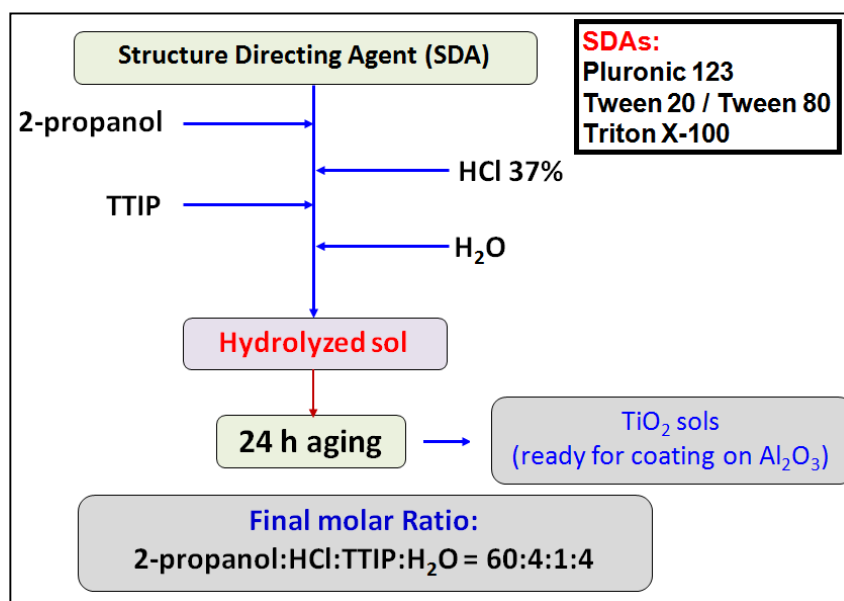


**Figure 3.2** Photograph of alumina ceramic membrane support.

The pelletized ceramic membrane support was calcined and sintered at 1280°C in a programmable muffle furnace (Nabertherm LHT04/16) for 24 h, and was cooled down naturally to the room temperature. Finally, the ceramic membrane support was subjected to the multi-step sandpaper polishing (ISO grit sizes of P360, P600, P1000 and P1500) in order to obtain a smooth surface for the subsequent dip coating process. Fig. 3.2 shows photograph of the as-fabricated alumina ceramic membrane support.

### 3.1.3 Preparation of TiO<sub>2</sub> sols

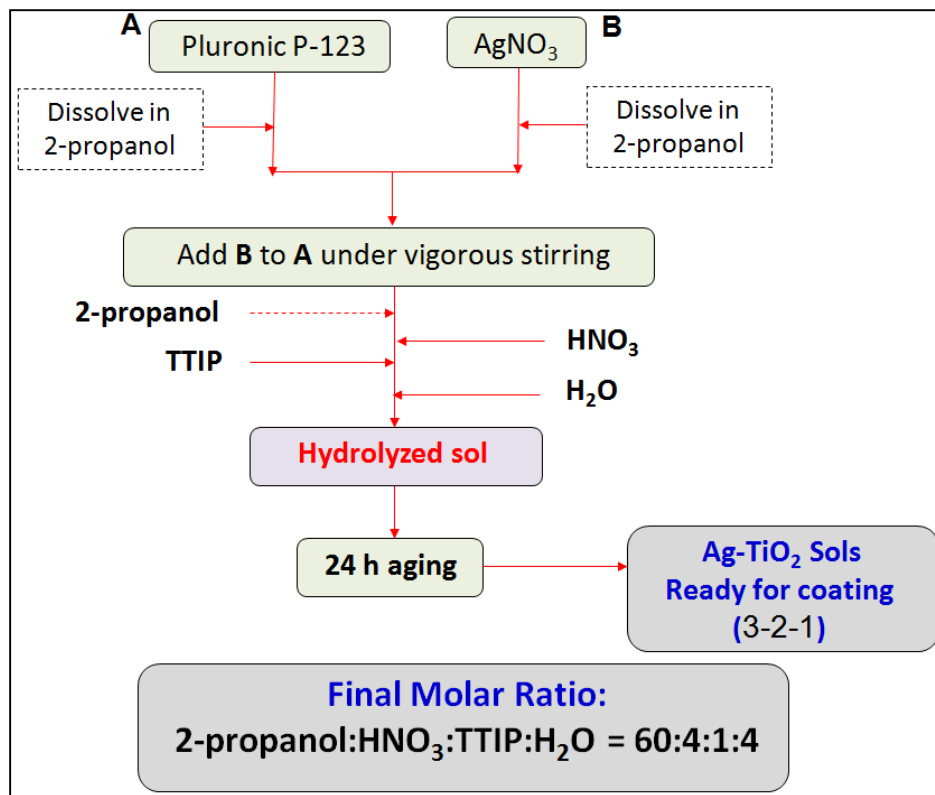
TiO<sub>2</sub> sol was prepared using an acid-catalyzed sol-gel method. Fig. 3.3 summarizes the sol-gel preparation of the TiO<sub>2</sub> sol. TTIP was used as the titanium alkoxide precursor with IPA as the solvent. Different types of SDAs (i.e. P-123, X100, T20 and T80) were employed in the preparation of the TiO<sub>2</sub> sol as the pore forming agents.



**Figure 3.3** Schematic of preparation of the TiO<sub>2</sub> sol using sol-gel method.

In a typical preparation of the TiO<sub>2</sub> sol, a predetermined amount of SDA was dissolved in IPA. The mixture was stirred for 1 h at the room temperature to ensure complete dissolution of the SDA. After which, HCl was added drop-wise to the mixture. Finally, the hydrolysis and condensation reactions were initiated by the drop-wise addition of TTIP and MilliQ water under vigorous stirring. The homogeneity of the resulting sols was enhanced by continuous stirring at the room temperature for 12-24 h. After the aging period, the final sols were ready for coating and had a constant molar ratio of IPA:HCl:TTIP:H<sub>2</sub>O equals to 60:4:1:4.

### 3.1.4 Preparation of Ag-TiO<sub>2</sub> sols

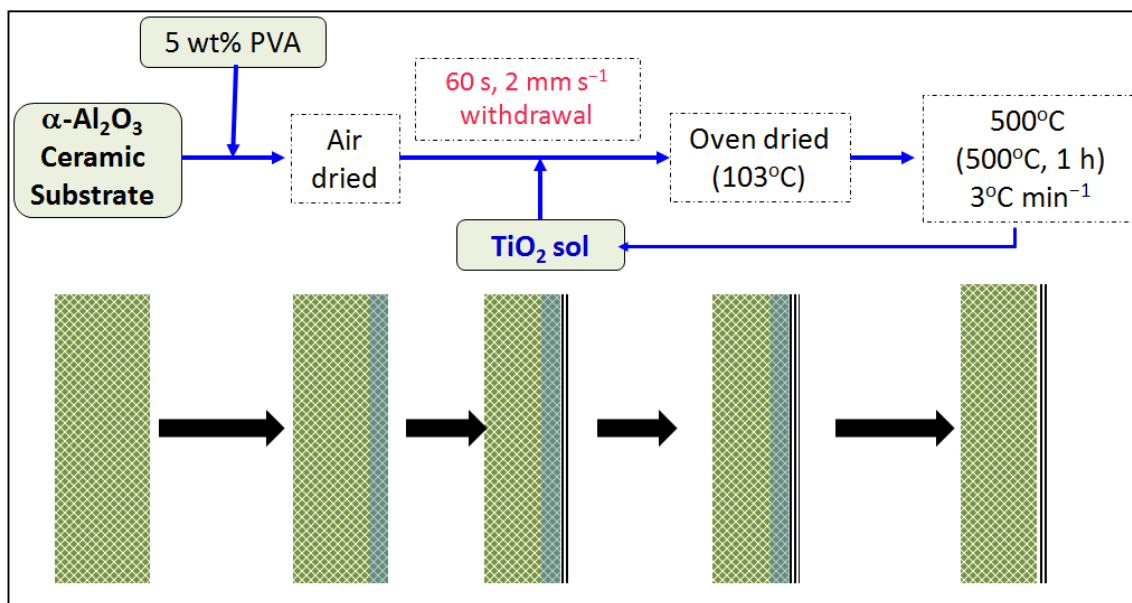


**Figure 3.4** Schematic of preparation of the Ag-decorated TiO<sub>2</sub> sol using sol-gel method.

Ag-TiO<sub>2</sub> sol was prepared using the modified acid-catalyzed sol-gel method. Fig. 3.4 summarizes the preparation of the Ag-TiO<sub>2</sub> sol. A predetermined amount of P-123 was dissolved in IPA to obtain solution A. Solution B was prepared by dissolving AgNO<sub>3</sub> in IPA and was stirred continuously at room temperature for 1 h to ensure complete dissolution of AgNO<sub>3</sub>. Solution B was then added drop-wise to the solution A under vigorous stirring. After which, HNO<sub>3</sub> was added into the mixture. Finally, TTIP and H<sub>2</sub>O were added drop-wise to the mixture for the hydrolysis and condensation reaction under a vigorous stirring. The resulting sols were stirred continuously for 12-24 h at room temperature to improve its homogeneity. The final Ag-TiO<sub>2</sub> sols had a molar ratio of IPA:HNO<sub>3</sub>:TTIP:H<sub>2</sub>O equal to 60:4:1:4. Variable amounts of P-123 and AgNO<sub>3</sub> were used in the preparation of different sols to obtain Ag-TiO<sub>2</sub> sols that contained 0.5, 1.0, 2.0, 5.0, or 10 wt% of P-123 and 0.5, 1.0, 2.0, 3.0 mol% of Ag (with respect to TiO<sub>2</sub>) respectively.

### **3.1.5 Fabrication of hierarchically porous TiO<sub>2</sub> photocatalytic ceramic membrane**

The hierarchical architecture of the TiO<sub>2</sub> photocatalytic ceramic membrane was obtained by coating different sols on the alumina ceramic membrane support. In this architecture, the porosity gradient was obtained through the coating of multiple TiO<sub>2</sub> photocatalytic sub-layers of different pore structures starting from coating of the layer of largest pore size on the Al<sub>2</sub>O<sub>3</sub> support, followed by coating of subsequent layers of decreasing pore sizes.



**Figure 3.5** Fabrication of hierarchically porous TiO<sub>2</sub> photocatalytic ceramic membrane.

Fig. 3.5 illustrates the step-by-step fabrication of the TiO<sub>2</sub> membrane. One side of the ceramic membrane support was covered with liquid-proof tape to allow only a single-side coating of TiO<sub>2</sub> sols. Prior to the coating, the smoothed alumina ceramic membrane support was first wetted with 5% PVA solution which would fill up the pores of Al<sub>2</sub>O<sub>3</sub>. This pre-wetting step is essential in order to prevent the possible infiltration of the TiO<sub>2</sub> sol into the macroporous support which would cause pore blocking and decreased porosity of the resulting membrane. The membrane support was dried at the room temperature and then dipped into the designated TiO<sub>2</sub> sol for 60 s using a home-fabricated dip-coater. The coated membrane was withdrawn from the sol at a rate of 2 mm s<sup>-1</sup>. The coated membrane was first oven dried (103°C, 15 min), then calcined in the muffle furnace (Nabertherm LHT04/16) at 500°C for 1 h (3°C min<sup>-1</sup> heating rate). The membrane was cooled down naturally to the room temperature and ready for the coating of the subsequent sub-layer. The process was

repeated until all the sub-layers have been coated. Ag-TiO<sub>2</sub> membranes were prepared with the similar fabrication steps with the details are delineated in Section 6.2.1.

In order to characterize the microstructure of the TiO<sub>2</sub> layer, a thick TiO<sub>2</sub> layer was coated onto a Petri dish. The resulting TiO<sub>2</sub> layer was then scrapped off, heat treated, pulverized, and stored for its subsequent characterizations. Different TiO<sub>2</sub> layers were also coated on a borosilicate glass for the evaluation of their hydrophilicity. The glass support was cleaned thoroughly and dried at the room temperature and then dipped into the designated TiO<sub>2</sub> sol for 60 s using a home-fabricated dip-coater. The coated glass was withdrawn from the sol at a rate of 2 mm s<sup>-1</sup>. The coated borosilicate glass was then heat-treated by the same method used for the TiO<sub>2</sub> membrane.

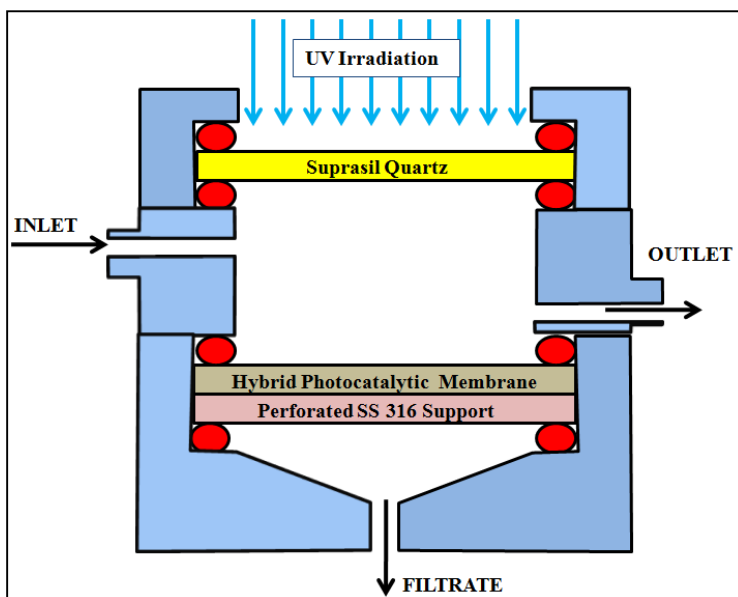
### **3.1.6 Preparation of microbial strain**

*Escherichia coli* (*E. coli*, ATCC<sup>®</sup> 25922<sup>™</sup>), a gram-negative bacteria, was chosen as the model bacteria for the anti-bacterial study of Ag-TiO<sub>2</sub> membrane. *E. coli* was inoculated in the tryptic soy broth at 37°C until their mid-exponential growth phase. *E. coli* cells were collected by centrifugation at 10,000 rpm and washed multiple times with 0.9 wt% NaCl (Merck) solution. After decanting the supernatant, the bacterial cell pellet was re-suspended in a 0.9 wt% NaCl solution. The *E. coli* stock solution of approximately 1 × 10<sup>8</sup> colony-forming units per mL (cfu mL<sup>-1</sup>) was then prepared for the subsequent anti-bacterial experiments.

### **3.2 Photocatalytic membrane reactor (PMR) setup**

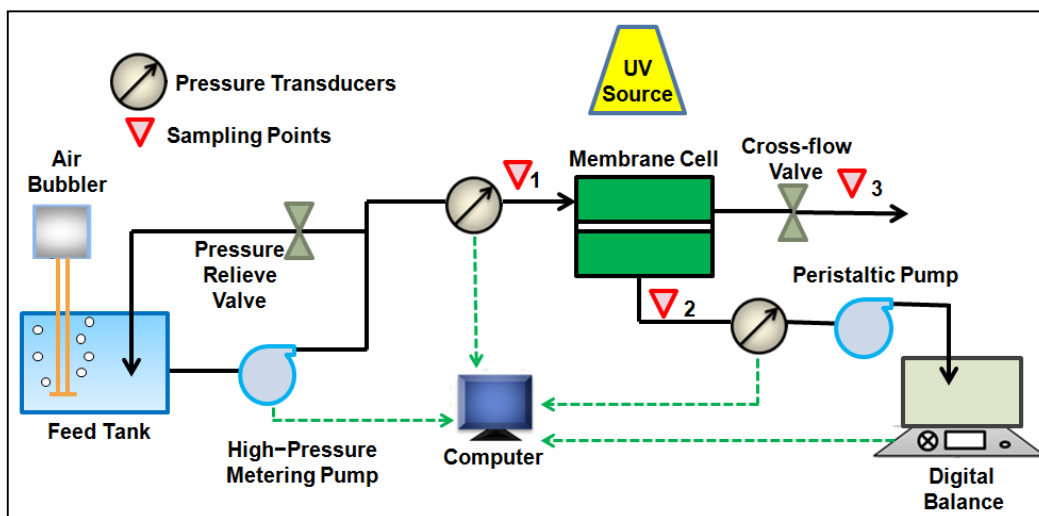
The performance of the hybrid TiO<sub>2</sub> photocatalytic ceramic membrane was evaluated using a photocatalytic membrane reactor (PMR) setup. The membrane cell module (Fig. 3.6)

was fabricated using stainless steel SS316 alloy. The chamber volume was 15 mL. The top side of the module (feed chamber) was made of transparent Suprasil<sup>®</sup> quartz that allows UV penetration to the surface of the mounted membrane. The TiO<sub>2</sub> photocatalytic ceramic membrane was mounted and tightly secured in the membrane cell. A perforated SS316 disk was used as the mechanical support to the TiO<sub>2</sub> membrane.



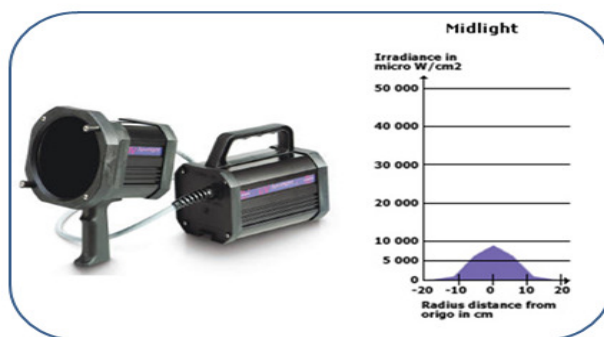
**Figure 3.6** Schematic diagram of the membrane cell module.

The cell module was connected to the PMR setup (Fig. 3.7). A high-pressure metering pump (up to 400 bar, 5979 Optos Pump 2HM, Eldex Laboratories) was connected to deliver the feed water. The permeate flux was monitored using an electronic balance and then re-circulated back to the feed tank. The transmembrane pressure (TMP) was recorded using a pressure transducer. Air stream was supplied into the feed tank to provide mixing and oxygen supply that would assist the photocatalytic reaction. The PMR setup with its various safety features was fully controlled by the computer setup.



**Figure 3.7** Schematic diagram of the PMR setup operating under dead-end filtration mode.

The PMR was operated under a dead-end filtration mode with constant flux. Three sampling points were designated in the setup to allow (1) sampling prior to the inlet of the membrane cell module, (2) sampling at the permeate side, and (3) sampling at the cross-flow outlet for the membrane cleaning step during the anti-bacterial experiment (Chapter 6). UV Labino 135 lamp (Fig. 3.8) ( $\lambda_{\max} = 365 \text{ nm}$ , intensity of  $60 \text{ W m}^{-2}$  measured on the surface of the RhB solution) was used as the UV-A source for the PCD reaction.



**Figure 3.8** UV Labino 135 midlight lamp as the source of UV irradiation.

### 3.3 Characterization techniques and analytical methods

Nitrogen (N<sub>2</sub>) adsorption/desorption isotherms for the porosimetry analysis of the TiO<sub>2</sub> layers were studied using Quantachrome Autosorb-1 Analyzer at liquid N<sub>2</sub> temperature of 77 K. The pulverized TiO<sub>2</sub> powders were degassed overnight at 150°C prior to the actual measurement. The Brunauer-Emmett-Teller surface area (S<sub>BET</sub>) and Barrett-Joyner-Halenda (BJH) pore size distribution were derived from the result (Barrett et al. 1951, Brunauer et al. 1938).

The mineralogy and crystal structures of the TiO<sub>2</sub> layers were analyzed using X-rays diffractometer (Bruker D8 Advance) with a monochromated high intensity Cu-Kα ( $\lambda = 1.5418 \text{ \AA}$ ) radiation over a  $2\theta$  range of 5-80° at a scan rate of 1.25° min<sup>-1</sup>. Scherrer's equation (Scherrer 1918) is used to calculate TiO<sub>2</sub> crystallite size from the peak broadening of (101) anatase crystal plane at 25.3°.

X-ray photoelectron spectroscopy (XPS) studies were conducted using a Kratos Axis Ultra spectrophotometer with a monochromatic Kα excitation source ( $h\nu = 1486.71 \text{ eV}$ ). All binding energies for elements of interest were corrected against an adventitious carbon C 1s core level at 284.8 eV. All XPS peaks were fitted using Shirley background together with Gaussian-Lorentzian function using CASA XPS software.

Fourier transformed infra-red (FTIR) spectra were collected using Perkin Elmer 2000 spectrophotometer to investigate the vibrational absorbance and structural characteristics of the TiO<sub>2</sub> layers. Samples for FTIR analysis were prepared by mixing 2 mg of sample with 275 mg of potassium bromide. The mixture was poured into the pellet poulder and was subjected to an initial hydraulic pressure of 10 kN for 1 min followed by 100 kN pressure for another 1 min using an uni-axial hydraulic press. The FTIR spectra were collected from wavenumber of 4,000 to 400 cm<sup>-1</sup>.

The Raman spectra were recorded using Renishaw RM1000 Raman spectrometer equipped with a Leica x50 Nplan objective lens. The spectra were generated with 50 mW, 633 nm He-Ne laser excitation with power at the sample surface < 2 mW. The Raman spectra were analyzed using Grams32/WiRE 1.3 software.

Scanning electron microscope (SEM) micrographs and energy-dispersive X-rays (EDX) spectra were obtained using a JEOL JSM-7600 FESEM equipped with an Oxford XMX0021 EDX analytical system. Prior to the analysis, the samples were coated with platinum using sputter coater to reduce the effect of surface charging.

High resolution transmission electron microscope (HRTEM) micrographs were obtained using a JEOL JEM-2010, operating at an accelerating voltage of 200 kV. Prior to the TEM analysis, the samples were ultrasonicated in ethanol for 10 min and then transferred to the copper grid for the analysis.

An atomic force microscope (AFM) (Park System) was used to study the morphology and relative surface roughness of the resulting TiO<sub>2</sub> photocatalytic membrane. A non-contact cantilever (PPP-NHCR-10M) was used to scan the surface of the TiO<sub>2</sub> photocatalytic membrane.

Rheological characteristic of the TiO<sub>2</sub> sols was investigated using a rheometer (Physica MCR 101, Anton Paar). The measurements were carried out using a 25 mm measuring plate (CP25-1) under a steady-state shear rate ranging from 0.1 to 100 s<sup>-1</sup> at 25 °C. The viscosity of dope solutions was recorded at the shear rate of 50 s<sup>-1</sup>.

Contact angle of the TiO<sub>2</sub> film coated on glass substrate was measured using video contact angle device (VCA Optima, AST Products). Droplet volume of 1 μL was dispensed from a 100 μL syringe.

The extent of RhB degradation was determined by measuring its light absorbance at 553 nm with an UV/Vis spectrophotometer (Genesys 10vis, Thermo Spectronic). Full spectra of RhB visible light absorption (from 600-450 nm) over the duration of the photocatalytic degradation were collected using UV/Vis-1700 Spectrophotometer (Shimadzu).

The concentration of PEG in the membrane retention capability experiments was determined with ASI-V TOC Analyzer (Shimadzu). The total-Ag concentration in the Ag leaching experiments (Section 3.4.4) was quantified using an inductively coupled plasma-mass spectrophotometer (ICP-MS, Perkin Elmer Elan DRC-e).

### **3.4 Experimental procedures**

#### **3.4.1 Determination of photo-induced super-hydrophilicity**

Contact angle of the TiO<sub>2</sub> or Ag-TiO<sub>2</sub> films coated on the borosilicate glass substrate was measured using video contact angle device (VCA Optima, AST Products). Prior to the contact angle measurement, the TiO<sub>2</sub> thin film was left in the dark for 24 h to remove any residual photo-induced super-hydrophilicity. The glass slide was then irradiated under UV for 1 h. For the measurement of the photo-induced super-hydrophilicity evolution of the representative TiO<sub>2</sub> thin film specimen, the contact angle was recorded at 0, 8, 24, and 48 h after the irradiation. The film was stored in the dark between each reading. For the rest of the thin film specimens, their contact angles were measured immediately after 1 h of UV irradiation.

#### **3.4.2 Photocatalytic degradation experiments using batch photoreactors**

The photocatalytic activity of TiO<sub>2</sub> photocatalytic ceramic membrane was evaluated in the batch photoreactor system. In a typical experiment, the membrane was fully submerged in 12

mL solution of RhB. The disk was left in the dark for 60 min to achieve RhB adsorption-desorption equilibrium. After the dark adsorption process, the TiO<sub>2</sub> batch photoreactor was subjected to UV irradiation ( $\lambda_{\text{max}} = 365 \text{ nm}$  with intensity  $60 \text{ W m}^{-2}$  measured on the surface of the RhB solution). There was no stirring or oxygen bubbling during the whole duration of the experiment in the batch photoreactor. Two mL of the solutions was taken at regular time intervals to evaluate photocatalytic degradation of RhB by measuring its light absorbance at 553 nm. After the measurement, the solution was immediately returned to the batch photoreactor in order to maintain a constant working volume throughout the duration of the PCD experiment. The extent of mineralization of RhB solution was also studied using TOC.

### **3.4.3 Photocatalytic degradation experiments using PMR**

Prior to the commencement of the experiment, the system was rinsed with Millipore ultrapure water to remove any possible impurities and to allow the permeate flux to reach a steady state. TiO<sub>2</sub> photocatalytic membranes were secured on the membrane cell module for performance evaluation of experiments using the PMR. The pure water permeability was determined by feeding Millipore ultrapure water into the reactor at various constant fluxes, and the resultant TMP values were recorded. PEG solutions ( $500 \text{ mg L}^{-1}$ ) of different molecular weights were fed into the reactor in order to determine molecular weight cut off (MWCO) of the membrane. As the standard protocol to compare the membrane retention capability, PEG solution ( $20,000 \text{ g mol}^{-1}$ ,  $500 \text{ mg L}^{-1}$ ) was fed into the PMR setup. After the steady-state flux was achieved, permeate was collected to determine the concentration of PEG.

The TiO<sub>2</sub> membranes were used to treat 100 mL of 25  $\mu\text{M}$  RhB solution. The PMR setup was fed with the RhB solution and was left in the dark for 60 min to achieve the RhB

adsorption-desorption equilibrium. After which, the pump and UV source were turned on to commence the experiment. In this experiment, permeate was re-circulated back to the feed tank. Control experiment was performed without UV to quantify the contribution of Ads-MR on the total RhB removal by the membrane.

The TiO<sub>2</sub> membranes were also tested for its reusability potential. In this study, the membrane was used for 4 cycles, each to treat 100 mL of 25 µM RhB fresh solution. At the end of each cycle of 8 h experimental run, the feed was replaced with MilliQ water. This was to clean the membrane under UV irradiation for 2 h, after which the fresh 25 µM RhB solution was fed into the reactor for the subsequent cycle of the experiment run.

#### **3.4.4 Silver leaching experiments**

The as-prepared membranes were immersed in MilliQ water (30 mL) to determine the total-Ag leaching (i.e. Ag<sup>+</sup> ions and Ag nanoparticles) from the membrane. Prior to the total-Ag leaching test, all glasswares were soaked in 10% (v/v) HNO<sub>3</sub> for 24 h to prevent cross-contamination. Triplicate aliquots (0.5 mL) were taken at regular intervals (up to 168 h immersion in MilliQ water) and digested in HNO<sub>3</sub> (150°C, 1 h) using a Hach DRB 200 digestion unit. Total-Ag leaching from the membrane operated in the PMR was also quantified. Each type of Ag-TiO<sub>2</sub> membranes was secured in the membrane cell module. MilliQ water was fed into the PMR with a constant flow rate of 4 mL min<sup>-1</sup>. Triplicate aliquots (0.5 mL) of permeate were taken at regular time interval (up to 480 min) and digested in HNO<sub>3</sub>. The total-Ag concentration in the aliquots was quantified using an inductively coupled plasma- mass spectrophotometer (ICP-MS, Perkin Elmer Elan DRC-e).

### 3.4.5 Diffusion inhibition zone experiments

Diffusion inhibition zone of various Ag-TiO<sub>2</sub> membranes with different hierarchical architectures were examined according to the standard Kirby-Bauer approach (Bauer et al. 1966). The diffusion inhibition zone test provides a fast qualitative indication of the effectiveness of the Ag-TiO<sub>2</sub> membrane to inhibit the growth of bacteria cells. An aliquot (200 µL,  $1 \times 10^8$  cfu mL<sup>-1</sup>) of each bacterial inoculums were spread evenly on the tryptic soy agar plates. Different types of Ag-TiO<sub>2</sub> membranes were placed on different agar plates with the photocatalytic layer facing down (in contact) with the agar surface. The development of the diffusion inhibition zone was examined after incubation at 37°C for 24 h.

### 3.4.6 Photocatalytic disinfection experiments using batch reactor

Prior to the anti-bacterial experiments, all glasswares were autoclaved (121°C, 15 min) and UV-irradiated (254 nm, 15 min) in order to avoid any contamination. Different Ag-TiO<sub>2</sub> membranes were immersed in 30 mL of *E. coli* bacterial suspensions ( $1 \times 10^8$  cfu mL<sup>-1</sup>, pH  $7.0 \pm 0.1$ ) which was kept in the dark. Control experiments were carried out without membrane or using Plu D membrane (which contained no Ag). Aliquots of the *E. coli* suspensions were drawn after 15 min of immersion. Serial dilutions of the aliquots were performed using 0.9 wt% NaCl solution. 100 µL of the aliquots of appropriate dilutions were streaked on the tryptic soy agar plates and incubated at 37°C for 24 h. After which, the colonies were enumerated to quantify the amount of active cells. All data were obtained from at least three replicates of experimental runs. Each membrane was used for 4 cycles of batch experiments.

### 3.4.7 Photocatalytic disinfection experiments using PMR

Ag-TiO<sub>2</sub> photocatalytic membranes were secured on the membrane cell module (Fig. 3.6) to evaluate its anti-bacterial performance in the PMR. The membrane cell was fed with 120 mL of *E. coli* bacterial suspension ( $1 \times 10^7$  cfu mL<sup>-1</sup>, pH  $7.0 \pm 0.1$ ) with a constant flux of 4 mL min<sup>-1</sup>. Aliquots of permeate were collected at regular time intervals of 5, 15, and 30 min respectively. The corresponding flux values were also recorded at the same time intervals. The control experiments without UV were also performed.

After 30 min of treatment cycle, the feed was replaced with 120 mL of 0.9 wt% NaCl solution. The NaCl solution was fed at a constant flux of 8 mL min<sup>-1</sup> while opening the cross-flow valve in order to dislodge any deposited bacterial cells from the surface of the membrane. At the end of 15 min cleaning cycle, an aliquot from cross-flow outlet was collected. The whole procedure was repeated 4 times in order to discern the reusability potential of the membrane. All of the collected aliquots were diluted to the appropriate concentration and enumerated on the agar plates. All data were obtained from at least three replicates of experimental runs.

### 3.4.8 Bacterial repair

In order to investigate the ability of bacteria to undergo repair, once the photocatalytic disinfection tests were completed, the treated bacterial suspension was collected and stored in the dark for 48 h. Aliquot of the suspension was spread evenly on the agar plate and enumerated to determine whether the bacteria could undergo dark repair after the photocatalytic disinfection.

# **CHAPTER 4 HIGH PERMEABILITY TiO<sub>2</sub> PHOTOCATALYTIC MEMBRANE WITH HIERARCHICAL POROSITY: FABRICATION, CHARACTERIZATIONS, AND PERFORMANCES**

## **4.1 Introductions**

The integration of heterogeneous photocatalysis and membrane treatment in a hybrid treatment system could be achieved either by separated membrane reactor with photoreactor operated in tandem or integrated membrane photoreactor (Lim et al. 2011). In each case, TiO<sub>2</sub> photocatalyst can be either used in a suspension or in an immobilized system. The former requires catalyst recovery after the photocatalytic treatment process. The latter suffers from mass transfer limitation and has a much smaller number of active sites compared to the former. By anchoring the TiO<sub>2</sub> photocatalyst onto a porous membrane support, or by confining it by means of a membrane, the issue of catalyst recovery can be solved. In addition, it also allows the synergistic coupling of photocatalytic reaction and membrane filtration which promotes mass transfer process through forced permeation. In this context, the crystallite size of the anchored TiO<sub>2</sub> photocatalyst must be optimized in order to achieve a high photocatalytic activity with low membrane resistance. Therefore, there is a need to produce a thin layer of nano-sized photocatalyst anchored on the highly porous membrane surface in order to maintain high water permeation through the membrane.

Ceramic membranes have many advantages as compared to the polymeric membranes such as excellent thermal, mechanical, chemical and biological stabilities, high permeability, easy cleaning, and resistance to UV irradiation (Anderson et al. 1988, Bhave 1991, Burggraaf

and Cot 1996, Chang et al. 1994, Guizard et al. 1992). In addition, during membrane cleaning, ceramic materials are resistant to various cleaning agents (e.g., chlorine, acid, and solvent) and they can be sterilized at higher temperatures. Furthermore, ceramic membranes possess a much longer life span compared to polymeric membranes.

Synergistic coupling of photocatalytic activity and membrane filtration was first investigated by Anderson et al. (1988) in which they investigated different sol-gel synthesis techniques to obtain a membrane with controllable pore size. Since then, there are many research efforts to improving the structure and performance of photocatalytic membrane. For instance, Zhang et al. (2006) found an increasing dye removal efficiency that coupled photocatalysis with membrane separation. Wang et al. (2008) developed a pure titania membrane using porous rutile as a support for both separation and photocatalytic degradation of methylene blue. Ma et al. (2009b) synthesized a thick Si-doped TiO<sub>2</sub> layer onto a tubular alumina membrane that showed promising flux and dye removal performance. Ding et al. (2006) fabricated a titania ultrafiltration membrane using a nanoparticle suspension that was effective in rejection of bovine serum albumin. Bosc et al. (2006) prepared a TiO<sub>2</sub> membrane on asymmetric tubular alumina membrane by incorporating polystyrene latex sphere and different amphiphilic molecules as mesostructure-directing agents. Choi et al. (2006d) developed a nanocrystalline TiO<sub>2</sub> membrane with hierarchical properties by using different types of surfactants as the pore forming agent.

Despite these important findings, synergistic coupling of photocatalysis and membrane filtration has long-standing issues which need to be addressed, i.e. the low water permeability and adverse loss of permeation flux over a prolonged usage due to fouling. Besides, there is a need to fine-tune the photocatalytic property and porosity of the membrane in order to obtain an optimum flux and high photocatalytic performance.

In this chapter, the fabrication and performance evaluation of TiO<sub>2</sub> photocatalytic membrane with hierarchical porosity which consists of multiple TiO<sub>2</sub> sub-layers with controllable pore structure is discussed. The overall flux performance could be enhanced by coating TiO<sub>2</sub> sub-layers of a larger porosity on the ceramic support leaving only a thin separating top sub-layer of a smaller porosity on the surface of the photocatalytic membrane. Pluronic P-123 triblock copolymer (hereafter referred as P-123) was incorporated into the TiO<sub>2</sub> sol to fine-tune the microstructure of the resulting gel. P-123 contains incompatible blocks that were able to form a periodic nanostructure via microphase separation. The preliminary investigation suggested that P-123 possessed a good miscibility with the organics solvent that would allow the formation of micellar structure. The resulting pore structure of TiO<sub>2</sub> thin films could be controlled by varying the amount of P-123 added into the TiO<sub>2</sub> sol. The dissolved pollutants could be photocatalytically degraded as they move along the illuminated TiO<sub>2</sub> surface layers.

Various characterization techniques were utilized to understand the physico-chemical and morphological characteristics of the membrane. The performances of the membrane were evaluated both using the batch photoreactor and the continuous flow PMR operated in the dead-end filtration mode. The experiments in batch reactor were performed to provide a quick performance evaluation of each type of membrane and for some experiment that may require a longer duration, while the experiments in the PMR were performed to simulate the real operation in a scale-up reactor.

## **4.2 Experimental procedures**

### **4.2.1 Membrane fabrication**

Six different TiO<sub>2</sub> sols were prepared by acid-catalyzed sol-gel method (Section 3.1.3) using P-123 as the SDA. The sols contained 0.5, 1, 2, 3, 5, and 10 wt% of P-123 respectively. The TiO<sub>2</sub> sols hereafter are referred as P-123-Xwt%, where X is the weight percentage of P-123 added. The TiO<sub>2</sub> sol without P-123 (denoted as P-123-0wt%) was also synthesized as a control.

The hierarchically porous P-123-based TiO<sub>2</sub> photocatalytic membrane was fabricated using layer-by-layer coating of different TiO<sub>2</sub> sols onto the alumina ceramic membrane support. The preparation of the membrane support and the fabrication of the photocatalytic membrane are delineated in Sections 3.1.2 and 3.1.5 respectively. In this hierarchical porous architecture, the porosity gradient was obtained through the coating of multiple photocatalytic layers of different pore structures starting from the layer of largest pore size on the support-photocatalyst interface, followed by the coating of subsequent layers of decreasing pore sizes, leaving only a thin separation layer of smallest pore size.

**Table 4.1** Types of P-123-based membrane fabricated

Types	Sub-layers Coated <sup>a</sup>			TiO <sub>2</sub> Loading (μg/cm <sup>2</sup> )	Thickness of TiO <sub>2</sub> Coating <sup>b</sup> (nm)
	1 <sup>st</sup> (bottom) Layer	2 <sup>nd</sup> Layer	3 <sup>rd</sup> (top) Layer		
Plu Control	0	0	0	69.1 ± 5.3	201 ± 21
Plu A	10-10-10	5-5-5	2-2-2	179.6 ± 10.0	896 ± 55
Plu B	10-10	5-5	2-2	123.4 ± 8.6	572 ± 37
Plu C	10	5	2	49.4 ± 5.2	245 ± 21
Plu D	10-10-10	5-5	2	130.3 ± 10.3	598 ± 38

<sup>a</sup> 0, 2, 5, and 10 indicated P-123-0wt%, 2wt%, 5wt%, and 10wt% respectively.

<sup>b</sup> Determined by considering different porosities of each sub-layers and assuming uniform density of anatase of 3.9 g.cm<sup>-3</sup>.

Different types of multi-layer TiO<sub>2</sub> photocatalytic membranes were prepared and summarized in Table 4.1. Each membrane specimen consists of 3 photocatalytic layers. Plu A consisted of 3 sub-layers of P-123-10wt%, followed by 3 sub-layers of P-123-5wt%, and finally 3 sub-layers of P-123-2wt%. Plu B and Plu C consisted of 2 sub-layers and 1 sub-layer of each type of sol respectively. Lastly, Plu D consisted of 3 sub-layers of P-123-10wt%, 2 sub-layers of P-123-5wt%, and a single sub-layer of P-123-2wt%. Plu Control, which consisted of 3 sub-layers of P-123-0wt%, was also prepared as control for the evaluation of membrane performance.

#### **4.2.2 Characterization techniques**

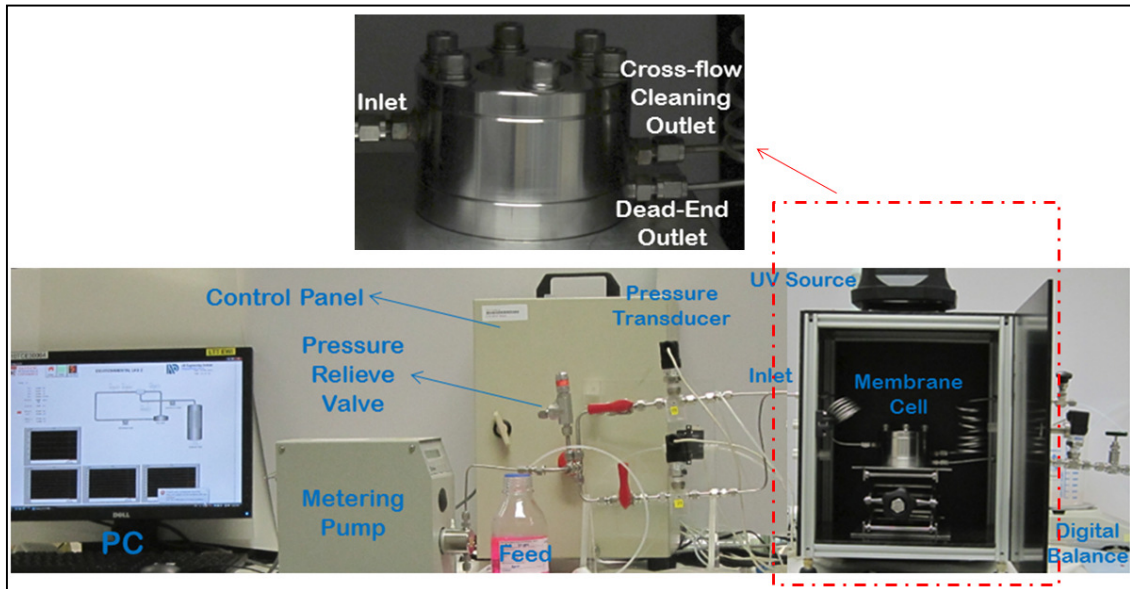
Various characterization techniques were used to understand physico-chemical and morphological properties of the membrane (the detailed description of the instrumentation and methodology are presented in Section 3.3). Viscosity of the sol was determined through rheological measurement. Characterization techniques used for the pulverized TiO<sub>2</sub> layer were: N<sub>2</sub> adsorption/desorption (for porosimetry analysis) and XRD. The surface morphological characteristic of the membrane was studied using FESEM. Finally, the photo-induced super-hydrophilicity property of the membrane was observed through the contact angle measurement.

#### **4.2.3 Evaluation of membrane performance**

The photocatalytic activity of the membrane in the batch photoreactor (Section 3.4.2) and the PMR (Section 3.4.3) was evaluated against RhB, a common tracer dye and bio-marker which was used as the model pollutant in this study. In a typical experiment using the batch photoreactor, each type of membrane specimens was used to treat 12 mL of RhB solution

without any stirring and oxygen bubbling. The extent of the photodegradation of RhB was monitored using UV/Vis spectrophotometer at 553 nm.

The PMR setup (Fig. 4.1) was used to evaluate the performance of the membrane while operating in the dead end filtration mode. The coated membrane disc was mounted and secured tightly in the membrane cells (Fig 3.6). The pure water permeability and the MWCO of the membrane were evaluated using the PMR. The membrane was also used to treat up to 5 cycles of 100 mL of 25  $\mu$ M RhB solution. The overall RhB removal could be differentiated to 2 different processes: adsorptive-membrane retention (Ads-MR) and photocatalytic activity of TiO<sub>2</sub> (PCA) by the membrane. Control experiments without turning on the UV source were performed to elucidate the effect of Ads-MR on the removal of RhB. Fouling-control property of TiO<sub>2</sub> photocatalytic membrane was examined in the PMR setup for 12 h without re-circulation of the permeate.



**Figure 4.1** Image of the PMR reactor.

## 4.3 Results and discussion

### 4.3.1 Physico-chemical characteristics of sols

The as-synthesized TiO<sub>2</sub> sols were transparent and showed good stability in continuous stirring condition at room temperature. TiO<sub>2</sub> sols with the addition of P-123 were relatively more stable over prolonged period of time as compared with P-123-0wt% sol which was only stable for 1 d before it turned chalky. The viscosity of the sols decreased from 0.054 mPa.s for P-123-0wt% to 0.006 mPa.s for P-123-10wt%. This showed that the addition of P-123 lowered the viscosity of the resulting sol and this phenomenon was crucial in fabricating uniform TiO<sub>2</sub> layers with minimal cracks and pinholes.

**Table 4.2** Physico-chemical characteristics of the as-synthesized TiO<sub>2</sub> layers

Parameters	Layers			
	P-123-0wt%	P-123-2wt%	P-123-5wt%	P-123-10wt%
BET specific surface area (m <sup>2</sup> g <sup>-1</sup> )	12.1 ± 0.4	83.3 ± 1.0	146.6 ± 1.1	200.6 ± 0.9
Pore volume (cm <sup>3</sup> g <sup>-1</sup> ) <sup>a</sup>	0.035 ± 0.01	0.14 ± 0.02	0.27 ± 0.01	0.36 ± 0.01
BJH <sub>ads</sub> pore diameter (nm)	3.11 ± 0.02	5.64 ± 0.02	6.24 ± 0.10	6.55 ± 0.10
BJH <sub>des</sub> pore diameter (nm)	3.83 ± 0.30	4.36 ± 0.50	5.15 ± 0.40	5.63 ± 0.40
Average pore diameter (nm) <sup>b</sup>	4.28 ± 0.20	6.32 ± 0.40	6.86 ± 0.50	7.12 ± 0.40
BET porosity (%) <sup>c</sup>	11.9 ± 0.3	35.0 ± 0.4	51.5 ± 0.4	58.1 ± 0.4
XRD crystallite size (nm) <sup>d</sup>	14	11	7	6
Viscosity (mPa s) <sup>e</sup>	0.0535	0.0247	0.0094	0.0060

<sup>a</sup> Calculated from BJH desorption curve.

<sup>b</sup> Calculated from BJH desorption curve, and indicating average pore size between primary particles.

<sup>c</sup> Determined by assuming uniform density of anatase of 3.9 g.cm<sup>-3</sup>.

<sup>d</sup> Calculated using Scherrer's equation with error < 1 nm.

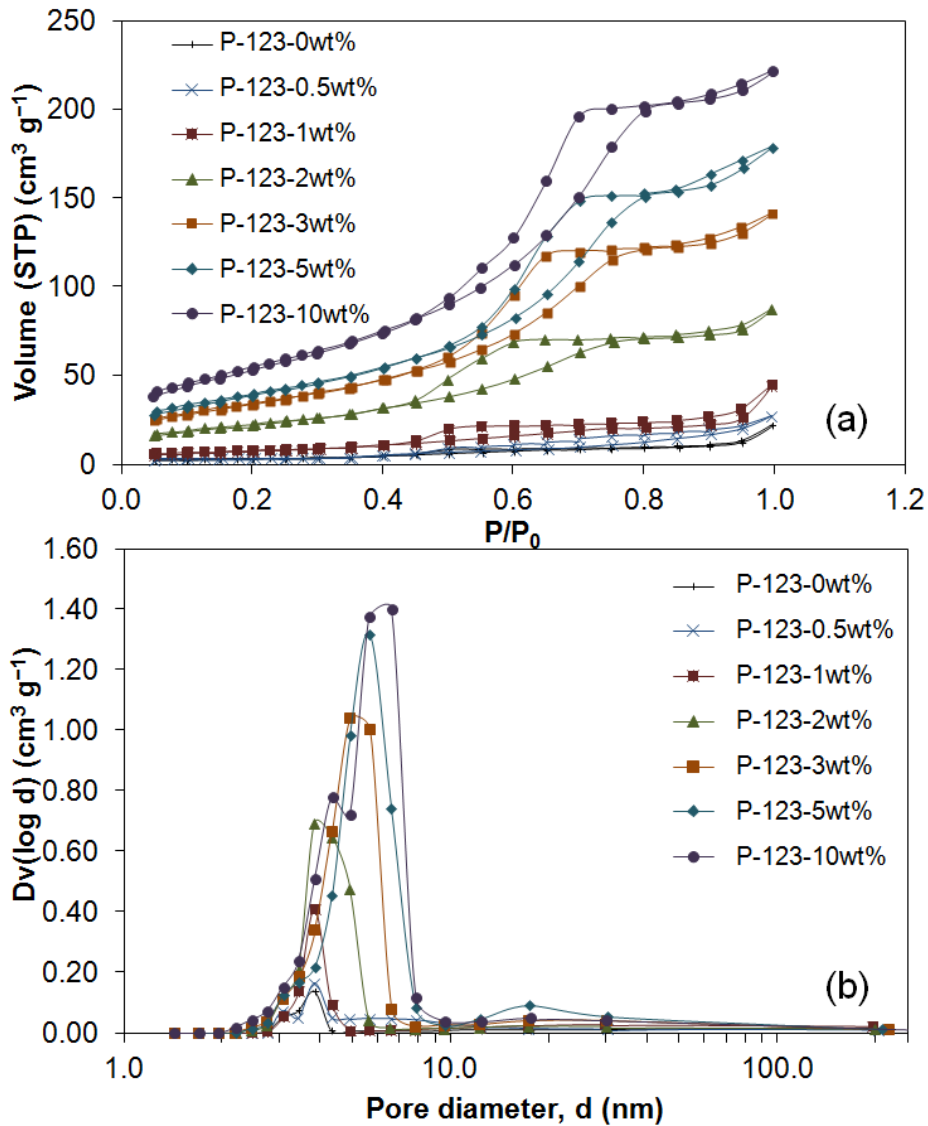
<sup>e</sup> As recorded at the shear rate of 50 s<sup>-1</sup>.

The values of important physico-chemical parameters of the as-synthesized TiO<sub>2</sub> layers are summarized in Table 4.2. Self-organized TiO<sub>2</sub> nanoparticles have been successfully

synthesized via acid-catalyzed sol-gel method using P-123 as the SDA. P-123 formed micellar structure via microphase separation due to the difference in hydrophilicity between the polyethylene glycol and polypropylene glycol blocks of the molecules. Attractive forces between TiO<sub>2</sub> hydrate and P-123 formed the mesoporous structure that was crystallized at elevated temperature to form the final oxide (Lu et al. 1997, Procházka et al. 2008). During the heat treatment, P-123 and other organic residue (i.e. IPA) were removed, leaving TiO<sub>2</sub> nanocrystals embedded in the mesoporous structure.

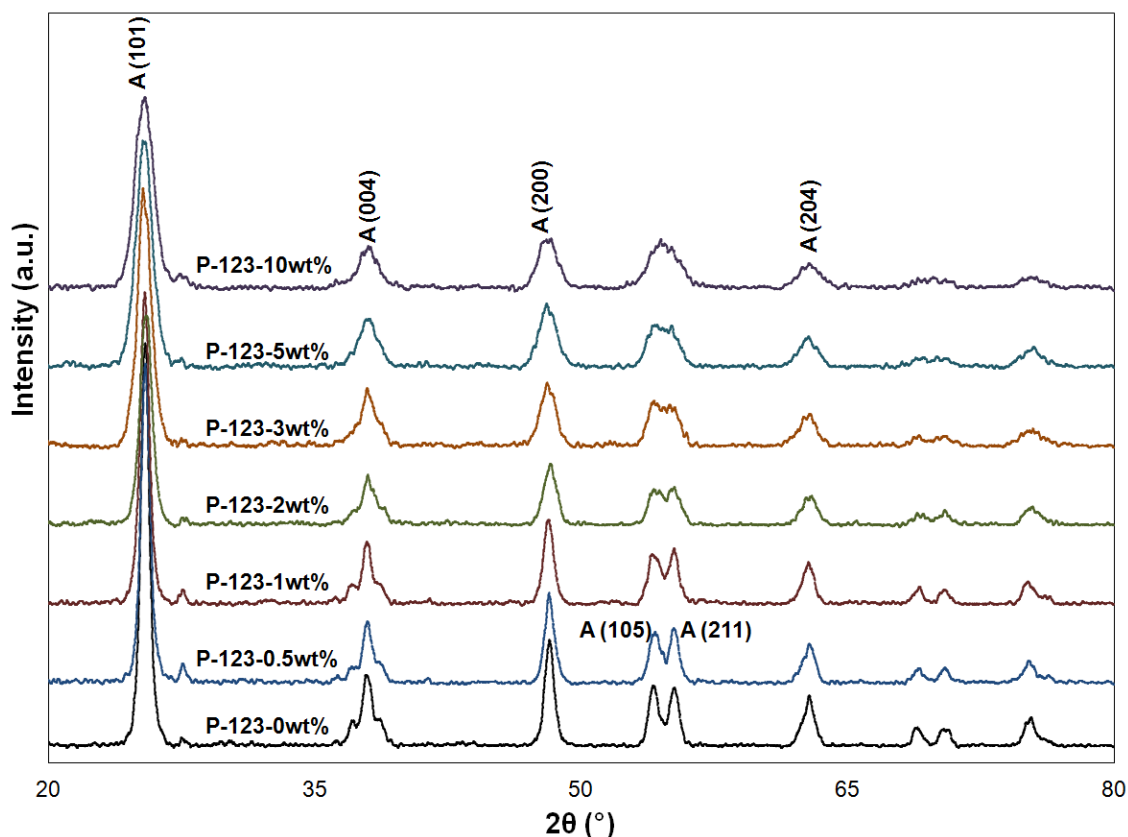
The ability of the SDA to fine-tune the pore size of the synthesized TiO<sub>2</sub> layers was evaluated via N<sub>2</sub> adsorption/desorption isotherms characterization and the result is summarized in Table 4.2. Fig. 4.2a shows that P-123-based TiO<sub>2</sub> layers exhibited a type-IV adsorption isotherm, indicative of well developed mesoporous materials. The difference in the shapes of adsorption and desorption branches of the hysteresis loop could be ascribed to the presence of smaller pores in the titania layers which caused a sharp drop in the desorption branch (Ravikovitch and Neimark 2002). A relatively similar average pore diameter obtained from the BJH adsorption and desorption branches indicates good homogeneity of the pore structures. Table 4.2 shows that as the amount of P-123 increased, the pore size, surface area, and porosity of the TiO<sub>2</sub> layers increased. BET specific surface area of the TiO<sub>2</sub> layers were enhanced from 12.1 m<sup>2</sup> g<sup>-1</sup> for P-123-0wt% to 200.6 m<sup>2</sup> g<sup>-1</sup> for P-123-10wt%, a 16-fold increase in the surface area by just adding 10 wt% of P-123 as the SDA. By assuming a uniform anatase density of 3.9 g cm<sup>-3</sup>, similar trend was also observed for the porosity of TiO<sub>2</sub> layers which showed an increase from 12% for (P-123-0wt%) to 57% (for P-123-10wt%). Higher P-123 concentration caused more pore coalescence and multi-micellar interactions during heat treatment which would result in relatively large pores and high porosity (Choi et al. 2006d).

Fig. 4.2b depicts absence of bimodal pore size distribution which suggests a good uniformity and stability of the sols. BET porosimetry results indicated that by varying the amount of P-123 added, fine-tuning the pore structure of the resulting TiO<sub>2</sub> layers could be achieved. This would allow the fabrication of a hierarchically porous membrane through layer-by-layer deposition of TiO<sub>2</sub> layers of different pore sizes.



**Figure 4.2** (a) N<sub>2</sub> adsorption/desorption curves and (b) pore size distribution of the pulverized TiO<sub>2</sub> layers with different amounts of P-123 added.

The wide-angle XRD spectra of the pulverized P-123-based TiO<sub>2</sub> sols with different amounts of P-123 added are shown in Fig. 4.3. The XRD spectra show five distinctive TiO<sub>2</sub> peaks at 25.3°, 37.9°, 48°, 54.6°, and 62.8° which correspond to (101), (004), (200), (105 and 211), and (204) of crystalline anatase planes respectively (JCPDS 21-1272). No rutile and brookite phases were observed. This indicates that all the P-123-based TiO<sub>2</sub> layers prepared were pure nanocrystalline anatase which was the most photocatalytically active and photostable form of TiO<sub>2</sub> (Gaya and Abdullah 2008, Tanaka et al. 1993b). No amorphous content of the TiO<sub>2</sub> was observed upon calcination indicating that calcination at 500°C was sufficient to induce the formation of anatase crystals (Mazzarino et al. 1999).



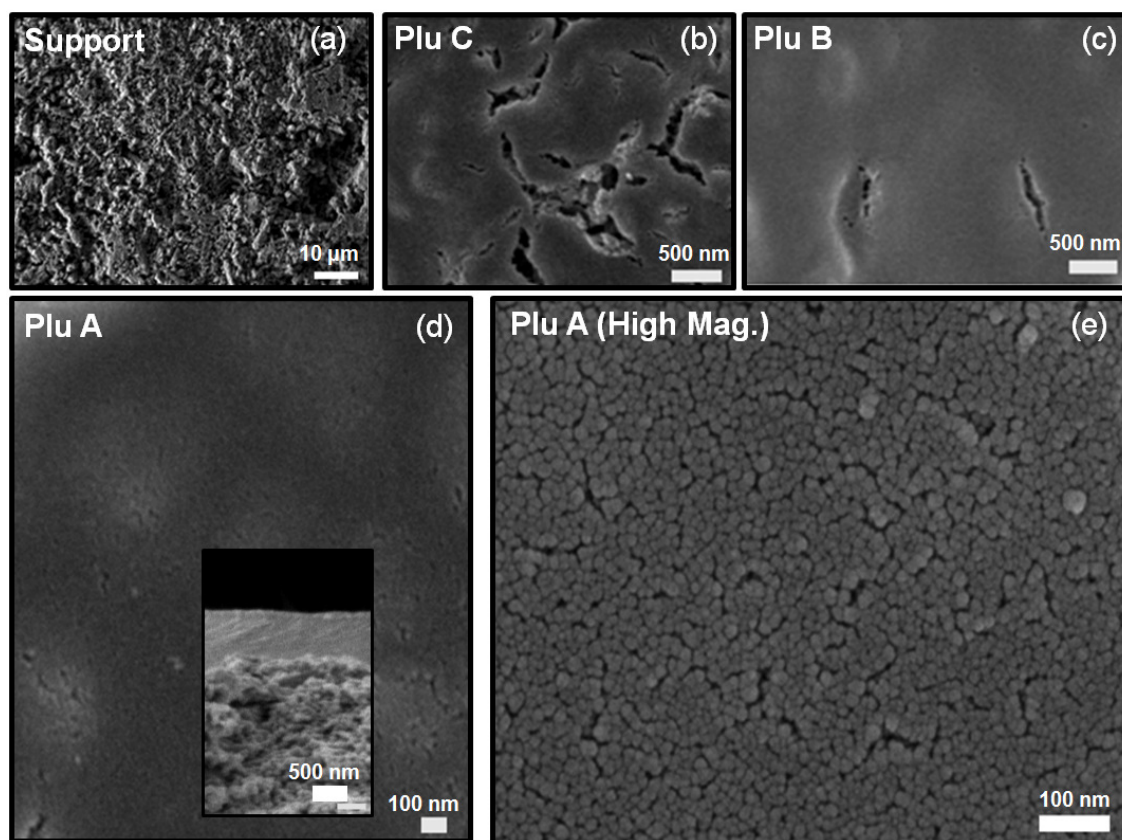
**Figure 4.3** XRD spectra of the pulverized TiO<sub>2</sub> layers with different amounts of P-123 added.

Scherrer's equation (Scherrer 1918) is used to calculate  $\text{TiO}_2$  crystallites size from the peak broadening of (101) anatase crystal plane at  $25.3^\circ$ . As shown in Fig. 4.3, with increasing concentration of P-123 loading, the intensity of (101) diffraction peak becomes weaker and the FWHM (full width at half maximum) becomes wider, indicating that the  $\text{TiO}_2$  grain sizes become smaller. Nanocrystalline  $\text{TiO}_2$  was synthesized to ensure a higher overall surface area or denser active catalytic sites of the photocatalyst, which is crucial for achieving a higher photocatalytic activity. However, excessively small crystallite size would cause a blue shift in the absorption spectrum and also induce surface recombination of photo-excited electrons and holes (Anpo et al. 1987, Henglein 1982). The derived  $\text{TiO}_2$  crystallite size varied from 14.4 nm for P-123-0wt% to 6.47 nm for P-123-10wt% (Table 4.2). The sizes of as-synthesized  $\text{TiO}_2$  crystals are close to the optimum  $\text{TiO}_2$  crystallite size for the highest photocatalytic activity as reported in the literature (i.e.  $\sim 10$  nm) (Zhang et al. 1998). It has been observed that the crystallinity of  $\text{TiO}_2$  decreases as the amount of P-123 loading increases. This was evidenced by the overlapping of anatase (105) and (211) reflections on samples with higher P-123 loadings. This highlights the role of the P-123 in limiting the growth of  $\text{TiO}_2$  crystals via spatial confinement mechanism (Guldin et al. 2011).  $\text{TiO}_2$  anatase network was assembled into an ordered spatial confinement which maintained the structural integrity of the P-123 scaffold.

#### **4.3.2 Characteristics of $\text{TiO}_2$ layers**

$\text{TiO}_2$  photocatalytic membrane was fabricated via layer-by-layer deposition of  $\text{TiO}_2$  of different porosities. Morphological study of the synthesized membrane could provide a better understanding of the coating process, which is important for tailoring the desired membrane performance. Fig 4.4a shows FESEM micrograph of unpolished support which shows a

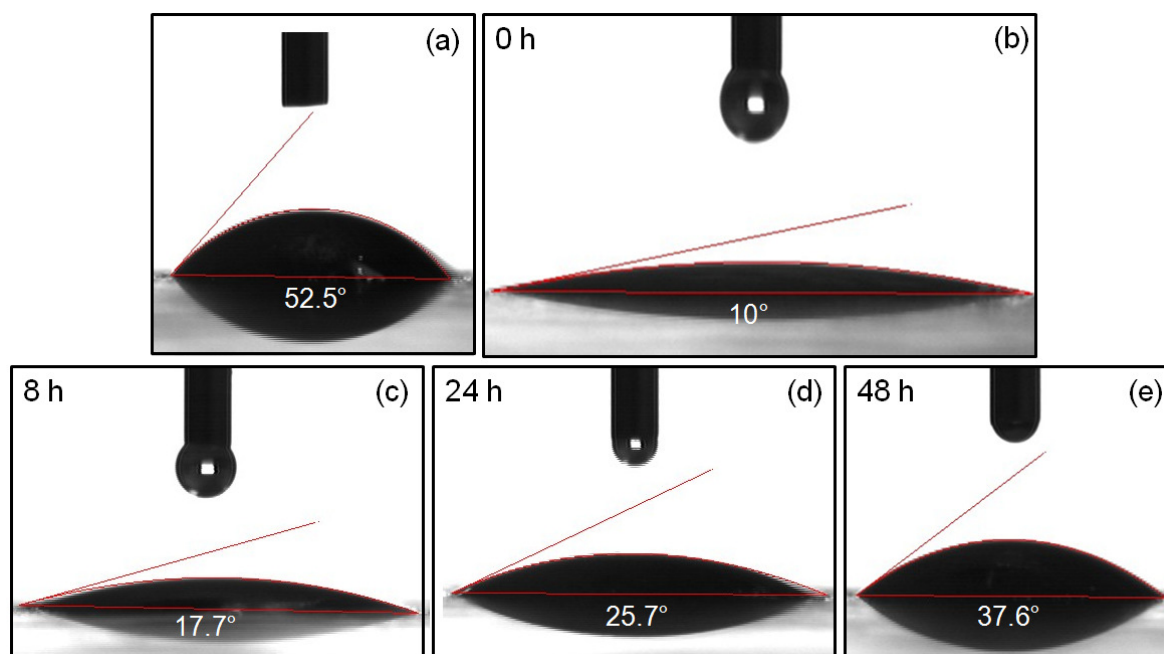
coarse packing of alumina particles. The support required polishing and PVA layering prior to the coating of TiO<sub>2</sub> sols. The thin PVA coating functioned both as the pores fillers, which prevent TiO<sub>2</sub> sol infiltration to the support, as well as the temporary binder between TiO<sub>2</sub> and the support material. As a binder, PVA increases the strength of the membrane layer (Alem et al. 2009b, Habibi et al. 2007a).



**Figure 4.4** SEM micrograph of surface of (a) alumina substrate, (b) Plu C, (c) Plu B, and Plu A membrane at (d) low and (e) high magnification (the inset in (d) depicts cross-sectional view of Plu A membrane).

Figs 4.4b and 4.4c show the surface morphology of Plu C and Plu B membrane respectively. Infrequent cracks and pinholes were evident in Plu C membrane probably due to

the thin  $\text{TiO}_2$  sub-layers that expand unequally during the calcination process. The cracks and pinholes formation were greatly reduced in Plu B membrane when each type of  $\text{TiO}_2$  sols were coated 2 times. The initial coating of the same type of sol functioned as an intermediate layer that smoothen the membrane surface for the subsequent coating. Fig 4.4d shows the FESEM micrograph of the surface of the Plu A membrane which shows a relatively smooth  $\text{TiO}_2$  layer coating on the alumina support. The  $\text{TiO}_2$  layer consists of ordered arrangement of  $\text{TiO}_2$  nanocrystals (as shown in magnified micrograph of Fig. 4.4e) with minimum presence of cracks or pinholes on its surface. This is important to ensure that the membrane has a uniform permeability and membrane retention characteristics. The cross-sectional view of Plu A membrane (inset in Fig. 4.4d) shows that distinct  $\text{TiO}_2$  layers were successfully coated on the support. The overall thickness of the  $\text{TiO}_2$  layers is around  $1\ \mu\text{m}$ .



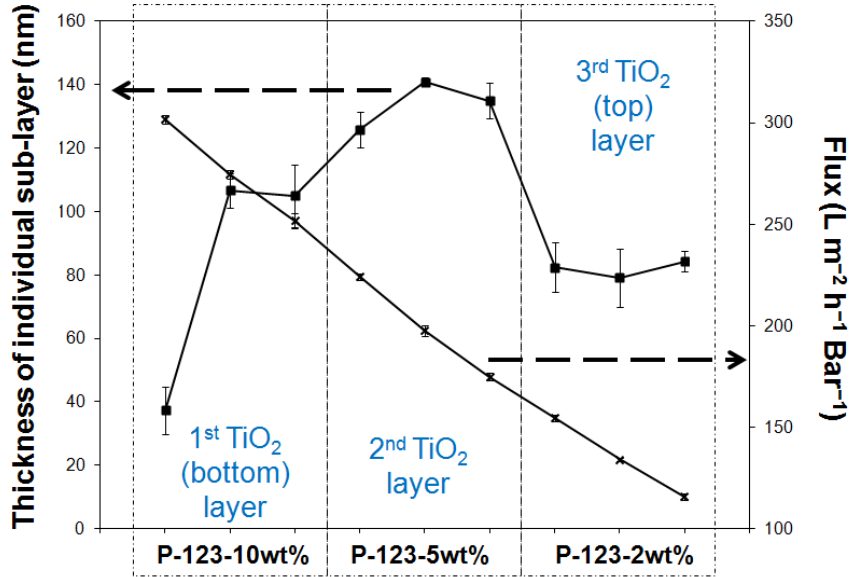
**Figure 4.5** Photoinduced super-hydrophilicity behavior of Plu A film coated on a borosilicate glass as shown on (a) as-coated sample, (b) upon 1 h of UV irradiation, and after (c) 8 h, (d) 24 h, and (e) 48 h left in the dark.

Photo-induced super-hydrophilicity (PSH) is another important characteristic for a good TiO<sub>2</sub> photocatalytic membrane. The contact angle micrographs and their corresponding values are shown in Fig. 4.5. The as-coated P-123-10wt% thin film shows a contact angle of 52.5° which subsequently decreased to 10° after 1 h of UV irradiation. When the UV lamp was switched off, the contact angle increased again to 17.7°, 25.7° and 36.7° after 8, 24, and 48 h respectively. PSH is caused by the hydroxylation of film surface upon UV irradiation. Photo-generated electrons react with lattice metal ions Ti<sup>4+</sup> to form Ti<sup>3+</sup> defective sites. Surface-trapped electron in Ti<sup>3+</sup> will react immediately with oxygen adsorbed on the surface to form O<sub>2</sub><sup>-</sup> or O<sub>2</sub><sup>2-</sup> ions leaving the oxygen vacancy sites (Sakai et al. 2003). Even if it was present in almost negligible amount, adsorbed water molecules would occupy the vacancy sites to reduce the surface energy, which in turn would release proton to a nearby oxygen atom and forms two hydroxyl groups at the surface of the photocatalyst.

#### **4.3.3 Pure water permeability of P-123-based TiO<sub>2</sub> photocatalytic membrane**

Fig. 4.6 shows the cumulative thicknesses of TiO<sub>2</sub> layers and the resulting pure water flux of Plu A membrane (Table 4.1) after each sub-layer coating. Layer thickness is calculated by measuring the incremental weight of the membrane after each sub-layer coating by considering the porosity of each sub-layer and assuming a uniform anatase density of 3.9 g cm<sup>-3</sup>. First P-123-10wt% sub-layer is a very thin layer (37 nm) coated on the PVA-filled alumina ceramic support. The initial thin layer could be attributed to the poor adhesion of P-123-10wt% to the PVA-filled alumina support. Subsequent coatings of P-123-10wt% layers yield a relatively similar thickness of 100 nm. A more viscous P-123-5wt% sol was used for forming the subsequent 3 middle TiO<sub>2</sub> sub-layers with average thicknesses of 125, 140, and 134 nm respectively. At this stage, the membrane was relatively smooth so that the addition of the final 3 sub-layers of P-123-2wt% yields relatively thinner sub-layers of 82, 79, and 84

nm, bringing a total thickness of the TiO<sub>2</sub> layers of Plu A membrane to 0.9 μm. This estimation is consistent with the observation using SEM which shows an overall thickness of 1 μm for the TiO<sub>2</sub> layer coated on the alumina support. The pure water flux of Plu A membrane decreased steadily with the increased number of sub-layer coated, from initial 300 L m<sup>-2</sup> h<sup>-1</sup> Bar<sup>-1</sup> to the final 120 L m<sup>-2</sup> h<sup>-1</sup> Bar<sup>-1</sup> after 9 TiO<sub>2</sub> sub-layers being coated.



**Figure 4.6** TiO<sub>2</sub> layer thickness and the resulting pure water flux of Plu A membrane with respect to the different sub-layers coated.

Fig. 4.7 shows pure water flux and PEG retention of the TiO<sub>2</sub> photocatalytic membrane. MWCO of the TiO<sub>2</sub> photocatalytic membrane was evaluated using 500 mg L<sup>-1</sup> PEG solutions with molecular weights ranging from 1,500-20,000 g mol<sup>-1</sup>. The 20,000 g mol<sup>-1</sup> PEG solution corresponds to PEG molecular size of 12 nm (Choi et al. 2006a). Only Plu A membrane showed an efficient retention of PEG with MWCO of 12,000 g mol<sup>-1</sup> which corresponds to pore size of 7 nm. This MWCO value is in good agreement with the result obtained from N<sub>2</sub> porosimetry analysis. Plu B and Plu C showed lesser retention of PEG which could be attributed to the lesser number of TiO<sub>2</sub> sub-layers coated (Table 4.1). Plu D showed lower

PEG retention when compared with Plu B which also consisted of a total of 6 TiO<sub>2</sub> layers but with a different porosity gradient. This can be explained by the thicker P-123-2wt% sub-layer in Plu B (2 sub-layers of P-123-2wt% in Plu B as compared to 1 sub-layer of P-123-2wt% in Plu D). Plu Control showed a better PEG retention as compared to Plu C which could be attributed to the smaller pore size and porosity of Plu Control (reflected by P-123-0wt% in Table 4.2).

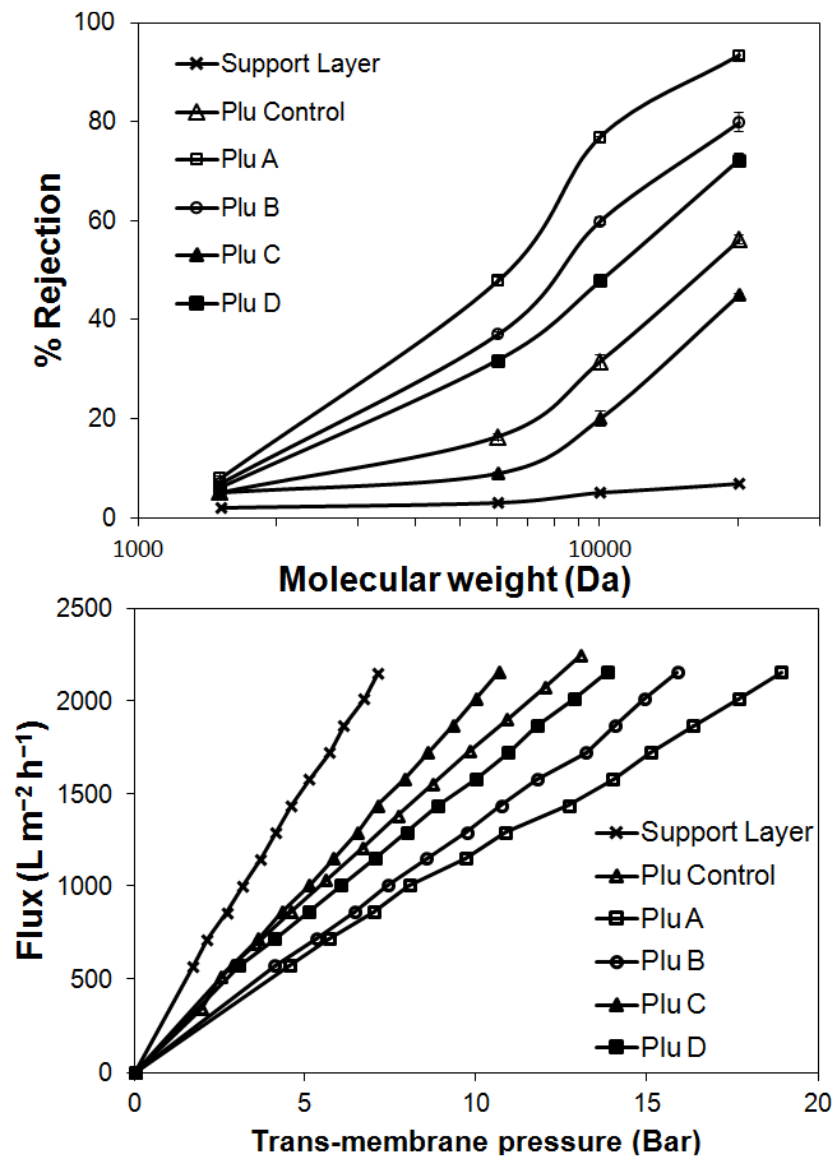


Figure 4.7 (a) PEG retention and (b) pure water permeability of P-123-based TiO<sub>2</sub> photocatalytic membrane.

Fig. 4.7b shows that the water permeability flux increases linearly with the TMP regardless of the type of TiO<sub>2</sub> layer deposited. The pure water permeability of Plu C membrane was 202 L m<sup>2</sup> h<sup>-1</sup> Bar<sup>-1</sup> which was slightly lower than that of the support layer (309 L m<sup>2</sup> h<sup>-1</sup> Bar<sup>-1</sup>). This showed that TiO<sub>2</sub> layers in the Plu C membrane formed a very thin porous film which only induced a minimal effect on the membrane filtration resistance. The effect of the coated layers on the pure water permeability can be evaluated by its intrinsic membrane resistance, R<sub>m</sub> (m<sup>-1</sup>), as defined below:

$$R_m = \frac{(\Delta P)At}{\mu V} \quad (4.1)$$

where  $\Delta P$  is the TMP (Pa),  $\mu$  is the kinematic viscosity of the liquid ( $1 \times 10^{-3}$  Pa s),  $V$  is the volume (m<sup>3</sup>) of liquid flowing through the membrane,  $A$  (m<sup>2</sup>) is the surface area of the membrane and  $t$  is the filtration time (s).

The intrinsic membrane resistance of the ceramic support layer is  $1.17 \times 10^{12}$  m<sup>-1</sup>. As the number of sub-layers of each types of the sol coated increased from 1 sub-layer (Plu C), 2 sub-layers (Plu B), and 3 sub-layers (Plu A), the corresponding intrinsic membrane resistance increased from  $1.79 \times 10^{12}$  m<sup>-1</sup> to  $3.11 \times 10^{12}$  m<sup>-1</sup>. As the structure of the 6 sub-layered membrane was varied, a lower intrinsic membrane resistance (higher pure water permeability) was obtained for Plu D membrane ( $R_m = 2.25 \times 10^{12}$  m<sup>-1</sup>) as compared to Plu B membrane ( $R_m = 2.68 \times 10^{12}$  m<sup>-1</sup>). This could be attributed to a thinner top separation layer (P-123-2wt%) of Plu D which allowed a higher flux. It has been found that the intrinsic membrane resistance of the P-123-based TiO<sub>2</sub> photocatalytic membrane is significantly lower than those reported in the literature (Choi et al. 2006d). The low intrinsic membrane resistance or high water permeability flux could be attributed to the photo-induced super-hydrophilicity property of the TiO<sub>2</sub> membrane. This is very important for membrane separation process, i.e.

high flux reduces the overall energy consumption in the water and wastewater treatment processes.

#### 4.3.4 P-123-based TiO<sub>2</sub> photocatalytic membrane performances

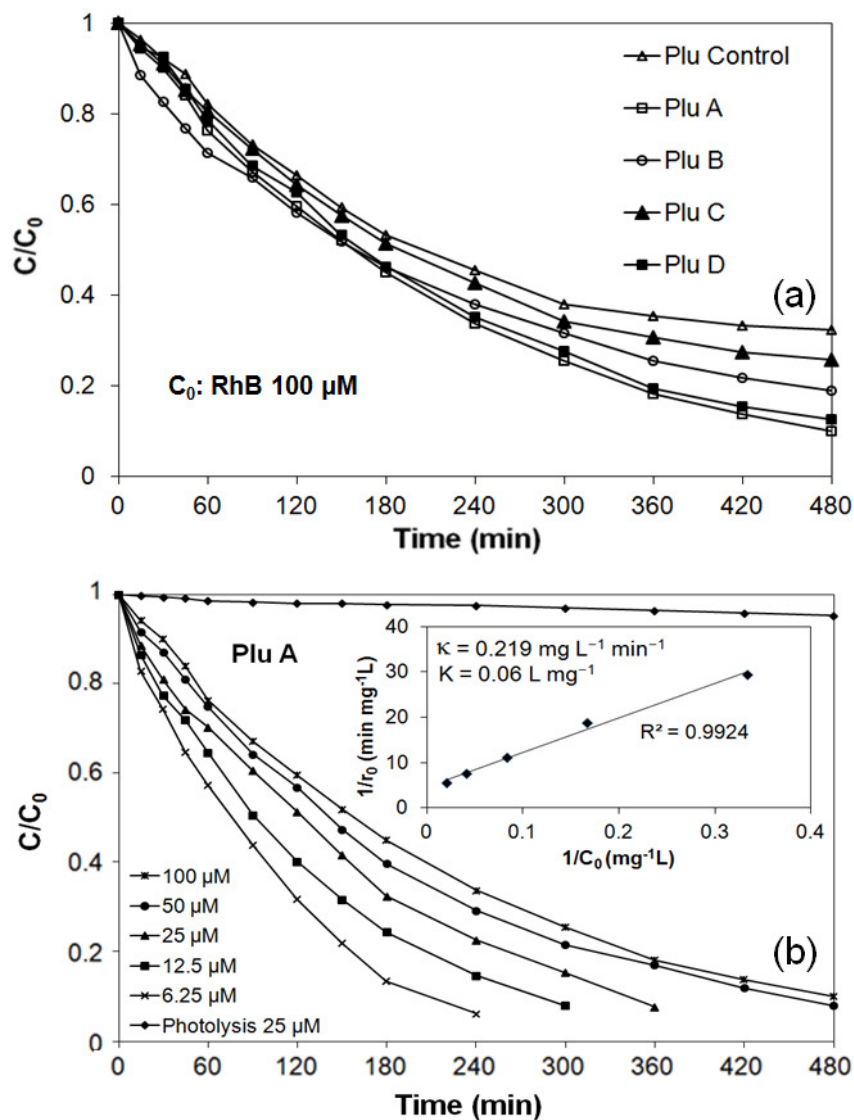
##### 4.3.4.1 Photocatalytic activity using batch photoreactor

Batch experiments were carried out to evaluate the photocatalytic activity of different structures of TiO<sub>2</sub> photocatalytic membrane and the results are presented in Fig. 4.8a. For a total degradation time of 8 h, Plu A membrane was able to remove > 90% RhB. Plu B and C removed 81% and 75% RhB respectively, which could be attributed to their lesser amount of TiO<sub>2</sub> coated on the membrane. Plu D removed 88% of initial RhB concentration, higher than that of Plu B which was also consist of 6 layers but in different structures. Plu Control showed the least amount of RhB removal (68%) which could be attributed to its smaller overall surface area of the membrane whereby RhB could be adsorbed and photodegraded. Plu A membrane was chosen as a representative sample to study the kinetics of RhB degradation and the results are presented in Fig. 4.8b. The photolysis of RhB at 25 μM under continuous UV irradiation (without the presence of the membrane) was < 5 %. In the presence of photocatalytic membrane, mass transfer rate, intra-layer pollutant diffusion, and adsorption/desorption equilibrium would affect the rate of RhB photocatalytic degradation by the membrane.

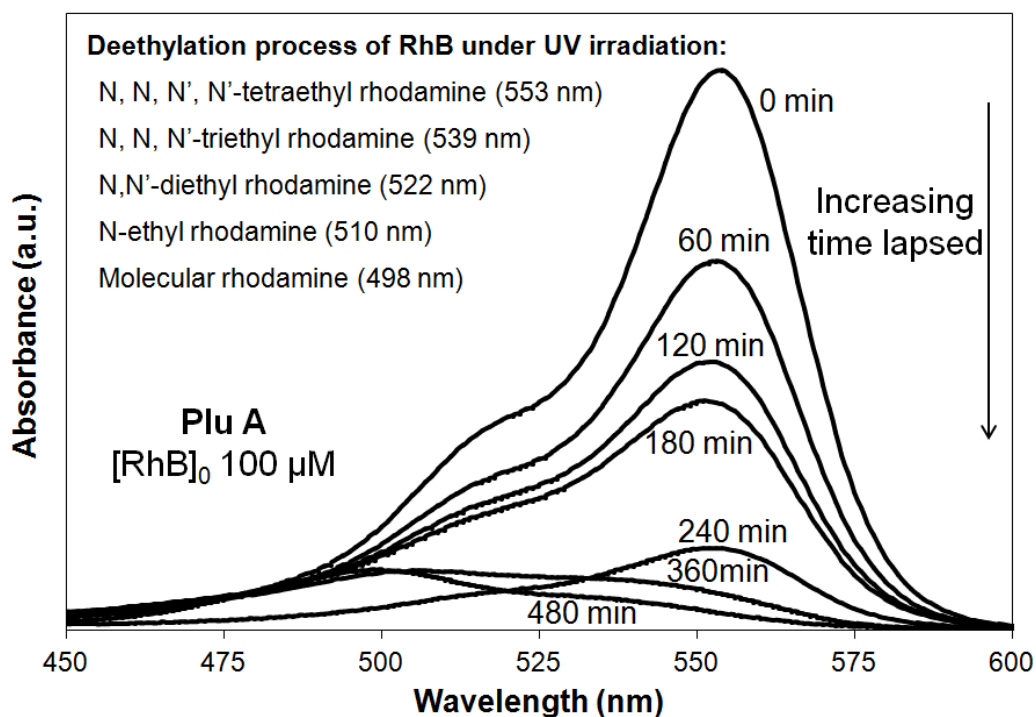
Generally, a pseudo-first order kinetic model can be used to model such photocatalytic degradation process. However, using this model, the derived reaction rate constant decreased with increasing initial concentration (6.25 to 100 μM RhB solution). Therefore, Langmuir-Hinselwood model (Eq. 4.2) is adopted to evaluate the RhB degradation kinetics.

$$\frac{1}{r_o} = \frac{1}{\kappa K} \frac{1}{C_o} + \frac{1}{\kappa} \quad (4.2)$$

where  $r_0$  is the initial reaction rate ( $\text{mg L}^{-1} \text{min}^{-1}$ ),  $\kappa$  the Langmuir-Hinshelwood reaction rate constant ( $\text{mg L}^{-1} \text{min}^{-1}$ ), and  $K$  the Langmuir adsorption constant ( $\text{L mg}^{-1}$ ). The inset of Fig. 4.8b shows the good fit and the derived values of  $\kappa$  and  $K$  was  $0.219 \text{ mg L}^{-1} \text{min}^{-1}$  and  $0.06 \text{ L mg}^{-1}$  respectively with  $R^2 > 0.99$ .



**Figure 4.8** Batch result of photocatalytic activity of (a) different configurations of  $\text{TiO}_2$  photocatalytic membrane and (b) Plu A membrane at different initial concentrations of RhB (the inset depicts the linear plot of Langmuir-Hinshelwood model).

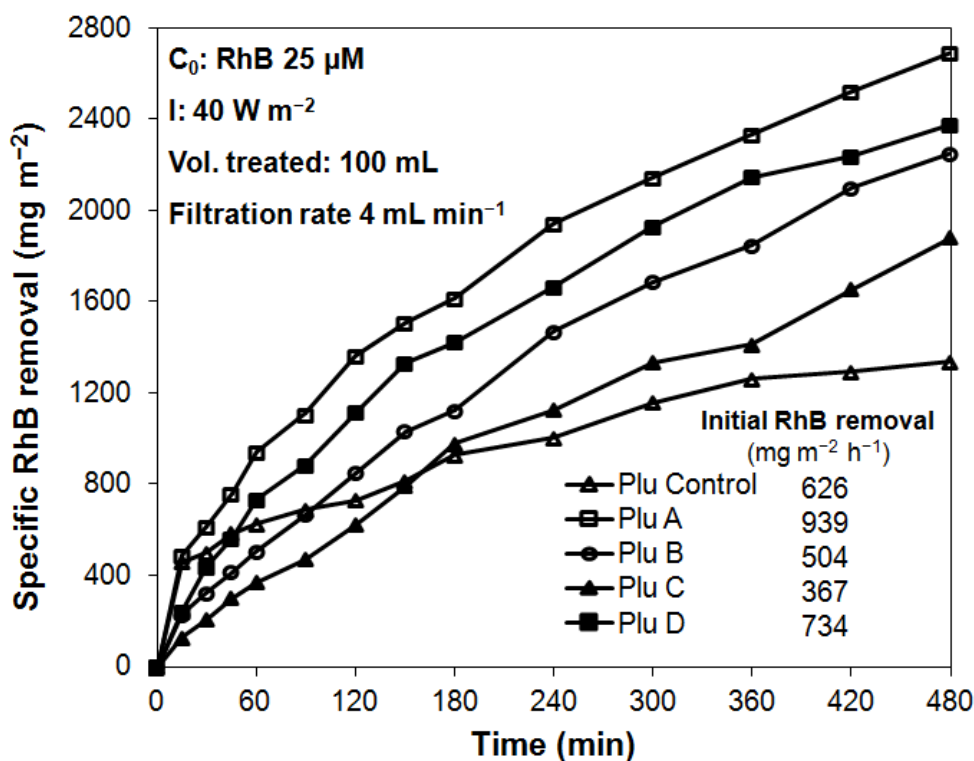


**Figure 4.9** Shift of RhB maximum light absorption peak over the duration of the photocatalytic degradation process.

RhB degradation can be monitored by shifting of RhB light absorption over the duration of photocatalytic degradation experiment. Fig. 4.9 shows time-dependent profile of RhB light absorption (from 600-450 nm) for 100 μM RhB solution photodegraded using Plu A membrane in the batch photoreactor. During the degradation process under UV irradiation, the maximum RhB absorption peak shifts gradually from 553 to 498 nm. The observed color of the RhB solution also changes from the initial red to a light greenish-yellow and finally to a transparent solution. This was due to the step-wise ethyl dissociation (de-ethylation) from N, N, N', N'-tetraethyl rhodamine (553 nm), N, N, N'-triethyl rhodamine (539 nm), N, N'-diethyl rhodamine (522 nm), N-ethyl rhodamine (510 nm) to form a final rhodamine molecules (498 nm) (Xie et al. 2009). It was worth noting that the photodecolorization of

chromogenic aromatic ring and dissociation of ethyl occurred simultaneously under UV irradiation. The TOC of treated RhB solutions from the batch photoreactor was measured to determine the extent of mineralization. It has been found that all the treated solutions showed a final TOC concentration  $< 1 \text{ mg L}^{-1}$  which was the detection limit of the equipment. This finding indicated  $> 90\%$  TOC removal from the initial RhB solution (from theoretical TOC of  $33.6 \text{ mg L}^{-1}$  for  $100 \text{ }\mu\text{M}$  solution).

#### 4.3.4.2 Photocatalytic activity and flux performance using PMR



**Figure 4.10** Specific RhB removal of Pluronic-based  $\text{TiO}_2$  photocatalytic membrane (the numerical values depict kinetic value based on initial RhB removal rate within  $1^{\text{st}}$  hour in  $\text{mg m}^{-2} \text{ h}^{-1}$ ).

The results of PMR experiments operated in the dead-end filtration mode are shown in Figs. 4.10 to 4.12. The specific RhB removal efficiency (i.e. the cumulative RhB removal per

unit area of membrane over the 8 h duration of experiments in the PMR,  $\text{mg m}^{-2}$ ) by the  $\text{TiO}_2$  photocatalytic membrane of different layered structures is illustrated in Fig. 4.10. The numerical values shown in Fig. 4.10 depict the initial rate of RhB removal. Plu A showed highest specific RhB removal of  $2700 \text{ mg m}^{-2}$  at 480 min. Plu B and Plu C showed declines in specific RhB removal (17% and 31% respectively) compared to Plu A. This can be attributed to the lesser amount of photocatalysts present on the surface of Plu B and Plu C. Plu D showed specific RhB removal of  $2400 \text{ mg m}^{-2}$ . Interestingly, although Plu D and Plu B have the same number of layers (i.e. 6 layers), the specific RhB removal of Plu D is higher than that of Plu B due to the different configurations of their layered structure.

The overall RhB removal could be itemized into 2 different phenomena i.e. photocatalytic activity (PCA) of  $\text{TiO}_2$  and adsorptive-membrane retention (Ads-MR) and they were summarized in Table 4.3. The overall contribution of Ads-MR of RhB to the membrane was relatively small with the exception of Plu Control (47.9%) and Plu A (22.2%, due to its larger  $\text{TiO}_2$  loading). Plu Control showed a largest percentage (47.9%) removal of RhB through Ads-MR (which could explain the high RhB removal efficiency at the initial stage of the PMR experiment) while Plu C, the thinnest membrane showed the smallest contribution of Ads-MR. The contribution of Ads-MR to the overall RhB removal by Plu D was smaller than that of Plu B which could be attributed to its hierarchical porous structure. All of the P-123-based  $\text{TiO}_2$  photocatalytic membranes showed a large contribution (up to 88%) of PCA to the overall removal of RhB. These results suggest that by tailoring the porosity gradient of the layered structure, the overall membrane performance could be improved. Membrane with more porous layers near the support exhibited a better RhB separation and water permeability characteristic.

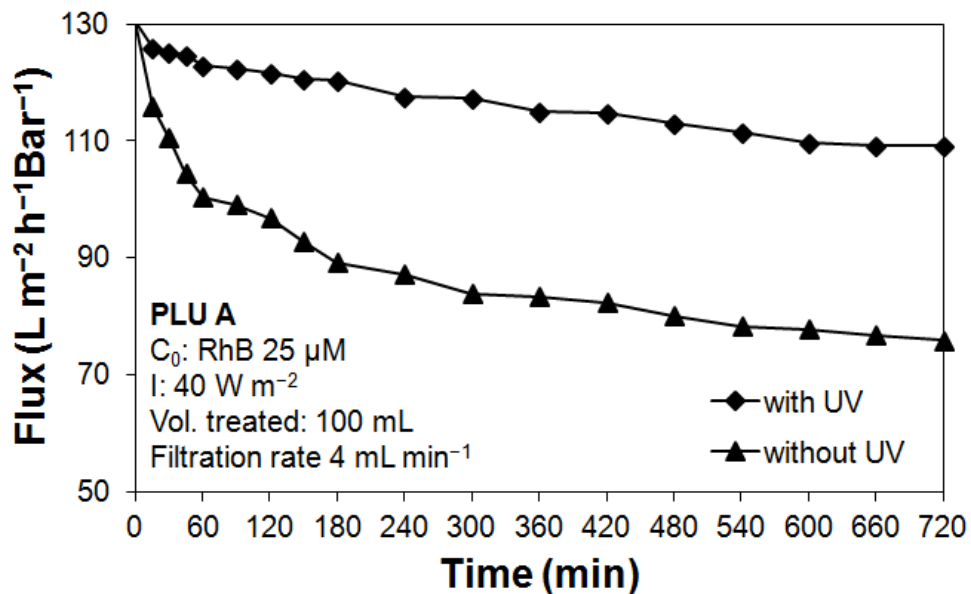
**Table 4.3** Membrane performance in terms of its photocatalytic activity (PCA) and adsorptive-membrane retention (Ads-MR) after 8 h of operation

Types	Removal ( $\text{mg m}^{-2}$ )			Removal (%)	
	PCA	Ads-MR	Total	PCA	Ads-MR
Plu Control	686 $\pm$ 36	630 $\pm$ 23	1316 $\pm$ 20	52.1	47.9
Plu A	2104 $\pm$ 31	600 $\pm$ 17	2704 $\pm$ 13	77.8	22.2
Plu B	1905 $\pm$ 21	378 $\pm$ 20	2283 $\pm$ 10	83.4	16.6
Plu C	1654 $\pm$ 18	230 $\pm$ 11	1884 $\pm$ 18	87.8	12.2
Plu D	2025 $\pm$ 24	329 $\pm$ 13	2354 $\pm$ 18	86.0	14.0

Fouling-control property of the  $\text{TiO}_2$  photocatalytic membrane is illustrated in Fig. 4.11. The initial decline of flux rate could be attributed to the adsorption of RhB molecules onto  $\text{TiO}_2$  photocatalytic membrane. After which, decreasing flux rate was observed until the sustainable (steady state) flux was reached. It has been observed that the PMR experiment with the presence of UV irradiation suffered only 16.5% of total flux decline over 720 min of experimental run as compared to 42% for the PMR experiment without UV irradiation. This could be attributed to a good wettability and self-cleaning induced by photocatalytic membrane surface. The results suggested that  $\text{TiO}_2$  layers were able to minimize and control fouling as they could photodegrade the adsorbed RhB molecules and minimize the flux decline throughout the duration of the experimental run.

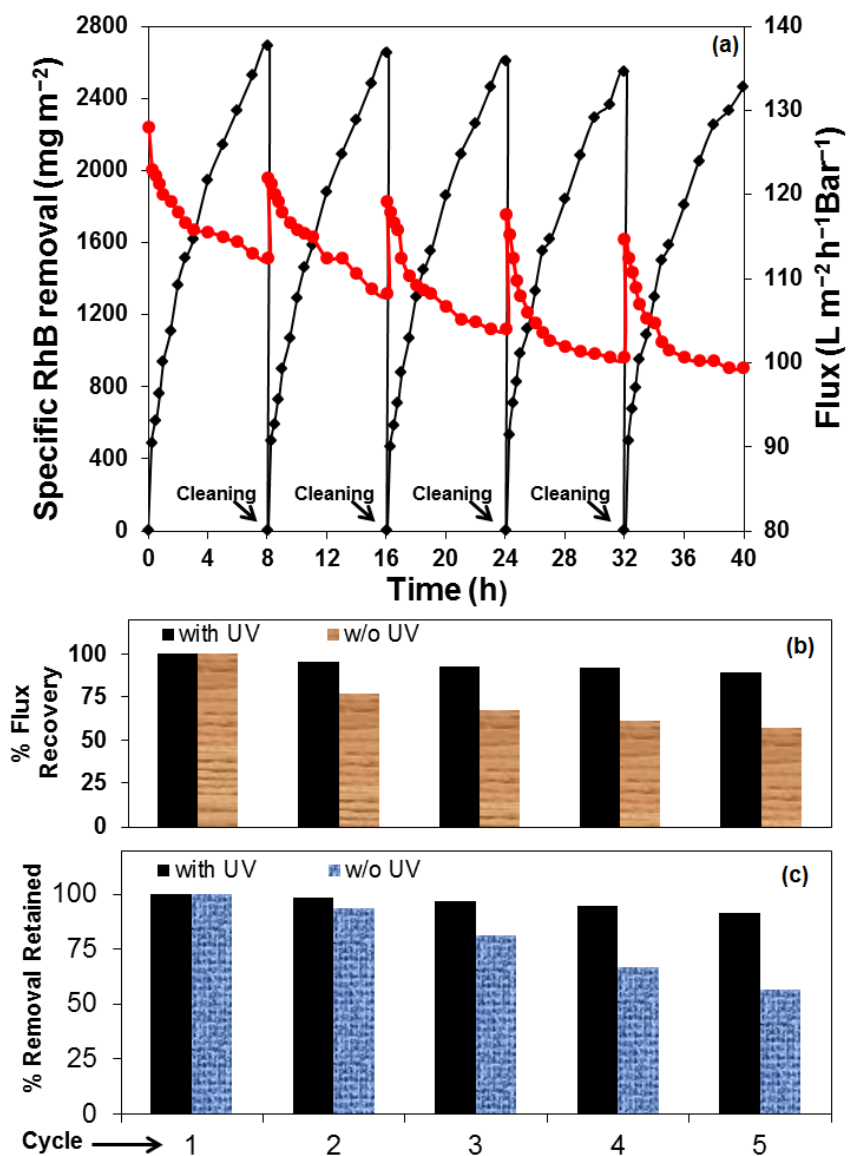
Reusability of membrane could significantly lower the operation cost of water and wastewater treatment plants. A Plu A membrane specimen was used for 5 treatment cycles of 25  $\mu\text{M}$  RhB solutions, and the results are shown in Fig. 4.12. Plu A membrane was able to degrade a relatively same amount of RhB over multiple cycles of 8 h each. The 5<sup>th</sup> cycle of treatment still showed 91% of the initial RhB removal efficiencies (a 9% drop from 2690 to 2460  $\text{mg m}^{-2}$  of RhB). The slight decrease in the RhB removal with increasing treatment

cycle could be explained by the accumulative adsorption of RhB onto the surface of the membrane that reduced the density of active photocatalytic sites.



**Figure 4.11** Anti-fouling property of  $\text{TiO}_2$  photocatalytic membrane.

Similar trend was observed for the flux profile. In each cycle, the permeability flux decreased with permeation time. However, upon each cleaning cycle with DI water under UV irradiation for 2 h, more than 95% of the initial flux could be recovered. Cleaning with DI water without the presence of UV irradiation (Fig. 11(b) and (c)) only recovered about 57% of the initial flux after 5<sup>th</sup> cycle of treatment and meanwhile the RhB removal efficiency also dropped to 56% of its initial efficiency. This showed that with intermittent UV-assisted self-cleaning, the  $\text{TiO}_2$  photocatalytic membrane was reusable over a prolonged period without a significant flux decline and deactivation.



**Figure 4.12** Reusability potential of the TiO<sub>2</sub> photocatalytic membrane: (a) specific RhB removal and flux performance with inter-cycles cleaning in the presence of UV irradiation; comparison of the effect of UV irradiation during inter-cycles cleaning in terms of (b) % flux recovery and (c) % RhB removal retained.

## 4.4 Conclusions

TiO<sub>2</sub> photocatalytic membrane was fabricated via acid-catalyzed sol-gel method incorporating Pluronic P-123 triblock-copolymer as pore forming agent and PVA as pore fillers and binder. Layer-by-layer coating of TiO<sub>2</sub> of different porosities and pore structures were thoroughly carried out. The resulting membranes were characterized for its physico-chemical and morphological characteristics. The membranes showed excellent photocatalytic activity when tested in the batch photoreactor. The Plu A membrane (which was coated with 3 different TiO<sub>2</sub> layers of different pore structures) showed a high water permeability flux of 116 L m<sup>2</sup> h<sup>-1</sup> Bar<sup>-1</sup> with the corresponding intrinsic membrane resistance of  $3.1 \times 10^{12} \text{ m}^{-1}$ . Plu A membrane also possessed excellent specific RhB removal of 2700 mg m<sup>-2</sup>. The membrane with a thinner top separation layer (Plu D) showed a higher water permeability flux and specific RhB removal when compared with the membrane with the same number of layers but a thicker separation layer (Plu B).

The result suggested that by tailoring the layered structures (porosity gradient), an optimum membrane performance could be obtained. The as-synthesized hybrid photocatalytic membrane has a great potential for use in water and wastewater treatment owing to its fouling-control capability, high intrinsic permeability, good photocatalytic activity, and reusability potential. These properties are favorable for practical applications of membrane separation processes. The integration of the heterogeneous photocatalysis and membrane process in the membrane photoreactor offers simultaneous photodegradation and membrane separation, simpler system configuration with less mechanical and hydraulic fittings, and smaller overall footprint (Lim et al. 2011).

# **CHAPTER 5 EFFECT OF DIFFERENT STRUCTURE DIRECTING AGENTS ON THE PERFORMANCES OF THE HIERARCHICALLY POROUS TiO<sub>2</sub> PHOTOCATALYTIC CERAMIC MEMBRANES**

## **5.1 Introductions**

The porous structure of the TiO<sub>2</sub> layer could be formed and fine-tuned by incorporating different structure directing agents (SDAs) during the preparation of the TiO<sub>2</sub> sols. SDAs are molecules that possess both hydrophobic and hydrophilic segments that exhibit partial affinity toward both polar and non-polar surfaces. Various SDAs that have been incorporated in the preparation of TiO<sub>2</sub> sols were Pluronic P-123 (P-123) (Goei et al. 2013, Liu et al. 2009, Procházka et al. 2008, Sun et al. 2009, Wu and Rankin 2011), Triton X-100 (Lei et al. 2011, Sanguanruang et al. 2011, Xu et al. 2013), Tween 20 (Chen and Dionysiou 2008, García-Benjume et al. 2009), and Tween 80 (Choi et al. 2006d, Choi et al. 2006c, Han et al. 2011). The important properties of these SDAs are summarized in Table 5.1. At a very low loading concentration, there is no assembly of the SDA molecules. At the higher concentration known as the critical micelle concentration (CMC), the SDA molecules would aggregate to form a unimolecular layer. Above the CMC, the SDA molecules would self-assemble into a micelle. In the TiO<sub>2</sub> sols, the SDA would form the self-assembled micelles that could be removed during the calcination step, leaving behind a mesoporous TiO<sub>2</sub> nano-structure. Non-ionic SDAs such as Triton X-100, Tween 20 and Tween 80 generally have the advantages over ionic SDAs in term of its compatibility with other types of SDA and the stability over a wider pH range (Attwood and Florence 1985, Porter 1994). P-123 is an amphiphilic triblock

copolymer that exhibits a similar micellar assembly as the non-ionic SDA. The hydrophile-lipophile balance (HLB) number (with values range from 0-20) describes the amphiphilic nature of the SDAs. All the SDAs have a relatively high HLB number which suggests the hydrophilic characteristic of the SDA.

**Table 5.1** Properties of different SDAs used

SDA	Pluronic® P-123	Triton X-100™	Tween® 20	Tween® 80
<b>Structure</b>				
<b>MW (g mol<sup>-1</sup>)</b>	5,800	647	1,228	1,310
<b>CMC<sup>a</sup> (μM)</b>	4.4	220-240	60	12
<b>HLB<sup>b</sup></b>	8.0	13.5	16.7	15.0
<b>Hydrophobic group</b>	Propylene	Phenyl ether	Lauric acid	Oleic acid
<b>Density (g cm<sup>-3</sup>)</b>	1.04	1.07	1.10	1.06

<sup>a</sup> Critical micelle concentration

<sup>b</sup> Hydrophile-lipophile balance

The hierarchically porous TiO<sub>2</sub> hybrid photocatalytic ceramic membrane could be constructed by multilayer coating of TiO<sub>2</sub> layers, starting with the layer of largest porosity, following a decreasing porosity gradient profile, ending with the thinnest separation layer of the smallest porosity. The performances of the resulting TiO<sub>2</sub> photocatalytic ceramic membrane could be controlled and optimized by coating an appropriate TiO<sub>2</sub> layer chosen from a wide range of the as-prepared TiO<sub>2</sub> sols. This fabrication scheme allows the flexibility of tailoring the porosity gradient of the membrane to obtain desired membrane performances.

In this chapter, the fabrication of the hierarchically porous TiO<sub>2</sub> photocatalytic ceramic membrane that possessed different porosity gradient configurations is discussed. Four specimens of the TiO<sub>2</sub> photocatalytic membranes were prepared each with multilayer coating of different TiO<sub>2</sub> sols prepared using one type of SDA. Two of the membrane specimens were prepared by coating TiO<sub>2</sub> sub-layers prepared with different SDAs, which was made possible by a good compatibility among the non-ionic SDAs. The physico-chemical and morphological properties of the membrane were elucidated using various characterization tools (i.e. N<sub>2</sub> porosimetry analysis, powder X-ray diffraction, scanning electron microscope, and video contact angle measurement). The performances of the membranes were evaluated using the batch photoreactor and photocatalytic membrane reactor (PMR). It was also the aim of this phase of study to optimize the performance of the membrane by fine-tuning its pore structure configuration.

## **5.2 Experimental procedures**

### **5.2.1 Membrane fabrication**

Four different SDAs (i.e. P-123, Triton X-100, Tween 20 and Tween 80) were used to modify the microstructure of the resulting TiO<sub>2</sub> layer. The properties of the SDAs used are summarized in Table 5.1. Twelve different TiO<sub>2</sub> sols were prepared by acid-catalyzed sol-gel method (Section 3.1.3). The final sols had a constant molar ratio of IPA:HCl:TTIP:H<sub>2</sub>O equals to 60:4:1:4 but contained 0.5, 1.0, or 2.0 mol% of SDAs (with respect to TiO<sub>2</sub>). The resulted TiO<sub>2</sub> layers hereafter are referred as X-Y where X is the type of SDA added (P, X, T20, and T80 for P-123, Triton X-100, Tween 20 and Tween 80 respectively) and Y is the amounts of SDA added in mol% with respect to TiO<sub>2</sub>.

Six different SDA-modified membrane specimens of different porosity gradients were fabricated and they are summarized in Table 5.2. Each membrane specimen consists of 3 photocatalytic layers. The first photocatalytic layer was formed through 3 coatings of the similar sol resulting into the formation of 3-sub-layers of the largest porosity. The intermediate layer which consists of 2-sub-layers was formed through 2 coating of the similar sol. Finally, a thin top-layer of smallest porosity was coated onto the membrane as the top separation layer. The first 4 membranes (Plu, X, T20, and T80) were fabricated from the sols prepared using only one type of SDA (hereafters are referred as one-SDA-type membranes). Membranes M1 and M2 were fabricated from the TiO<sub>2</sub> sols prepared using different types of SDAs (i.e. P-2.0, T20-1.0, T80-0.5 and T80-2.0, X-2.0, P-0.5 for membranes M1 and M2 respectively). A control membrane specimen consisting of 6 sub-layers of SDA-free TiO<sub>2</sub> sols was also prepared for comparisons.

**Table 5.2** Types of TiO<sub>2</sub> photocatalytic ceramic membranes fabricated

Types	Layers coated			TiO <sub>2</sub> loading ( $\mu\text{g cm}^{-2}$ )	Thickness of TiO <sub>2</sub> layer (nm) <sup>a</sup>	PEG rejection (%) <sup>b</sup>	Pure water permeance ( $\text{L m}^{-2} \text{h}^{-1}$ $\text{Bar}^{-1}$ )
	1 <sup>st</sup> (bottom) 3-sub-layers	2 <sup>nd</sup> 2-sub-layers	3 <sup>rd</sup> (top) 1-layer				
Plu	P-2.0	P-1.0	P-0.5	117.4 ± 0.7	532 ± 23	91.8 ± 0.5	116 ± 2
X	X-2.0	X-1.0	X-0.5	100.7 ± 0.5	408 ± 12	84.9 ± 0.7	127 ± 3
T20	T20-2.0	T20-1.0	T20-0.5	95.9 ± 1.0	455 ± 19	79.0 ± 0.4	141 ± 2
T80	T80-2.0	T80-1.0	T80-0.5	105.9 ± 0.5	511 ± 18	76.4 ± 0.3	149 ± 3
M1	P-2.0	T20-1.0	T80-0.5	107.9 ± 0.5	536 ± 16	76.0 ± 0.3	155 ± 3
M2	T80-2.0	X-2.0	P-0.5	104.7 ± 0.6	471 ± 10	89.5 ± 0.8	121 ± 1
Control	Control	Control	Control	107.3 ± 0.4	312 ± 6	94.1 ± 0.4	109 ± 1

Note: All numbers after ± indicate the standard deviation.

<sup>a</sup> Determined by considering different porosities of each sub-layers and assuming uniform density of anatase of 3.9 g cm<sup>-3</sup>.

<sup>b</sup> Determined using PEG of MW 20,000 g mol<sup>-1</sup>.

### **5.2.2 Characterization techniques**

Various characterization techniques were used to understand physico-chemical and morphological properties of the membrane (the detailed description of the instrumentation and methodology can be found in Section 3.3). Characterization techniques used for the pulverized TiO<sub>2</sub> layer were: FTIR, N<sub>2</sub> adsorption/desorption porosimetry analysis, Raman spectroscopy, and XRD. The surface morphological characteristic of the membrane was studied using FESEM. Finally, the photo-induced super-hydrophilicity property of the membrane was observed through the contact angle measurement.

### **5.2.3 Evaluation of membrane performance**

The photocatalytic activity of the membrane was evaluated both using the batch photoreactor (Section 3.4.2) and the PMR (Section 3.4.3) against photocatalytic degradation of RhB. In a typical experiment in the batch photoreactor, each types of membrane were used to treat 12 mL of RhB solution without any stirring and oxygen bubbling. The extent of the photodegradation of RhB was monitored using UV/Vis spectrophotometer at 553 nm.

The PMR setup was used to evaluate the performance of the membrane in the dead end filtration mode. The coated membrane disc was mounted and secured tightly in the membrane cells. The pure water permeability and the MWCO of the membrane were evaluated using the PMR. The membrane was also used to treat up to 5 cycles of 100 mL, 25 μM RhB solutions. The overall RhB removal could be itemized into 2 different processes: Ads-MR and PCA by the membrane. Control experiments without turning on the UV source were performed to elucidate the effect of Ads-MR on the removal of RhB. Fouling-control property of TiO<sub>2</sub> photocatalytic membrane was tested in the PMR setup for 12 h without re-circulation of permeate.

## 5.3 Results and discussion

### 5.3.1 Physico-chemical characteristics of TiO<sub>2</sub> layers.

A total of 12 different TiO<sub>2</sub> layers of varying types and amounts of SDAs incorporated were prepared, producing 6 different SDA-modified membrane specimens (Table 5.2). The important physico-chemical characteristics of the as-prepared TiO<sub>2</sub> layers are summarized in Table 5.3.

**Table 5.3** Physico-chemical characteristics of the as-prepared TiO<sub>2</sub> layers

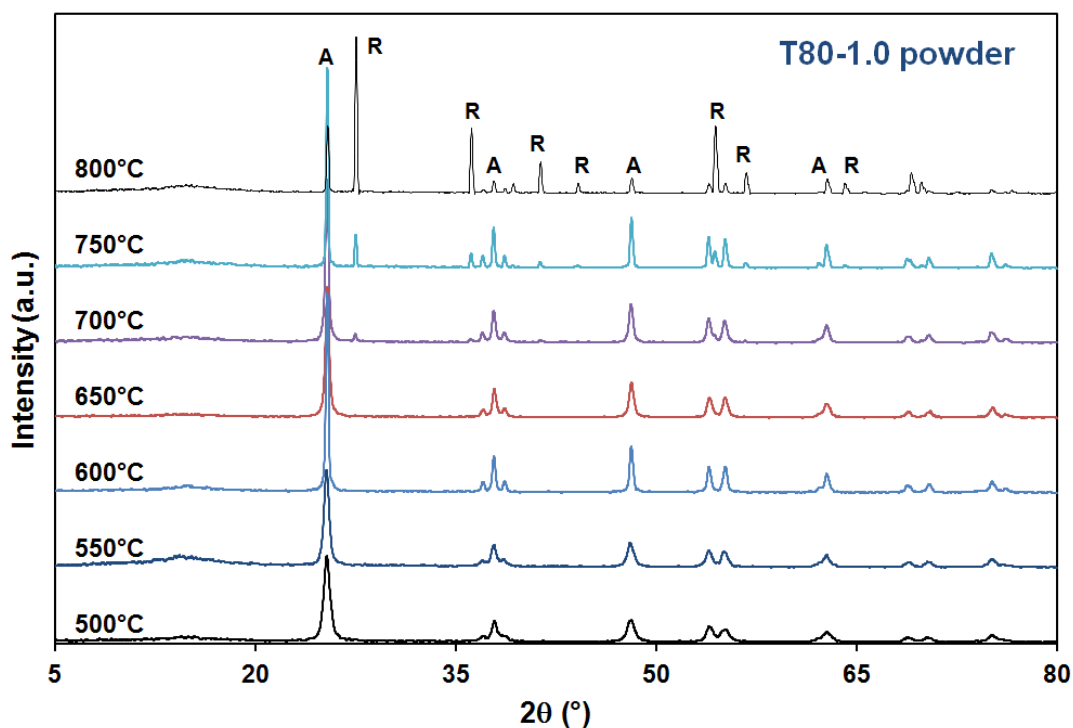
Surfactant		BET Surface Area (m <sup>2</sup> g <sup>-1</sup> )	Porosity (%) <sup>a</sup>	XRD Crystallite Size (nm) <sup>b</sup>
Types	Loading			
TiO <sub>2</sub> Control	Control	11.9 ± 0.3	12.1 ± 0.4	14.4
Pluronic <sup>®</sup> P-123	P-0.5	27.6 ± 0.4	22.0 ± 0.6	13.3
	P-1.0	83.3 ± 1.0	35.0 ± 0.4	10.8
	P-2.0	146.7 ± 1.1	51.5 ± 0.4	7.3
Triton <sup>™</sup> X-100	X-0.5	102.5 ± 1.2	30.5 ± 0.3	7.4
	X-1.0	107.7 ± 0.3	35.5 ± 0.4	7.2
	X-2.0	123.9 ± 0.9	38.9 ± 0.2	6.6
Tween <sup>®</sup> 20	T20-0.5	134.9 ± 1.0	35.6 ± 0.7	7.3
	T20-1.0	140.0 ± 0.4	45.1 ± 0.3	6.9
	T20-2.0	150.4 ± 0.9	48.9 ± 0.1	6.3
Tween <sup>®</sup> 80	T80-0.5	134.5 ± 1.1	40.8 ± 0.4	7.7
	T80-1.0	141.8 ± 0.5	44.8 ± 0.4	6.9
	T80-2.0	154.2 ± 1.1	49.4 ± 0.1	6.4

Note: All numbers after ± indicate the standard deviation.

<sup>a</sup> Determined assuming uniform density of anatase of 3.9 g cm<sup>-3</sup>.

<sup>b</sup> Calculated using Scherrer's equation with error < 1 nm.

The formation of the mesoporous structure in the P-123-based TiO<sub>2</sub> layer was due to microphase separation caused by the difference in the hydrophilicity of the polyethylene glycol and polypropylene glycol blocks of P-123. The incorporation of P-123 into the preparation of TiO<sub>2</sub> sols also lowered the viscosity and increased the stability of the sols allowing the coating of uniform TiO<sub>2</sub> thin layers with minimum presence of cracks and pinholes (Goei et al. 2013). A non-ionic surfactant such as Triton X-100, Tween 20, and Tween 80 formed the self-assembled micelles via solvent evaporation during drying and ageing period. The TiO<sub>2</sub> mesoporous structure was formed as the result of hydrogen bonding between the surfactant and the titanium hydrates. Besides, in the case of T20 (a hydrophilic SDA), the addition of surfactant could decrease the rate of solvent evaporation and minimize the development of tensile stress of the TiO<sub>2</sub> layer during the calcination resulting in a TiO<sub>2</sub> layers with minimum presence of cracks and pinholes (Chen et al. 2011).

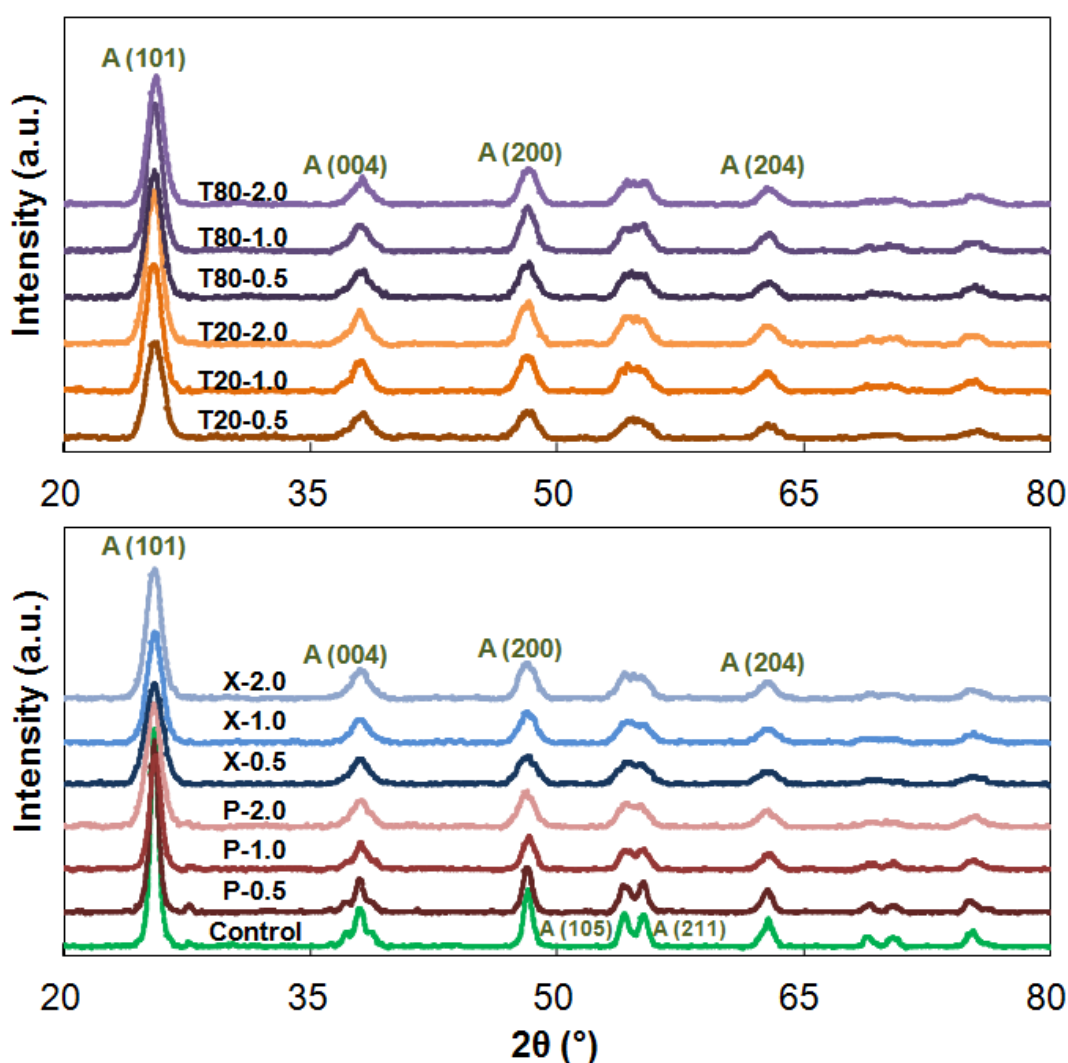


**Figure 5.1** XRD spectra of the pulverized T80-1.0 TiO<sub>2</sub> layers calcined at different temperatures.

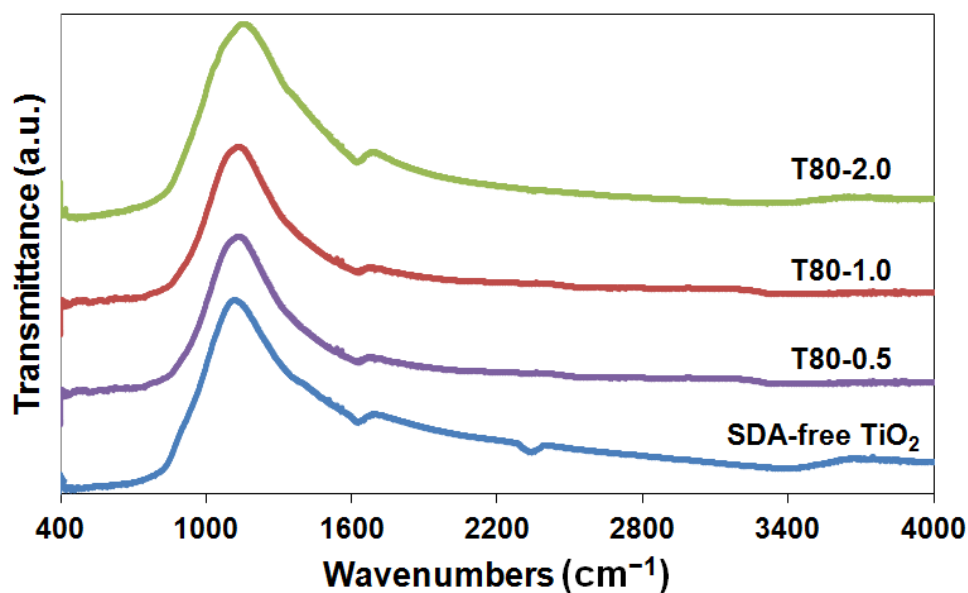
The wide-angle XRD spectra of different TiO<sub>2</sub> layers are shown in Figs. 5.1 and 5.2. The effect of calcination temperature on the purity and crystal phase of TiO<sub>2</sub> is shown in Fig. 5.1. At calcination temperature of 500°C, pure anatase phase is successfully formed. Five distinctive anatase-TiO<sub>2</sub> peaks at 25.3°, 37.9°, 48.0°, 54.6°, and 62.8° which correspond to (101), (004), (200), (105 and 211), and (204) reflections of crystalline anatase-TiO<sub>2</sub> planes respectively (JCPDS 21-1272) can be observed. The crystallization process of TiO<sub>2</sub> occurred when the calcination temperature was higher than 350°C. No other peaks other than characteristic peaks of anatase could be observed on the XRD spectra showing that calcination temperature of 500°C was sufficient to remove surfactant used in the synthesis process. As the calcination temperature increased, the FWHM decreased and the crystallites size increased. For the calcination temperature higher than 700°C, 3 characteristics rutile peaks at 25.34°, 30.31°, and 25.69° corresponding to (120), (121) and (111) crystal planes respectively (JCPDS 82-0514) were observed, signifying that anatase-rutile phase transformation had occurred. At higher calcination temperatures, the rutile peaks intensified to replace the anatase peaks.

The XRD spectra of different types of SDA-modified TiO<sub>2</sub> layers calcined at 500°C are presented in Fig. 5.2. No amorphous or other TiO<sub>2</sub> polymorphs peak can be observed in all of the spectra indicating a successful formation of anatase. TiO<sub>2</sub> crystallite sizes are calculated from the peak broadening of (101) anatase crystal plane at 25.3° using Scherrer's equation (Scherrer 1918) and are summarized in Table 5.3. The relatively wide (101) peak indicates a small TiO<sub>2</sub> crystallite size. TiO<sub>2</sub> layers with varying crystallite sizes from 6.3 nm (T20-2.0) to 14.4 nm (control) could be fabricated. The sizes of TiO<sub>2</sub> crystal decreased as the amount of SDAs loading increased for all types of the SDA incorporated. This phenomenon was caused

by the decrease in the hydrolysis and condensation rate of the titanium alkoxide resulting in the smaller TiO<sub>2</sub> crystallites (Pelaez et al. 2010). For the case of P-123-based TiO<sub>2</sub>, this phenomenon could be attributed to the spatial confinement mechanism through which TiO<sub>2</sub>-anatase crystals were assembled while maintaining the integrity of the P-123 scaffold (Guldin et al. 2011). The crystallinity of resulting TiO<sub>2</sub> layer decreased as the amount of SDAs loading increased. This was evidenced by the overlapping of anatase (105) and (211) reflections from samples with a higher SDA loading.



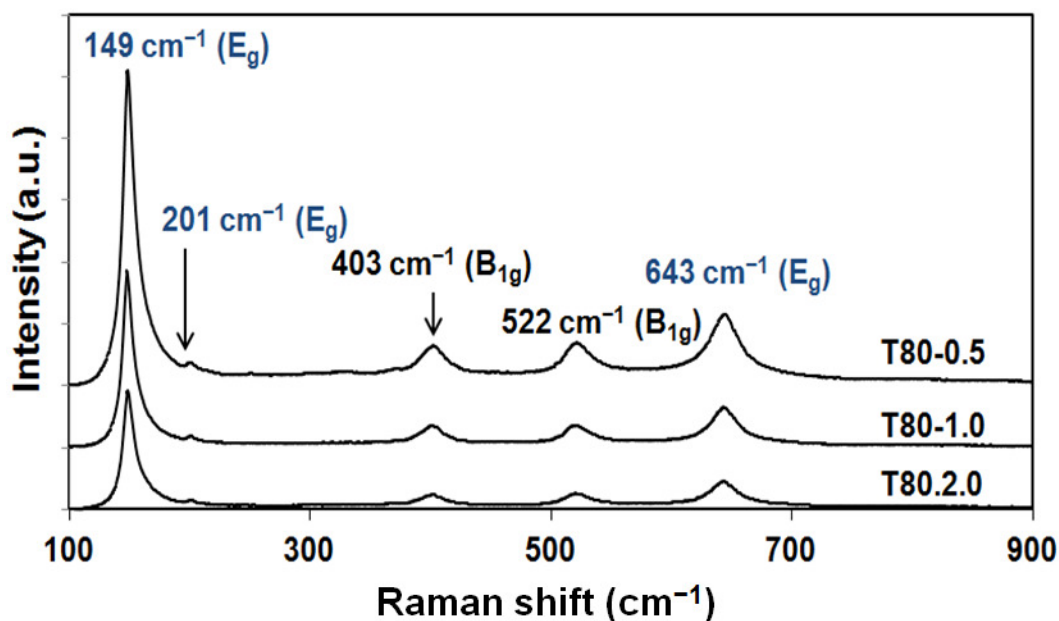
**Figure 5.2** XRD spectra of the pulverized TiO<sub>2</sub> layers prepared with different SDAs.



**Figure 5.3** FTIR spectra of the pulverized TiO<sub>2</sub> layers prepared with T80.

The FTIR spectra of the representative TiO<sub>2</sub> layers prepared using T80 SDA is shown in Fig. 5.3. FTIR spectra observed in this study were compared with the literature (Bradley et al. 1978, Kumar et al. 2000, Pavia et al. 2009, Vinodgopal et al. 1996, Yu et al. 2003). The spectra show the main bands at 400–700 cm<sup>-1</sup>, which could be attributed to Ti-O bond stretching and Ti-O-Ti bridging stretching modes. The relatively weak band at 1400 cm<sup>-1</sup> could be attributed to a relatively weak OH<sup>-</sup> bending vibration. The bending vibration of the adsorbed water could be observed at 1630 cm<sup>-1</sup>. The broadband at 3100–3700 cm<sup>-1</sup> could be assigned to stretching vibration of the hydrogen bonded hydroxyl group and the titanium hydroxide. The titanium hydroxide was formed by hydrolysis of titanium alkoxide source with band at 3400 cm<sup>-1</sup> associated with weakly chemisorbed hydroxyl group. The peaks for carbonyl bonding are located at 1635, 1638, 2360, and 2922 cm<sup>-1</sup> corresponding to C=C, C=O, -CH and -CH<sub>2</sub> respectively. For the SDA-free TiO<sub>2</sub> layer, the only carbonyl peak observable from the FTIR spectra is -CH peak. As no other significant organic content could be observed in the FTIR spectra for all of the as-synthesized TiO<sub>2</sub> layers, the calcination

temperature of 500°C as adopted in this study was deemed sufficient to remove the organic component present in the sol. The presence of a small peak at 1630 cm<sup>-1</sup> shows that hydroxyl groups in the TiO<sub>2</sub> thin films could never be removed completely which was beneficial to enhance the surface hydrophilicity of the TiO<sub>2</sub> photocatalytic membrane.



**Figure 5.4** Raman spectra of the pulverized TiO<sub>2</sub> layers prepared with T80.

The Raman spectra of the representative TiO<sub>2</sub> layers prepared using T80 SDA is shown in Fig. 5.4. Anatase is a tetragonal structure (space group D<sub>19</sub><sup>4h</sup> (I4/amd)) with 2 formula units per unit cell. Information about the structure of anatase can be represented in 10 optical modes which are 1A<sub>1g</sub> + 1A<sub>2u</sub> + 2B<sub>1g</sub> + 1B<sub>2u</sub> + 3E<sub>g</sub> + 2E<sub>u</sub>. The A<sub>2u</sub> and E<sub>u</sub> modes are active in the infrared spectra while A<sub>1g</sub>, B<sub>1g</sub>, and E<sub>g</sub> modes are in the Raman spectra. The peaks of the bulk anatase are observed at Raman shift at 149 cm<sup>-1</sup> (E<sub>g</sub>), 201 cm<sup>-1</sup> (E<sub>g</sub>), 403 cm<sup>-1</sup> (B<sub>1g</sub>), 522 cm<sup>-1</sup> (B<sub>1g</sub>), and 643 cm<sup>-1</sup> (E<sub>g</sub>). No rutile peaks (143 cm<sup>-1</sup> (B<sub>1g</sub>), 447 cm<sup>-1</sup> (E<sub>g</sub>), 612 cm<sup>-1</sup> (A<sub>1g</sub>), and 399 cm<sup>-1</sup> (B<sub>2g</sub>)) could be observed in all the analyzed TiO<sub>2</sub> layers. It could be observed from the main anatase peak located at 149 cm<sup>-1</sup> that as the amount of T80 in the sol

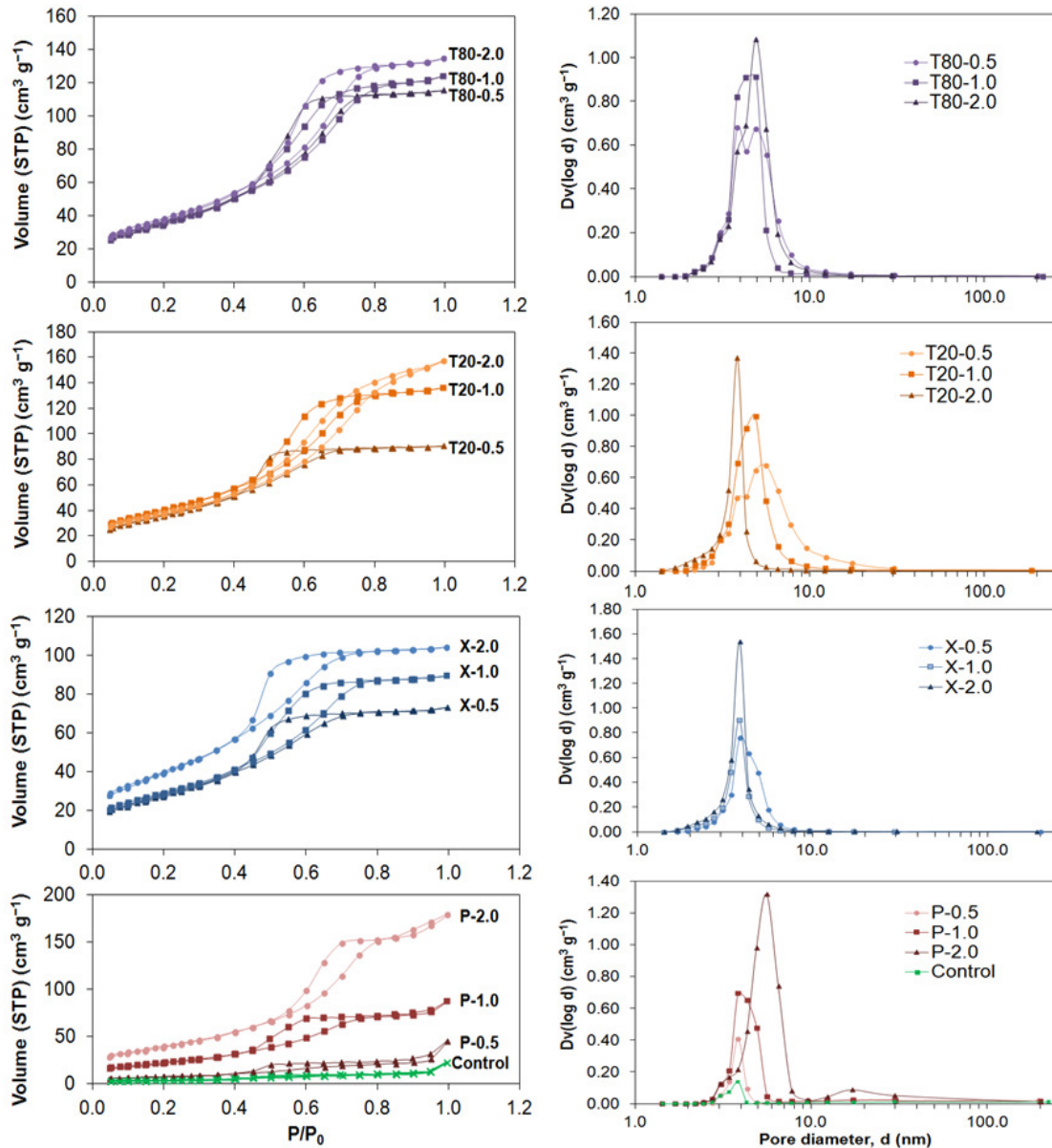
increased, the relative intensity of the peak decreased. This indicated that a larger TiO<sub>2</sub> crystal was resulted from the enhancement of the Ti-O bonding, illustrating the effectiveness of T80 (or other SDAs) in controlling the TiO<sub>2</sub> crystallite size. This trend was in a good agreement with the crystallite size derived from XRD result.

The Raman peaks observed in this study are compared with the literature (Ohsaka et al. 1979). There is a blue shift in the Raman spectra of the as-prepared TiO<sub>2</sub> layers. As reported before, the peak shift could be caused either by oxygen deficiency of the non-stoichiometric TiO<sub>2</sub> (Parker and Siegel 1990), or the dimensional effect known as phonon confinement, in the case of stoichiometric TiO<sub>2</sub>, (Bersani et al. 1998).

The ability of SDA to fine-tune the resulting microstructure of the TiO<sub>2</sub> layers is further evidenced from the N<sub>2</sub> adsorption/desorption isotherm. The result is summarized in Table 5.3 and Fig. 5.5. All samples exhibited the type-IV adsorption isotherm indicating their well developed mesoporous structures. The narrow distribution of TiO<sub>2</sub> pore sizes (4-6 nm) are evidenced from the sharp hysteresis loops. The SDA-modified TiO<sub>2</sub> was highly porous with highly interconnected network which yielded TiO<sub>2</sub> layer with high porosity. It has been observed that as the amount of SDAs loading increased, the BET surface area and porosity of the resulting TiO<sub>2</sub> layers increased for all types of the SDAs incorporated.

The increases in the BET surface area and the overall porosity of the TiO<sub>2</sub> layers were caused by the pore coalescence and the multi-micellar interactions during the calcination step (Choi et al. 2006d). The increase in the pore size of the TiO<sub>2</sub> layer would result in a thinner mesoporous wall. This observation was in a good agreement with the decreasing XRD crystallite size for the layer with of a higher amount of SDA added. Smaller TiO<sub>2</sub> crystals would result in a larger overall surface area as measured by N<sub>2</sub> adsorption/desorption. The increase in BET surface area and the overall porosity was the most significant in the P-123-

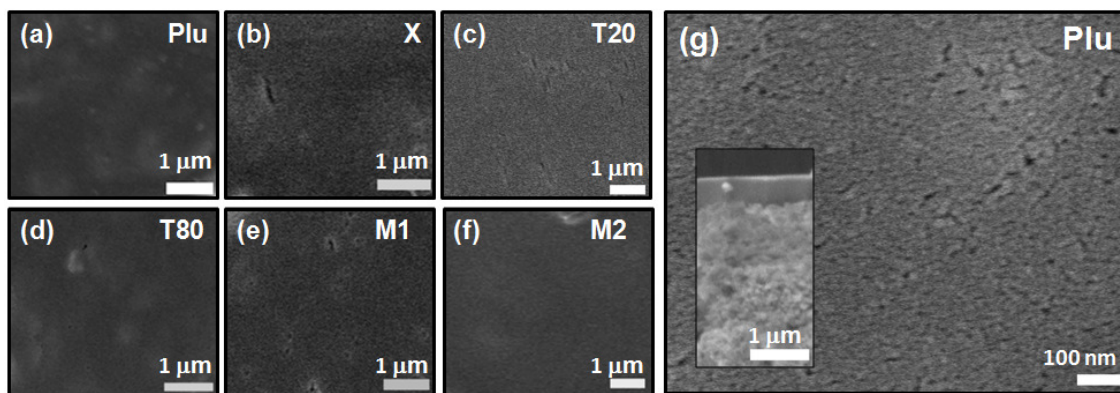
based TiO<sub>2</sub> layer. TiO<sub>2</sub> layer prepared using P-123 at 0.5 mol%, showed the smallest surface area (27.6 m<sup>2</sup> g<sup>-1</sup>) and porosity (22 %). The surface area and porosity of the P-123-based TiO<sub>2</sub> would eventually increase to 146.7 m<sup>2</sup> g<sup>-1</sup> and 51.5 % respectively for the P-2.0 layer. This is in agreement with the greater variation observed in the TiO<sub>2</sub> crystallite size of P-123-based TiO<sub>2</sub> (from 13.3 nm for P-0.5 to 7.3 nm for P-2.0).



**Figure 5.5** (a) N<sub>2</sub> adsorption/desorption isotherms and (b) pore size distributions of the pulverized TiO<sub>2</sub> layers prepared with different SDAs.

There was only a small variation of BET surface area and porosity observed for TiO<sub>2</sub> layers prepared using T20 and T80. This was due to the small difference in their molecular weights and HLB. The only difference between T20 and T80 was the type of its hydrophobic group, lauric acid and oleic acid respectively. Triton-based TiO<sub>2</sub> showed the smallest surface area and porosity at 2 mol% SDA loading which could be attributed to its small molecular weight. Also, SDA with longer chain length (e.g. Tween SDA, 20 ether groups) would produce TiO<sub>2</sub> layer with higher porosity and larger pore size when compared to the SDA with shorter chain length (e.g. Triton X-100, 10 ether groups). The XRD, Raman and N<sub>2</sub> porosimetry analysis have exhibited the successful formation of the SDA-modified TiO<sub>2</sub> layer with controllable mesoporous structure.

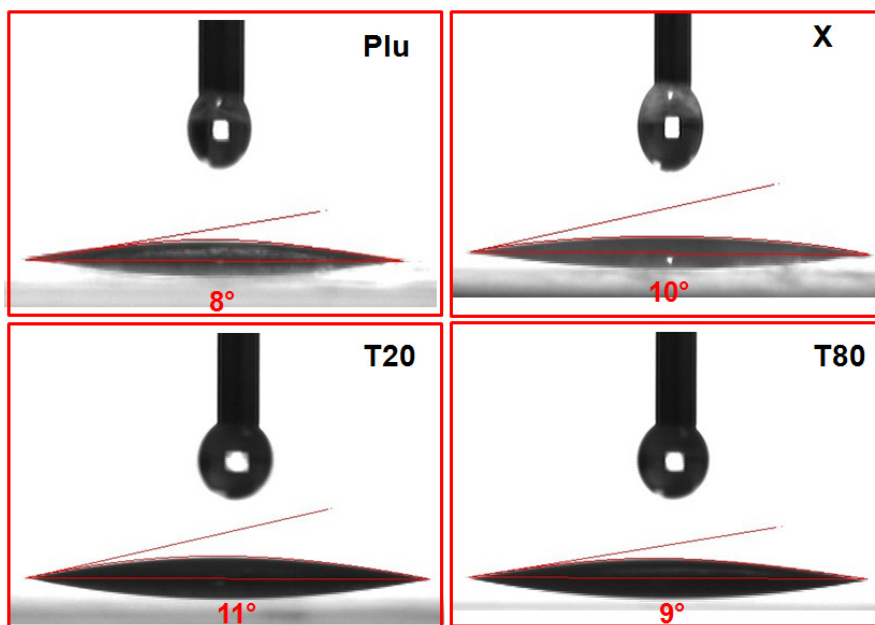
### 5.3.2 Characteristics of TiO<sub>2</sub> photocatalytic ceramic membranes



**Figure 5.6** FESEM micrographs of the surface of: (a) Plu, (b) X, (c) T20, (d) T80, (e) M1 and (f) M2 membrane. (g) a high magnification FESEM micrograph of Plu membrane (the inset depicts cross-sectional view of Plu membrane).

All the membranes were prepared to produce the following porosity gradient configuration scheme: the first (bottom) 3-sub-layers were the most porous, followed by the subsequent less porous 2-sub-layers, and finally a thin least porous separating (top) layer. Figs. 5.6a-f show

the FESEM micrographs of the membrane surface. It can be observed from the FESEM micrographs that relatively smooth TiO<sub>2</sub> layers were successfully coated onto the finished membranes. The presence of cracks and pinholes are minimal in all the membrane specimens. This is an important observation to ensure uniform permeability and good separation performance across the membrane area.

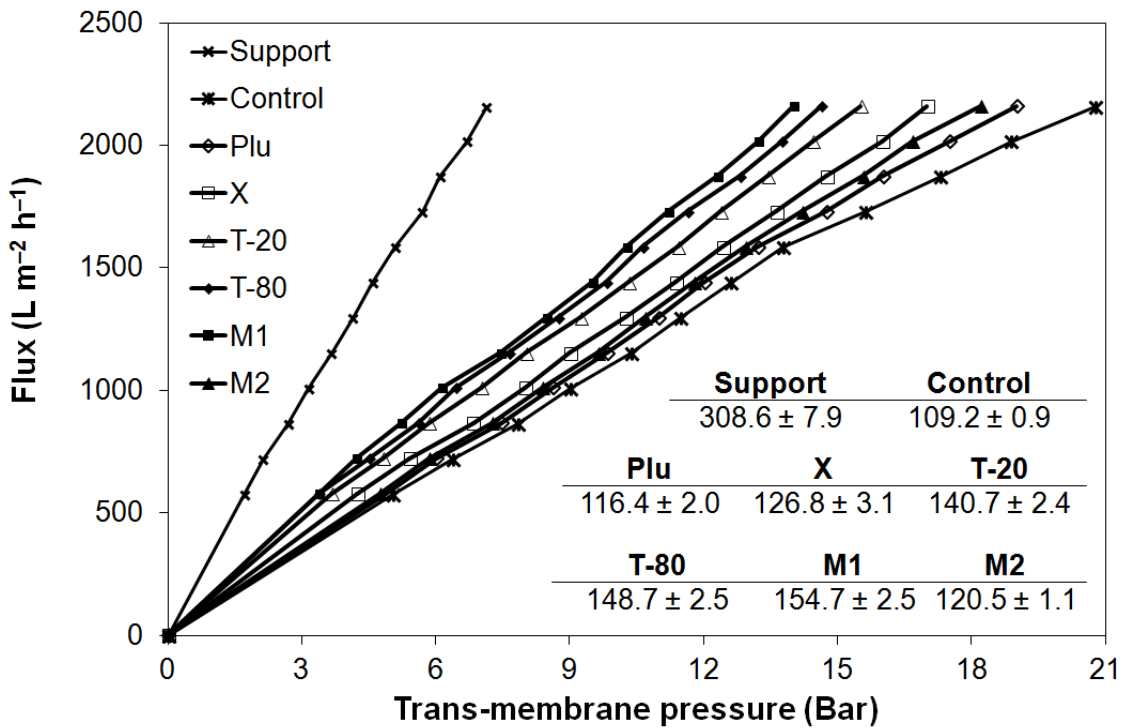


**Figure 5.7** Photoinduced super-hydrophilicity (PSH) property of TiO<sub>2</sub> thin films prepared using different SDAs.

The TiO<sub>2</sub> membranes exhibited a photoinduced super-hydrophilicity (PSH) phenomenon. The contact angle micrographs of TiO<sub>2</sub> layers prepared using different SDAs and its corresponding contact angle values are shown in Fig. 5.7. Upon UV irradiation, all the TiO<sub>2</sub> layers coated on a borosilicate glass slides shows a relatively small contact angle  $\leq 11^\circ$ . This was caused by hydroxylation of TiO<sub>2</sub> thin film surface when subjected to the UV irradiation. Ti<sup>3+</sup> defective sites are formed when lattice metal ions Ti<sup>4+</sup> interact with photogenerated electrons. Surface-trapped electron Ti<sup>3+</sup> would react with oxygen adsorbed on the surface to form O<sub>2</sub><sup>-</sup> or O<sub>2</sub><sup>2-</sup> ions leaving the oxygen vacancy sites (Sakai et al. 2003). Adsorbed water

molecules would occupy the oxygen vacancy sites to reduce the overall surface energy, releasing proton to a nearby oxygen atom and forming two hydroxyl groups on the surface of the TiO<sub>2</sub> photocatalyst.

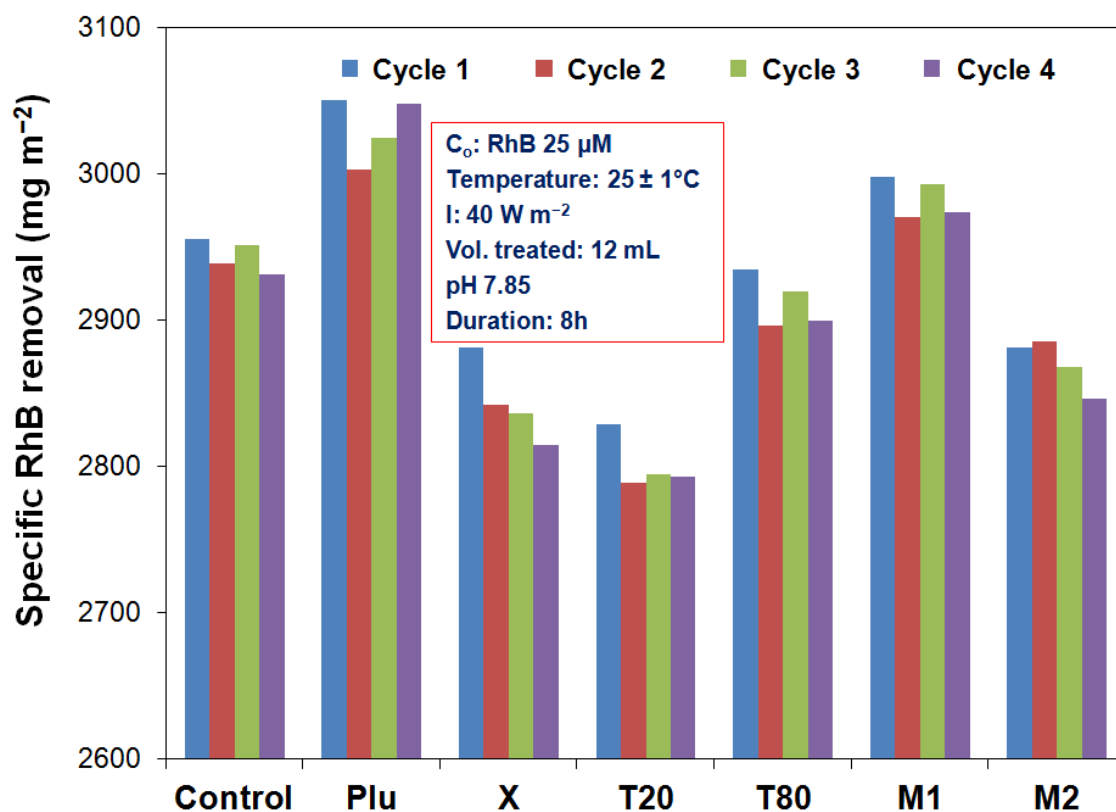
The hierarchical configuration of different types of the TiO<sub>2</sub> photocatalytic ceramic membranes and some important characteristics are summarized in Table 5.2. The thickness of TiO<sub>2</sub> layer of the Control membrane specimen (312 nm) is relatively smaller than the other membrane specimens. The incorporation of SDA into the TiO<sub>2</sub> sols would increase the overall viscosity of the sol, resulting in a thicker TiO<sub>2</sub> layer. Plu membrane contained the highest amount of TiO<sub>2</sub> loading among the one-SDA-type membrane specimens and consequently had the thickest TiO<sub>2</sub> layer (Table 5.2).



**Figure 5.8** Pure water permeability of different types of TiO<sub>2</sub> photocatalytic ceramic membranes (the numerical values depict average pure water permeance in L m<sup>-2</sup> h<sup>-1</sup> Bar<sup>-1</sup>).

Fig. 5.8 shows the pure water permeability of different types of the TiO<sub>2</sub> membranes. The macroporous alumina ceramic support could allow average pure water permeance of 309 L m<sup>-2</sup> h<sup>-1</sup> Bar<sup>-1</sup>. The resulting pure water permeability of the membranes is strongly dependent on the thickness and the porous structure of the TiO<sub>2</sub> membranes. T80 membrane showed the highest pure water permeability among the one-SDA-type membrane which could be attributed to its most porous top separation layer (T80-0.5). On the other hand, Plu membrane showed the lowest pure water permeability among the SDA-modified membranes due to its least porous separating layer (P-0.5). M1 membrane was constructed such that each of its photocatalytic layers was of the most porous TiO<sub>2</sub> layers (3 P-2.0 sub-layers, followed by 2 T20-1.0 sub-layers and a thin T80-0.5 top separation layer). As expected, M1 membrane showed the highest pure water permeance of 155 L m<sup>-2</sup> h<sup>-1</sup> Bar<sup>-1</sup>. Consequently, M1 membrane showed the least PEG rejection of 76%. The other mixed membrane (M2) showed a relatively high pure water permeance of 121 L m<sup>-2</sup> h<sup>-1</sup> Bar<sup>-1</sup>. Although the Control membrane possessed the thinnest TiO<sub>2</sub> photocatalytic layer, the pure water permeance was the lowest among the membrane specimens (109 L m<sup>-2</sup> h<sup>-1</sup> Bar<sup>-1</sup>) which could be attributed to the low porosity TiO<sub>2</sub> layers. The pure water permeability of the SDA-modified TiO<sub>2</sub> membranes is generally higher than those reported in the literature (Choi et al. 2006d, Qi et al. 2013, Romanos et al. 2013). The relatively high pure water permeability of the membranes could be also attributed to the PSH phenomena of the membrane. This is a very important aspect for the operation of membrane separation process whereby high permeability would reduce the overall energy consumption in the water and wastewater treatment processes. The trend observed for the pure water permeability is also in agreement with the PEG rejection profile, i.e. the least porous membrane rejected the highest percentage of the PEG solution.

### 5.3.3 Photocatalytic degradation of RhB using batch photoreactor



**Figure 5.9** Performances of different types of TiO<sub>2</sub> photocatalytic ceramic membranes in the batch photoreactor.

Fig. 5.9 shows the performances of different types of the TiO<sub>2</sub> membranes using the batch photoreactor for 8 h. The photolysis of 25 μM RhB under continuous UV irradiation (without the presence of the membrane) was < 5 %. In the presence of TiO<sub>2</sub> coated membrane, the rate of RhB degradation in the batch photoreactor was controlled by mass transfer rate, intra-layer pollutant diffusion, and adsorption/desorption equilibrium. It could be observed that the Plu membrane removed the highest amount of RhB (3,000 mg m<sup>-2</sup>) over the 8 h duration of treatment in the batch photoreactor. This could be explained by its highest TiO<sub>2</sub> content in the top layer of the membrane. The membrane with the least amount of TiO<sub>2</sub>, T20, could remove up to 2,800 mg m<sup>-2</sup> of RhB from its solution over the same treatment duration. The small

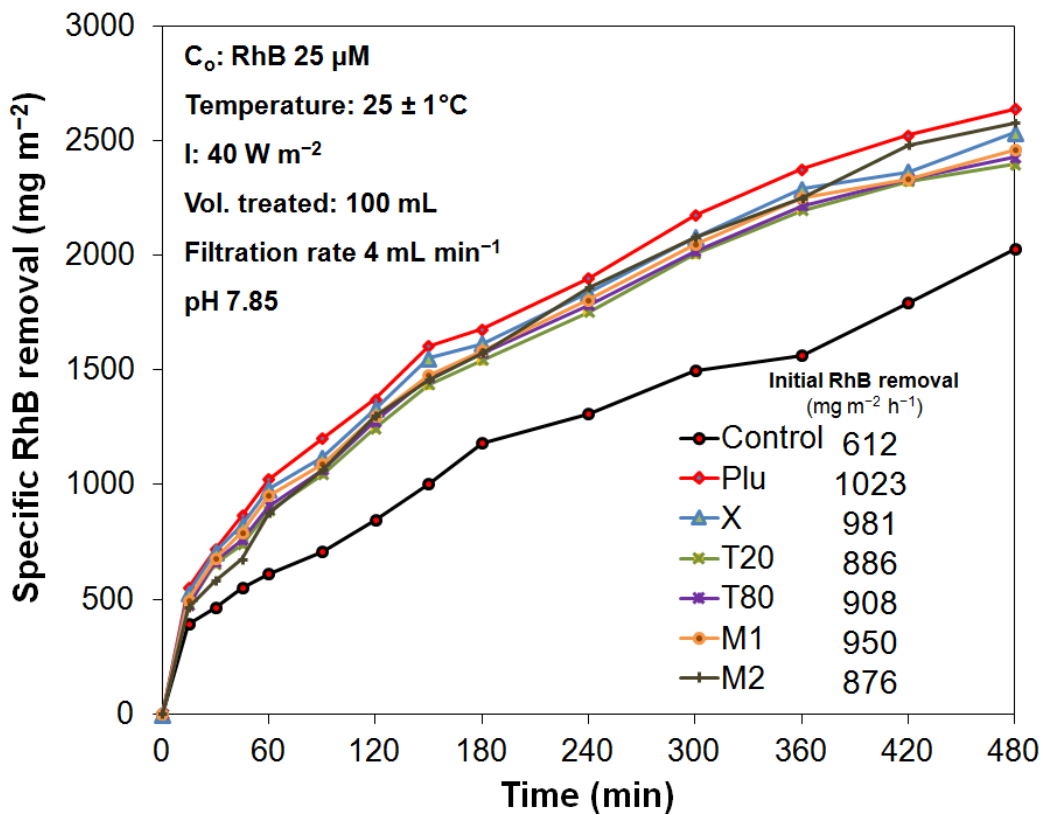
variation in the RhB removal efficiency among the TiO<sub>2</sub> membranes suggested that the effect of thickness and porous structure of the TiO<sub>2</sub> layers on the RhB removal efficiency in the batch photoreactor was marginal.

The degradation of RhB could be monitored by UV-Vis spectrophotometer as the maximum absorbance of the RhB solution would shift gradually from 553 nm to 498 nm. The gradual shift was caused by the step-wise de-ethylation of RhB to form the rhodamine solution (from the initial N, N, N', N'-tetraethyl rhodamine to the final rhodamine molecules). The observed color of the RhB solution also changes from the initial pinkish-red to a light greenish-yellow and finally to a transparent solution. The photodecolorization of the chromogenic aromatic ring and the dissociation of ethyl branches from RhB occurred simultaneously (Xie et al. 2009). In order to determine the extent of mineralization of RhB solution, the TOC of the treated RhB solutions from the batch photoreactor was measured. It was found that all the treated solutions showed a final TOC concentration smaller than 1 mg L<sup>-1</sup> after 8 h, which was the detection limit of the equipment. This finding indicated > 90% TOC removal from the initial RhB solution (from the initial TOC of 8.6 mg L<sup>-1</sup> corresponding to 25 μM solution). The membranes were also used up to 4 cycles of treatment in the batch photoreactor. There was no significant drop of RhB removal efficiency (Fig. 5.9), indicating that the TiO<sub>2</sub> membranes could be re-used.

#### **5.3.4 Photocatalytic degradation of RhB using PMR.**

The results of experiments using the PMR are shown in Figs. 5.10-5.12 and Table 5.3. The efficacy of different membranes to remove RhB is illustrated in Fig. 5.10 and reported as specific RhB removal. The numerical values shown in Fig. 5.10 depict the initial rate of RhB removal. All membranes showed a rapid initial RhB removal which could be attributed by

initial RhB adsorption by the membrane. After which the photocatalytic degradation initiated by UV irradiation would take place. Plu membrane showed the highest specific RhB removal of  $2,657 \text{ mg m}^{-2}$  for 8 h of treatment duration in the PMR. Interestingly, M2 membrane shows the second highest removal ( $2,577 \text{ mg m}^{-2}$ ) followed by X, M1, T80, and T20 membranes. It is shown that a membrane constructed from  $\text{TiO}_2$  layers prepared using different SDAs exhibited no compatibility issue among the different SDA-modified  $\text{TiO}_2$  layers thus also exhibited a good RhB removal efficiency.



**Figure 5.10** Performances of different types of  $\text{TiO}_2$  photocatalytic ceramic membrane in the PMR (the numerical values depict kinetic value based on initial RhB removal rate within 1<sup>st</sup> hour in  $\text{mg m}^{-2} \text{ h}^{-1}$ ).

The contributions of different phenomena (i.e. PCA and Ads-MR) that were responsible for the overall removal of RhB in the PMR are summarized in Table 5.4. Prior to the light on of UV source, the PMR cell module was filled with RhB solution and left in the dark for 1 h in order to reach the adsorption-desorption equilibrium. Among the SDA-modified membranes, Plu membrane showed the highest contribution of Ads-MR ( $501 \text{ mg m}^{-2}$ ) due to its thickest  $\text{TiO}_2$  layer. The contribution of Ads-MR on the overall efficiency of RhB removal varied from 9.5 to 17.5% ( $235$  to  $466 \text{ mg m}^{-2}$ ) for the SDA-modified membranes. The highest contribution of Ads-MR among the SDA-modified membranes was observed for Plu membrane, followed by M2, T-20, T-80, X and M1 membranes. For M1 membrane, the lowest contribution of Ads-MR could be caused by its most porous structure (M1 membrane also showed the highest pure water permeability among the tested membrane specimens). The Control membrane showed the highest overall contribution of Ads-MR ( $529 \text{ mg m}^{-2}$ , 26.4%) compared to the SDA-modified membrane due to its least porous configuration hence a smaller overall surface area for adsorption. The overall contribution of adsorptive-membrane retention was lower than the result reported on author's previous work (Goei et al. 2013). This is due to the porosity gradient configuration that was shown to improve the flux and overall PCA efficiency was adopted for the present work.

RhB molecules were photocatalytically degraded as their travelled through the porosity gradient of  $\text{TiO}_2$  layers. All the SDA-modified  $\text{TiO}_2$  photocatalytic ceramic membranes showed more than 81% contribution of photocatalytic degradation to the overall RhB removal. M1 membrane showed the largest contribution of PCA ( $2,234 \text{ mg m}^{-2}$ , 89.9%) to the overall RhB removal. This could be attributed to its most porous structure, allowing a higher flux through the membrane and hence higher photocatalytic degradation. Even the

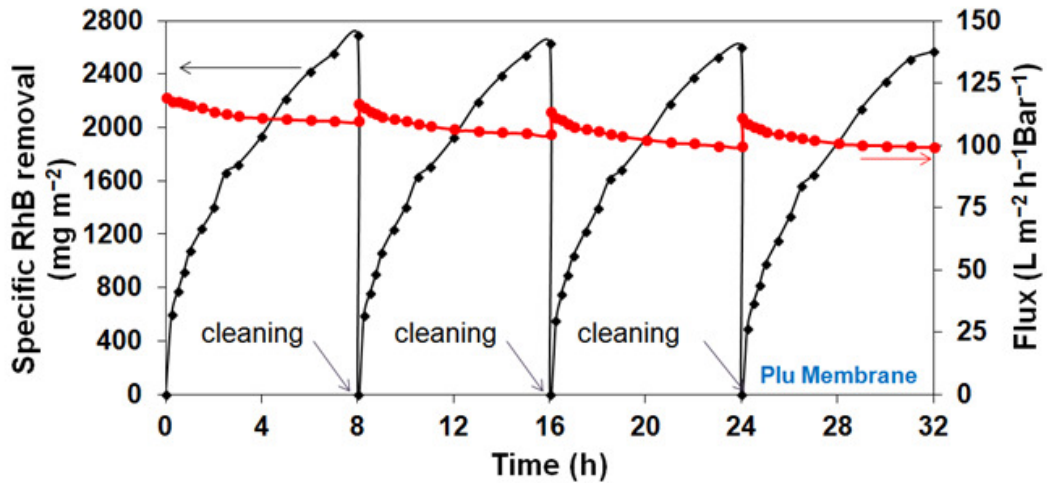
Control membrane with a relatively small porous structure could remove 1,476 mg m<sup>-2</sup> of RhB through the photocatalytic degradation.

**Table 5.4** Performance of TiO<sub>2</sub> photocatalytic ceramic membrane in terms of its photocatalytic activity (PCA) and adsorptive-membrane retention (Ads-MR) and percentage of initial flux retained after 8 h of operation

Types	Removal (mg m <sup>-2</sup> )			Removal (%)		Flux Decline (%)
	PCA	Ads-MR	Total	PCA	Ads-MR	
Plu	2156 ± 32	501 ± 16	2657 ± 30	81.1	18.9	93.3
X	2185 ± 70	364 ± 36	2549 ± 34	88.9	11.1	90.9
T20	2088 ± 48	319 ± 26	2407 ± 24	86.7	13.7	93.6
T80	2129 ± 27	302 ± 12	2431 ± 22	87.6	12.4	93.9
M1	2234 ± 32	249 ± 30	2483 ± 13	89.9	10.1	94.3
M2	2121 ± 40	456 ± 30	2577 ± 11	82.3	17.7	91.9
Control	1476 ± 14	529 ± 13	2005 ± 21	73.6	26.4	79.0

Fouling control is an important requisite of an efficient membrane process. The overall flux declines of different TiO<sub>2</sub> membranes over the duration of RhB photocatalytic degradation experiment are listed in Table 5.4. The SDA-modified TiO<sub>2</sub> photocatalytic ceramic membranes exhibited only a small percentage (maximum of 10 %) of flux decline over the duration of 8 h of photocatalytic degradation of RhB. The higher initial flux decline could be attributed to the cumulative adsorption of RhB molecules onto the membrane. After which, the smaller flux decline would be observed and the final steady-state flux would be achieved and maintained. The initial flux could be recovered by inter-cycle cleaning steps by replacing the feed with MilliQ water for 2 h with UV irradiation. Fig. 5.11 illustrates the reusability potential of the TiO<sub>2</sub> photocatalytic membrane. Over the duration of the first treatment cycle, 92% of the initial flux was maintained with 98% of the initial flux was

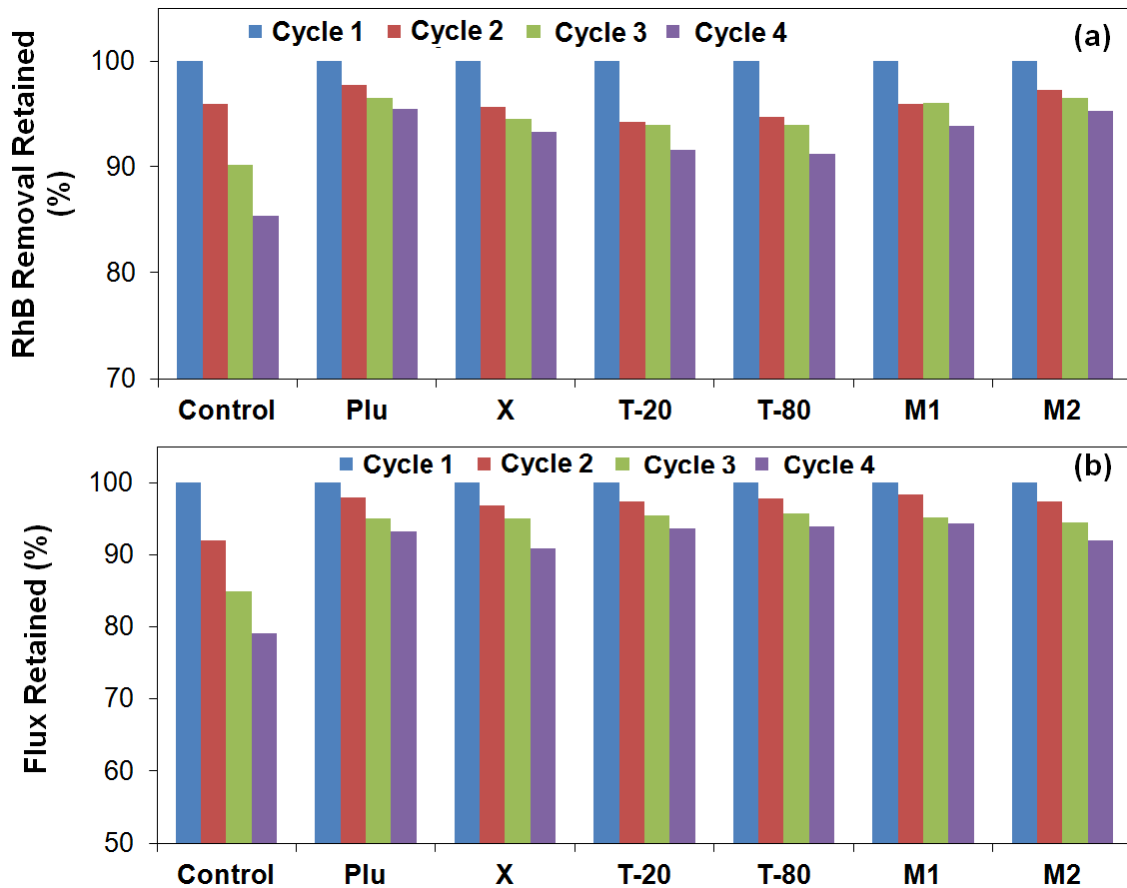
recovered after the first cleaning step. Even after 4<sup>th</sup> cycle of usage, 83% of the initial flux was maintained. The results suggest the potential of TiO<sub>2</sub> photocatalytic ceramic membrane to be reused over a prolonged period.



**Figure 5.11** Reusability potential of the TiO<sub>2</sub> photocatalytic ceramic membrane in terms of flux and specific RhB removal performance with UV-assisted inter-cycle cleaning.

Fig. 5.12 summarizes the performances of different TiO<sub>2</sub> membranes when they were utilized over 4 cycles of treatment with the inter-cycles cleaning steps. The highest decrease of total RhB removal and % flux retained showed by the Control membrane. Only 85% of the initial RhB removal capacity and 79% of the initial could be retained. Better performance was shown by the membranes with porosity gradient configuration. Plu membranes could retain the highest (95.9%) total RhB removal capability respectively after 4 treatment cycles followed by X, T-20, T-80, M1 and M2 membranes respectively. The percentages of the initial flux retained after 4 treatment cycles for Plu, X, T-20, T-80, M1 and M2 membranes are 93.3, 90.9, 93.6, 93.9, 94.3, and 91.9% respectively. The results suggested the ability of the membrane to control fouling via UV-assisted self-cleaning mechanism that preserved the

removal capability and flux flowing through the membrane. It can also be observed from Fig. 5.12 that the decline of flux and overall RhB removal capability of the subsequent treatment cycle is decreasing. This indicated the possibility of attaining a steady-state sustainable flux and overall RhB removal capability in the subsequent treatment cycles.



**Figure 5.12** Reusability potential of different types of TiO<sub>2</sub> photocatalytic ceramic membranes in terms of (a) specific RhB removal retained and (b) flux retained after each UV-assisted inter-cycles cleaning (8h for each cycle).

## 5.4 Conclusions

The hierarchically porous TiO<sub>2</sub> photocatalytic ceramic membranes have been successfully constructed by using TiO<sub>2</sub> layer prepared with different SDAs. The membranes possessed a porosity gradient configuration that was achieved by multilayer coating of TiO<sub>2</sub> layers of unique porous structures. 4 different SDAs were used in the preparation of the TiO<sub>2</sub> sol i.e. Pluronic P-123, Triton X-100, Tween 20 and Tween 80. Six types of membranes were prepared, 2 of which consisted of TiO<sub>2</sub> layers prepared incorporating different types of SDAs. The TiO<sub>2</sub> sols prepared using different SDAs exhibited a good compatibility among them, allowing the flexibility of constructing the TiO<sub>2</sub> membrane that exhibited favorable operating parameters, i.e., high permeability, good separation or both. Membrane M1 exhibited the highest flux performance while membrane Plu exhibited the largest RhB removal. The TiO<sub>2</sub> photocatalytic membrane could remove RhB from its solution through different processes which were classified as Ads-MR and PCA. The reusability potential of the TiO<sub>2</sub> membranes has been showed using both the batch photoreactor and flow-through PMR which would reduce the overall operating cost of the treatment system.

# CHAPTER 6 SILVER-DECORATED TiO<sub>2</sub> PHOOCATALYTIC CERAMIC MEMBRANE WITH HIERARCHICAL ARCHITECTURE: PHOTOCATALYTIC AND ANTIBACTERIAL ACTIVITIES

## 6.1 Introductions

In order to improve the photocatalytic activity of TiO<sub>2</sub>, doping of various metallic and non-metallic element was advocated (Chen and Mao 2007). Among the possible metal dopants, Ag is favorable due to its remarkable catalytic, electric, and specific optical characteristics (Morones et al. 2005, Roucoux et al. 2002). Also, Ag nanoparticles have exhibited the highest bactericidal activity and biocompatibility among other bactericidal nanoparticles (Akhavan and Ghaderi 2010, Gumy et al. 2006, Li et al. 2008). The synergistic coupling of Ag and TiO<sub>2</sub> is attributed to the Schottky barriers that are formed due to the difference in their work function. The Schottky barriers facilitate electron transfer from a higher Fermi energy level TiO<sub>2</sub> to Ag which would then reduce molecular oxygen to produce reactive oxygen radicals. This phenomenon would lead to a better charge separation thus inhibiting photogenerated electrons and holes recombination (Kubacka et al. 2008, Seery et al. 2007, Subba et al. 2003, Yu et al. 2005). Furthermore, Ag doping would add an additional functionality of anti-bacterial/anti-biofouling property to the already robust TiO<sub>2</sub> photocatalyst. However, there exists an optimum level of Ag doping, beyond which photohole trapping effect (increase in the probability of recombination by suppressing active photogenerated charge transfer to the reactant species at the surface) would happen (Ma et al. 2009a, Yin et al. 2004).

Recently, there are many research efforts to incorporate Ag nanoparticles into a membrane filtration setup (including some treatment systems that combine Ag anti-bacterial property, TiO<sub>2</sub> photocatalysis, and membrane filtration). For instance, Krylova et al. (2009) have deposited Ag nanoparticles onto different ceramic support (such as silica, titania, and zirconia) by sol-gel method. Liu et al. (2013a) fabricated Ag-loaded nanocomposite nanofiltration (NF) and forward osmosis (FO) membranes via layer-by-layer assembly method. Ma et al. (2009a) prepared a Ag-TiO<sub>2</sub>/HAP/Al<sub>2</sub>O<sub>3</sub> composite to that exhibited improved adsorption of bacterial cells and good anti bacterial property. Ma et al. (2010) also fabricated Ag-TiO<sub>2</sub>/HAP microfiltration (MF) membrane to treat humic acid solutions. Liu et al. (2013b) designed a direct observation experiment to study the effect of Ag nanoparticles on the bacteria deposition and its associated detachment kinetics from a polysulfone membrane. Lei et al. (2011) synthesized Ag/AgCl coated polyacrylonitrile nanofiber membranes that possess a high photocatalytic activity. Lv and coworkers (Lv et al. 2009a, Lv et al. 2009b) have fabricated Ag-decorated porous ceramic composite for the inactivation of *E. coli*. Yin et al. (2013) have attached Ag nanoparticles to the surface of polyamide membrane that showed an anti biofouling property.

In this chapter, the fabrication of different types of Ag-decorated TiO<sub>2</sub> photocatalytic membranes that possess a hierarchically porous architecture was described. Hierarchically porous architecture is a preferred structure to allow optimum operating parameters of photocatalytic membrane (Colombo et al. 2010). In this architecture, porosity gradient was obtained through coating of multi- photoactive layers of different pore structures (coating with larger pore size on the support-photocatalyst interface). Pluronic P-123 triblock copolymer was incorporated into the preparation of TiO<sub>2</sub> sol to control the microstructure of the resulting gel. This was achieved by the formation of a periodic nanostructure caused by

microphase separation of the incompatible polymer blocks of P-123. Besides, EO-type nonionic surfactants such as P-123 could assist reduction of  $\text{Ag}^+$  to  $\text{Ag}^0$  through the oxidation of their oxyethylene group to aldehydes (Andersson et al. 2002, Liz-Marzán and Lado-Touriño 1996). Various characterization techniques were employed to elucidate the physico-chemical and morphological characteristics of the membranes. Different performance parameters were used to evaluate the photocatalytic activity and anti-bacterial action of the membranes. Finally, it was the objective of this chapter to gain an insight into different phenomena that govern the performance of the  $\text{Ag-TiO}_2$  membranes including their various anti-bacterial actions and its reusability potential.

The potential applications of the  $\text{Ag-TiO}_2$  membranes are not only limited to remove turbidity and pathogen in the water and wastewater treatment but also to remove organic pollutants as a hybrid UF/NF photocatalytic membrane in the filtration system (as a reactive membrane). The multi-functionality of the  $\text{Ag-TiO}_2$  membrane and its reusability potential are important criteria for the application of low cost yet effective photocatalytic membrane treatment system.

## **6.2 Experimental procedures**

### **6.2.1 Membrane fabrication**

$\text{Ag}$ -decorated  $\text{TiO}_2$  ( $\text{Ag-TiO}_2$ ) sols were prepared with the incorporation of Pluronic P-123 as the SDA (Section 3.1.4).  $\text{AgNO}_3$  was used as the  $\text{Ag}$  source. The  $\text{Ag-TiO}_2$  sols had a molar ratio of  $\text{IPA:HNO}_3:\text{TTIP:H}_2\text{O}$  equals to 60:4:1:4. Variable amounts of P-123 and  $\text{AgNO}_3$  were used in the preparation of different sols to obtain  $\text{Ag-TiO}_2$  sols that contained 0.5, 1.0, 2.0, 5.0, or 10 wt% of P-123 and 0.5, 1.0, 2.0, 3.0 mol% of  $\text{Ag}$  (with respect to  $\text{TiO}_2$ ) respectively. The resulted  $\text{TiO}_2$  layers hereafter are referred as  $\text{PX-AgY}$  where X and Y are the amounts of P-123 and  $\text{Ag}$  added respectively.

**Table 6.1** Types of Ag-TiO<sub>2</sub> photocatalytic membrane fabricated

Types	Layers coated			TiO <sub>2</sub> loading ( $\mu\text{g cm}^{-2}$ )	Thickness of Ag-TiO <sub>2</sub> layer (nm) <sup>a</sup>	PEG rejection (%) <sup>b</sup>	Water Permeance ( $\text{L m}^{-2} \text{h}^{-1}$ $\text{Bar}^{-1}$ )
	1 <sup>st</sup> (bottom) 3-sub-layers	2 <sup>nd</sup> 2-sub-layers	3 <sup>rd</sup> (top) 1-layer				
R1	P10-Ag0.0	P5.0-Ag0.0	P2.0-Ag0.5	$58.6 \pm 7.1$	$323 \pm 39$	$75.2 \pm 0.6$	$159 \pm 1$
R2	P10-Ag0.5	P5.0-Ag0.5	P2.0-Ag0.5	$48.3 \pm 7.7$	$260 \pm 41$	$76.4 \pm 2.6$	$146 \pm 2$
R3	P5.0-Ag0.0	P2.0-Ag0.0	P1.0-Ag0.5	$70.3 \pm 5.2$	$341 \pm 25$	$78.8 \pm 0.6$	$142 \pm 3$
R4	P5.0-Ag0.5	P2.0-Ag0.5	P1.0-Ag0.5	$65.8 \pm 9.9$	$298 \pm 45$	$82.5 \pm 1.3$	$129 \pm 3$
R5	P5.0-Ag0.0	P2.0-Ag0.0	P1.0-Ag1.0	$78.5 \pm 5.6$	$355 \pm 24$	$80.1 \pm 1.2$	$134 \pm 2$
R6	P5.0-Ag1.0	P2.0-Ag1.0	P1.0-Ag1.0	$72.9 \pm 10.8$	$325 \pm 40$	$84.8 \pm 0.5$	$123 \pm 2$
Plu D <sup>c</sup>	P10-Ag0.0	P5.0-Ag0.0	P2.0-Ag0.0	$130.3 \pm 10.3$	$598 \pm 38$	$72.3 \pm 1.4$	$160 \pm 1$

<sup>a</sup> Determined by considering different porosities of each sub-layers and assuming uniform density of anatase and metallic silver of 3.9 and 10.5 g cm<sup>-3</sup> respectively.

<sup>b</sup> Determined using PEG of MW 20,000 g mol<sup>-1</sup>.

<sup>c</sup> Obtained from author's previous work [Goei et al. (2013)] as control.

The hierarchical architecture of Ag-TiO<sub>2</sub> membrane was obtained by coating different sols on the alumina support. Prior to the coating, the alumina support was coated with 5 wt% PVA solution and air dried to prevent possible infiltration of TiO<sub>2</sub> sol into the alumina support. One side of the alumina support was covered to allow only single-side coating of Ag-TiO<sub>2</sub> sols. The alumina support was then dipped into the designated Ag-TiO<sub>2</sub> sol for 60 s using a home-fabricated dip-coater, and withdrawn at a rate of 2 mm s<sup>-1</sup>. The coated membrane was first oven dried (103°C, 15 min), then calcined in the muffle furnace (Nabertherm LHT04/16) at 500°C for 1 h (3°C min<sup>-1</sup> heating rate). Six different membrane specimens of different hierarchical architectures were fabricated and they are summarized in Table 6.1. The first photocatalytic layer was formed through 3 coatings of the similar sol resulting into the formation of 3-sub-layers. The intermediate layer which consists of 2-sub-layers was formed through 2 coating of another sol. Finally, a thin top-layer was coated once with Ag-containing sol. R1, R3, and R5 were decorated with Ag only in the top-most layer

while R2, R4, and R6 were decorated with Ag in all sub-layers. All the membranes were UV irradiated ( $\lambda_{\max} = 365 \text{ nm}$ ,  $60 \text{ W m}^{-2}$ ) for 1 h (after the heat treatment of each coated sub-layers) in order to reduce  $\text{Ag}^+$  species in the membrane to metallic  $\text{Ag}^0$ . A previously prepared Ag-free  $\text{TiO}_2$  membrane, Plu D, was included in the present study for comparison (Goei et al. 2013). In order to characterize the microstructure of the Ag- $\text{TiO}_2$ , a thick Ag- $\text{TiO}_2$  layer was also coated onto a Petri dish. The resulting layer was then scrapped off, heat treated, pulverized, and stored for its subsequent characterizations.

### 6.2.3 Evaluation of membrane performance

The photocatalytic activity of the membrane was evaluated both using the batch photoreactor (Section 3.4.2) and the PMR (Section 3.4.3) against photocatalytic degradation of RhB. In a typical experiment in the batch photoreactor, each types of membrane were used to treat 12 mL of RhB solution without any stirring and oxygen bubbling. The extent of the photodegradation of RhB was monitored using UV/Vis spectrophotometer at 553 nm.

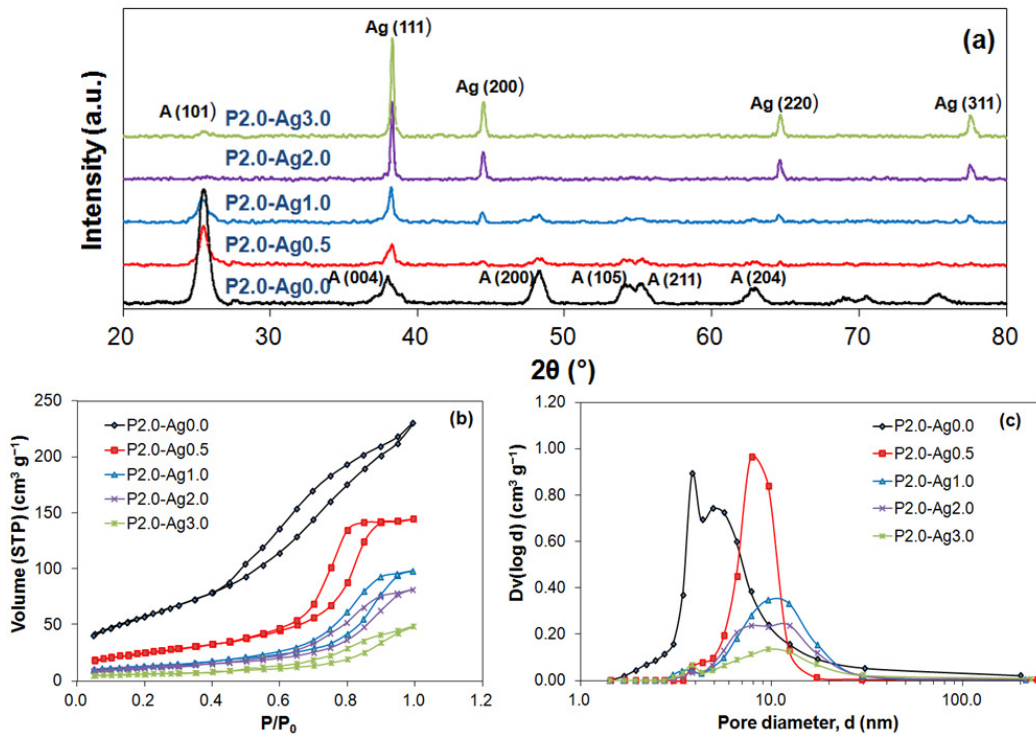
The PMR setup was used to evaluate the performance of the membrane in the dead end filtration mode. The coated membrane disc was mounted and secured tightly in the membrane cells. The pure water permeability and the MWCO of the membrane were evaluated using the PMR. The membrane was also used to treat up to 5 cycles of 100 mL of 25  $\mu\text{M}$  RhB solutions. Control experiments without turning on the UV source were performed to elucidate the effect of Ads-MR on the removal of RhB. The overall RhB removal could be attributed to 2 different processes: PCA of the  $\text{TiO}_2$  layer and Ads-MR by the membrane.

The total amount of Ag leaching from the Ag- $\text{TiO}_2$  photocatalytic membrane was quantified using ICP-MS (Section 3.4.4). The study of diffusion inhibition zone of the Ag- $\text{TiO}_2$  photocatalytic membrane was performed (Section 3.4.5). The anti-bacterial performance

of Ag-TiO<sub>2</sub> photocatalytic membrane was also evaluated by the means of photocatalytic disinfection of *E. coli* both in the batch reactor (Section 3.4.6) and PMR (Section 3.4.7). Lastly, the ability of bacteria to undergo repair after the disinfection reaction was evaluated (Section 3.4.8).

## 6.3 Results and discussion

### 6.3.1 Characterization of Ag-TiO<sub>2</sub> layers



**Figure 6.1** (a) XRD spectra, (b) N<sub>2</sub> adsorption/desorption curves, and (c) pore size distribution of the pulverized Ag-TiO<sub>2</sub> layers with different amounts of Ag added.

The important physico-chemical characteristics of the as prepared Ag-TiO<sub>2</sub> layers are summarized in Table 6.2. Various types of Ag-TiO<sub>2</sub> materials have been prepared by acid-catalyzed sol-gel method. Thirty types of Ag-TiO<sub>2</sub> layers were prepared by varying its

Pluronic P-123 and  $\text{AgNO}_3$  content of the sols. The difference in the hydrophilicity of the polyethylene glycol and polypropylene glycol blocks of P-123 would cause a microphase separation. This phenomenon was responsible for micellar structure that would lead to the mesoporous structure formation of the resulting Ag-TiO<sub>2</sub> layers. The mesoporous structure was formed by attractive forces between titanium dioxide hydrate and P-123 and would crystallize during the calcination stage to obtain the final Ag-TiO<sub>2</sub> layers (Lu et al. 1997, Procházka et al. 2008).

The wide-angle XRD patterns of the representative Ag-TiO<sub>2</sub> sols are shown in Fig. 6.1a. It showed the XRD patterns of the pulverized Ag-TiO<sub>2</sub> with increasing Ag content (from 0 up to 3 mol% Ag) while the amount of P-123 added was kept constant. The XRD spectra show five distinctive anatase TiO<sub>2</sub> peaks at 25.3°, 37.9°, 48°, 54.6°, and 62.8° which correspond to (101), (004), (200), (105 and 211), and (204) reflections of crystalline TiO<sub>2</sub> anatase planes respectively (JCPDS 21-1272). No amorphous content was observed in the spectra indicating a successful formation of anatase crystals upon calcination at 500°C. Anatase phase was the most photocatalytically active form among the TiO<sub>2</sub> polyforms (Gaya and Abdullah 2008, Tanaka et al. 1993a). Four distinctive peaks of face-centered cubic metallic Ag at 38.1°, 44.3°, 64.5°, and 77.4° which correspond to (111), (200), (220), and (311) reflection were also observed in the spectra of Ag-containing sample (JCPDS 04-783). The result from XRD analysis confirmed the successful deposition of Ag on TiO<sub>2</sub> nanocrystals.

A high atom density facet of (111) crystal plane of metallic Ag was found to be a favorable condition for effective disinfections upon interaction with bacterial cell (Morones et al. 2005, Pal et al. 2007). TiO<sub>2</sub> crystallites size was calculated from the peak broadening of (101) anatase crystal plane at 25.3° using Scherrer's equation (Scherrer 1918) and are summarized in Table 6.2. The size of TiO<sub>2</sub> crystal decreased as the amount of P-123 loading

increased. This could be attributed to spatial confinement mechanism of P-123 scaffold (Guldin et al. 2011). The concentration of Ag doping would also affect the resulting TiO<sub>2</sub> crystallite size. Ag was found to suppress the growth of anatase crystal by inclusion of Ag nanoparticles on the mesoporous TiO<sub>2</sub> layer (Ma et al. 2011).

**Table 6.2** Physico-chemical characteristics of synthesized Ag-TiO<sub>2</sub> materials: (a) TiO<sub>2</sub> crystallite size, (b) BET surface area, and (c) BET porosity

<b>(a) TiO<sub>2</sub> Crystallite Size (nm)<sup>a</sup></b>					
<b>↓ P-123   Ag → (wt%)   (mol%)</b>	<b>0.0</b>	<b>0.5</b>	<b>1.0</b>	<b>2.0</b>	<b>3.0</b>
<b>0.0</b>	14.8	14.6	12.9	10.8	8.9
<b>0.5</b>	14.4	13.4	12.8	10.5	8.3
<b>1.0</b>	13.3	12.7	10.8	9.8	7.7
<b>2.0</b>	7.7	6.8	6	5.2	4.7
<b>5.0</b>	5.5	5.3	4.6	3.7	3.6
<b>10</b>	5	4.5	3.7	3.4	2.6

<b>(b) BET Surface Area (m<sup>2</sup> g<sup>-1</sup>)</b>					
<b>P-123   Ag</b>	<b>0.0</b>	<b>0.5</b>	<b>1.0</b>	<b>2.0</b>	<b>3.0</b>
<b>0.0</b>	27.68 ± 0.71	20.15 ± 0.70	17.55 ± 0.57	5.83 ± 0.13	1.61 ± 0.01
<b>0.5</b>	51.29 ± 0.76	35.15 ± 1.07	24.07 ± 0.25	13.81 ± 0.08	9.36 ± 0.23
<b>1.0</b>	82.19 ± 0.51	46.29 ± 0.57	34.91 ± 0.93	19.97 ± 0.14	10.84 ± 0.09
<b>2.0</b>	127.06 ± 2.95	49.33 ± 0.59	45.64 ± 0.29	36.33 ± 0.40	20.79 ± 0.27
<b>5.0</b>	139.41 ± 1.08	56.08 ± 0.47	53.59 ± 0.61	40.84 ± 0.18	30.51 ± 0.30
<b>10</b>	146.84 ± 1.07	75.52 ± 0.42	68.58 ± 0.52	48.72 ± 0.36	38.32 ± 0.28

<b>(c) BET Porosity (%)<sup>b</sup></b>					
<b>P-123   Ag</b>	<b>0.0</b>	<b>0.5</b>	<b>1.0</b>	<b>2.0</b>	<b>3.0</b>
<b>0.0</b>	14.19 ± 0.17	13.22 ± 0.22	11.23 ± 0.13	5.79 ± 0.21	3.97 ± 0.04
<b>0.5</b>	29.84 ± 0.19	28.53 ± 0.23	23.38 ± 0.26	16.35 ± 0.36	12.02 ± 0.14
<b>1.0</b>	34.60 ± 0.39	33.49 ± 0.26	29.86 ± 0.12	18.09 ± 0.17	14.05 ± 0.05
<b>2.0</b>	45.63 ± 0.32	40.52 ± 0.42	37.27 ± 0.43	33.05 ± 0.19	22.82 ± 0.09
<b>5.0</b>	47.98 ± 0.23	46.67 ± 0.33	43.86 ± 0.16	35.18 ± 0.07	32.26 ± 0.06
<b>10</b>	58.20 ± 0.21	51.41 ± 0.42	50.02 ± 0.07	45.70 ± 0.30	21.19 ± 0.10

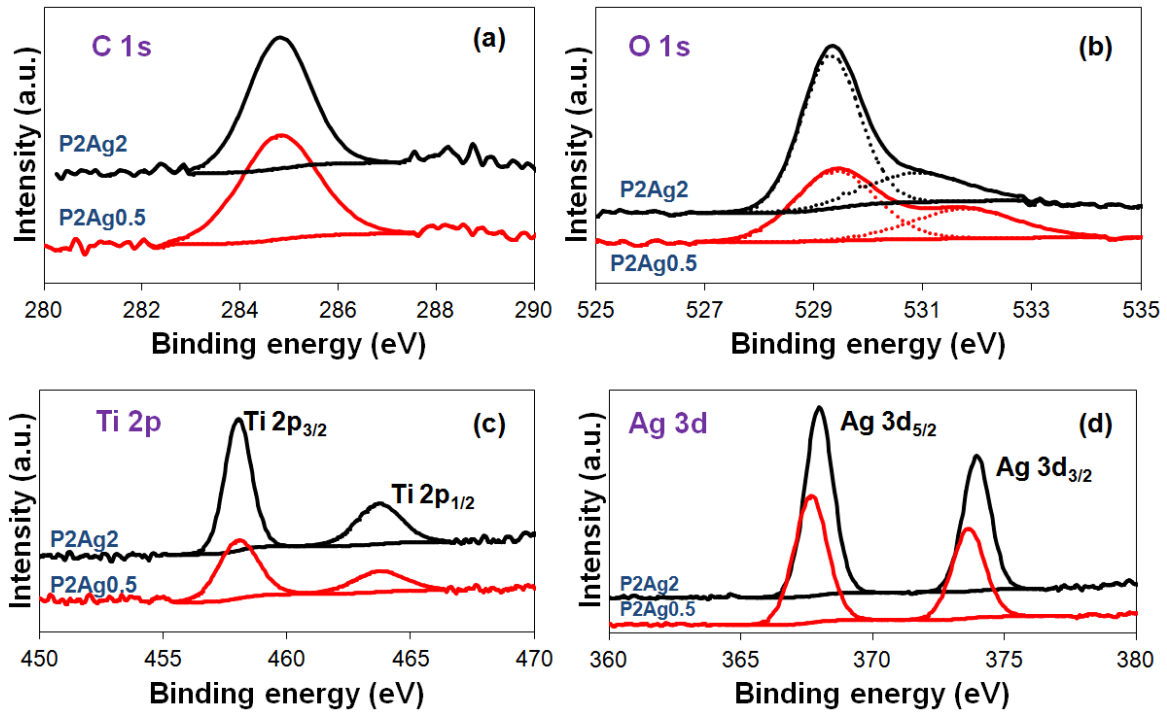
<sup>a</sup> Calculated using Scherrer's equation with error < 1 nm.

<sup>b</sup> Determined assuming uniform densities of anatase and metallic silver of 3.9 and 10.5 g cm<sup>-3</sup> respectively.

Further evidence of the ability to fine-tuning the resulting microstructure of Ag-TiO<sub>2</sub> layers just by altering the amount of P-123 and AgNO<sub>3</sub> added into the sol were obtained from N<sub>2</sub> adsorption/desorption isotherm characterization. The result is summarized in Table 6.2a-b, and Fig. 6.1b-c. A well developed mesoporous material was evidenced from a type-IV adsorption isotherm. The sharp hysteresis loops indicate that pore sizes in the Ag-TiO<sub>2</sub> layers are of narrow distribution. It has been observed that as the amount of P-123 added increased, the BET surface area and porosity of the resulting Ag-TiO<sub>2</sub> increased. More pore coalescence and multi-micellar interaction during calcination are expected for higher P-123 loading which would result in increase in pore size and overall porosity (Choi et al. 2006d). However, as the amount of Ag doping increased, the decreased in BET surface area and overall porosity was observed. This could be attributed to the inclusion of Ag nanoparticles into the mesoporous TiO<sub>2</sub> layers. The control of surface area and porosity profile is important to maximize the numbers of catalytic active sites.

XPS analyses were carried out to understand the chemical states of element in Ag-TiO<sub>2</sub> layers. Two samples of the pulverized Ag-TiO<sub>2</sub> layers (P2Ag0.5 and P2Ag2.0) were chosen as representative for the XPS analysis. The high resolution XPS spectra of C 1s, O 1s, Ti 2p, and Ag 3d core levels are presented in Fig. 6.2. There were 2 main peaks observed in O 1s, the dominant peak at 529.6 eV which was characteristics of metallic oxide and a smaller peak at 531.8 eV which was attributed to chemisorbed oxygen on the surface of Ag-TiO<sub>2</sub> layer. The adsorbed oxygen allows the H<sup>+</sup> hydroxylation to form -Ti(OH)-O-Ti-(OH)- bond which would generate hydroxyl radical that are beneficial for photocatalysis (Hoffmann et al. 1995). A separation of 5.7 eV of Ti 2p doublet indicates that Ti exists in Ti<sup>4+</sup> oxidation state. Distinct doublet was also observed at Ag 3d core level. A spin-orbit splitting energy of 6.0 eV for the 3d doublet of Ag indicates the formation of metallic Ag<sup>0</sup> (Moulder et al. 1992). No

peak from other form of Ag oxide (i.e. AgO or Ag<sub>2</sub>O) were observed) indicates the successful photoreduction of Ag species to Ag<sup>0</sup>.

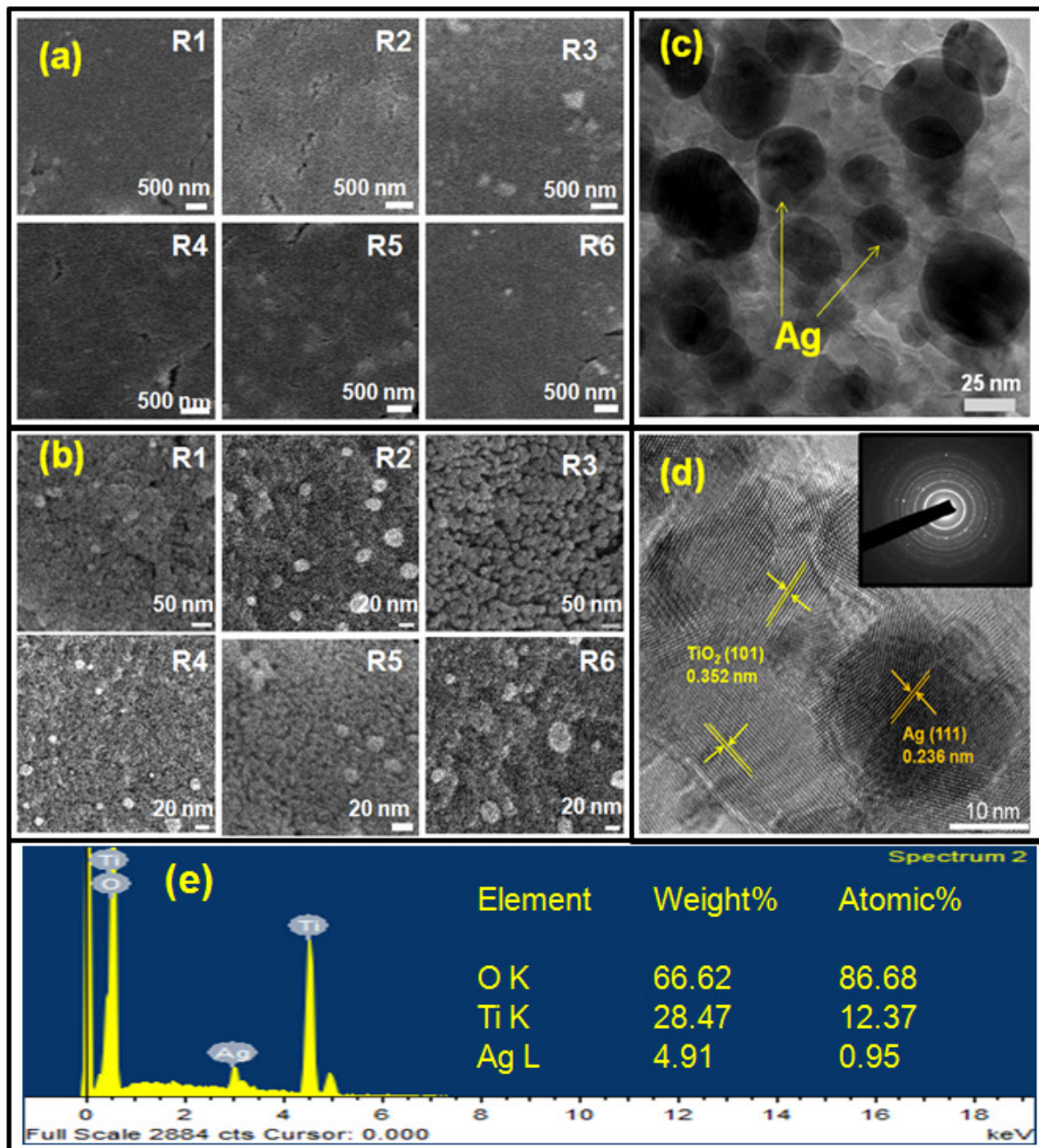


**Figure 6.2** High resolution XPS spectra of (a) C 1s, (b) O 1s, (c) Ti 2p and (d) Ag 3d regions of the pulverized Ag-TiO<sub>2</sub> layers.

### 6.3.2 Characteristics of Ag-TiO<sub>2</sub> membranes.

Six types of Ag-TiO<sub>2</sub> membrane with hierarchical architecture were fabricated. All membranes followed the following hierarchical architecture scheme: the first 3 sub-layers were the most porous, followed by subsequent 2 less porous sub-layers, and finally a thin least porous separating layer was coated. For comparisons, Plu D membrane from author's previous study (Goei et al. 2013) was also fabricated. R1 and R2 membranes were prepared similar to Plu D by using P10, P5, and P2 sols. R1 used TiO<sub>2</sub> sol doped with 0.5 mol% Ag only on the top-most sub-layer, while R2 used TiO<sub>2</sub> sols doped with 0.5 mol% Ag in all of its sub-layers. R3 and R4 membranes were prepared using P5, P2, and P1 sols which structure

were analogous to R1 and R2. Finally, R5 and R6 membranes were prepared using P5, P2, and P1 sols which structure analogous to R3 and R4 but using instead a 1 mol% of Ag-decorated TiO<sub>2</sub> sol.



**Figure 6.3** FESEM micrographs of Ag-TiO<sub>2</sub> photocatalytic membrane at (a) low and (b) high magnifications. (c) TEM and (d) HRTEM micrographs of R2 membrane (the inset depicts the corresponding SAED pattern). (e) EDX of the surface of R2 membrane.

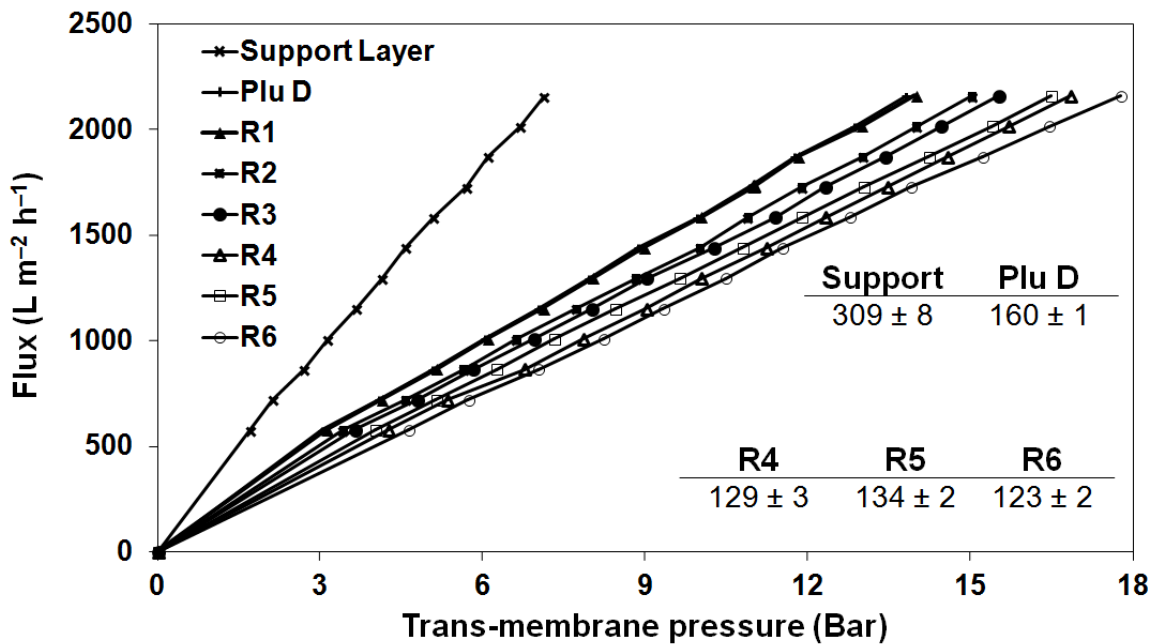
Fig. 6.3a shows FESEM micrographs of the membrane surface with the corresponding high magnification micrograph shown in Fig. 6.3b. The FESEM images suggest that a relatively smooth Ag-TiO<sub>2</sub> layer has been successfully coated onto the surface of the alumina support. The coated layers showed a minimal presence of cracks and pinholes which was important to ensure uniform permeability and good separation performance. Apparent presence of well-dispersed Ag nanoparticles (particles that appear brighter) could be observed from the high magnification FESEM micrographs of the membrane. It showed a successful dispersion of Ag nanoparticles (approximately 20 nm in diameter) onto TiO<sub>2</sub> matrix.

TEM micrograph of scrapped photoactive layers of R2 membrane (Fig. 6.3c.) revealed a dispersion of spherical Ag nanoparticles into the cluster of smaller TiO<sub>2</sub> nanoparticles. This is in agreement with earlier FESEM observation. However, some of the Ag nanoparticles were found in the agglomerated form. Ag nanoparticles are more prone to agglomeration at a higher Ag loading (Herrmann et al. 1988). HRTEM micrograph of the same membrane R2 (Fig. 6.3d.) confirms the successful formation of TiO<sub>2</sub> anatase crystals and deposition of Ag<sup>0</sup> nanoparticles. Fig. 6.3e depicts an EDX elemental analysis spectrum of a randomly selected area on the surface of R2 membrane. Ag loading was 0.5 mol% at all the sub-layers coating of R2. However, the elemental analysis showed a slightly higher Ag concentration. This indicates that Ag tends to agglomerate at the surface of the membrane. This observation is important to explain a high anti-bacterial activity of the Ag-TiO<sub>2</sub> membrane.

The hierarchical architecture of the Ag-TiO<sub>2</sub> membrane and some important characteristics are summarized in Table 6.1. Few trends could be observed from the characteristics of membranes of different hierarchical architectures. Firstly, membrane decorated with Ag tends to possess a thinner photoactive layer than the one without (323 nm

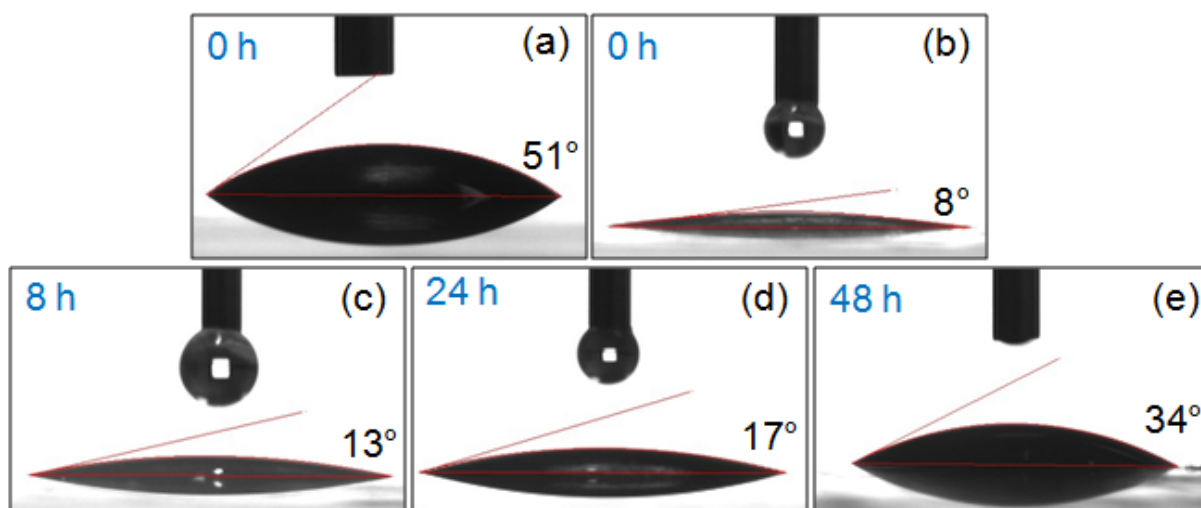
of R1 vs 598 of Plu D). In the same manner, membrane with all sub-layers decorated with Ag was thinner than the one decorated with Ag only on the top-most layer. Consequently, membrane with thinner photoactive layer had a smaller amount of TiO<sub>2</sub> loading. This might be due to different in the viscosity of the sols. TiO<sub>2</sub> sol with higher P-123 and Ag loading tends to be less viscous, thus a thinner layer would be coated.

Secondly, R2, R4, and R6 membranes showed a higher PEG (MW 20,000 g mol<sup>-1</sup>) rejection than R1, R3, and R5 membranes respectively. This showed the effect of Ag doping that would lower the porosity and overall surface area of the TiO<sub>2</sub> layers that eventually affect the resulting PEG rejection profile. The 20,000 g mol<sup>-1</sup> PEG solution correspond to PEG molecular size of 12 nm (Choi et al. 2006a) which is in a good agreement with the porosity profile obtained from N<sub>2</sub> porosimetry analysis.



**Figure 6.4** Pure water permeability of Ag-TiO<sub>2</sub> photocatalytic membrane (The numerical values depict average pure water permeance in L m<sup>-2</sup> h<sup>-1</sup> Bar<sup>-1</sup>).

Thirdly, membranes with a more porous photocatalytic layer would exhibit larger pure water permeability. The numerical value of pure water fluxes of different membranes as a function of TMPs (Fig. 6.4) are listed in Table 6.1. It can be observed that the pure water permeability flux of the membranes increased linearly with the TMP regardless of the types of their hierarchical architectures. R1 and R2 membranes showed higher fluxes due to their more porous structure. All the membranes with Ag in all of its sub-layers showed a marginally smaller flux (< 10% difference) when compared with its counterpart which was consistent with the observation from N<sub>2</sub> porosimetry analysis. This suggests that by altering the amount of Ag incorporated would only marginally affect the resulting pure water permeability performance. Even the ‘tightest’ membrane (R6) showed a relatively high pure water permeability of 123 L m<sup>-2</sup> h<sup>-1</sup> Bar<sup>-1</sup> which could be attributed to the photo-induced super-hydrophilicity (PSH) of the membrane.



**Figure 6.5** Photo-induced super-hydrophilicity of R6-like thin film coated on a borosilicate glass as shown on (a) as coated thin film, (b) upon 1 h of UV irradiation, and after (c) 8 hr, (d) 24 h, and (e) 48 h left in the dark.

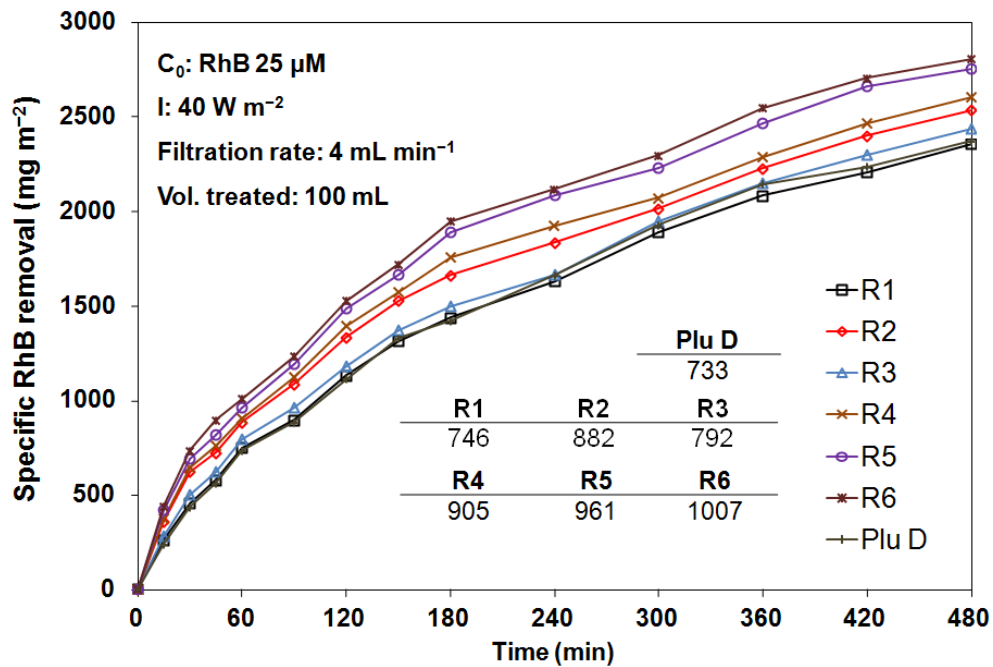
The evidence of PSH property of the membrane is shown in Fig. 6.5. The coated R6-like thin film shows a contact angle of  $51^\circ$  which subsequently decreased to  $8^\circ$  after 1 h of UV irradiation. This result illustrated the photo-induced super-hydrophilicity property of Ag-TiO<sub>2</sub> thin film. When the UV source was switched off, the contact angle increased again to  $13^\circ$ ,  $17^\circ$  and  $34^\circ$  after 8, 24 and 48 h respectively.

### 6.3.3 Photocatalytic degradation of RhB in the PMR reactor

Fig. 6.6 shows the specific RhB removal (i.e. the cumulative RhB removal per unit area of membrane over a period of time,  $\text{mg m}^{-2}$ ) of the Ag- TiO<sub>2</sub> membrane. The photolysis of RhB at 25  $\mu\text{M}$  under continuous UV irradiation (without the presence of the membrane) was  $< 5\%$ . All the membranes with Ag in all of its sub-layers showed a higher specific RhB removal as compared to the membrane with Ag only on its top-most layer. R6 showed the highest specific RhB removal owing to its tightest pore structure and highest amount of Ag incorporated. R5 and R6 membranes, which contained higher amount of Ag, showed a higher specific RhB removal as compared to their respective counterparts, R3 and R4 membranes. R1 and R2 showed a higher specific RhB removal than the control specimen Plu D.

The overall RhB removal could be attributed to two different phenomena: photocatalytic activity (PCA) of the TiO<sub>2</sub> layer and adsorptive-membrane retention (Ads-MR) of the membrane. The contribution of each of these phenomena is summarized in Table 6.3. It can be observed that the RhB removal through the adsorptive-retention by the membrane was lower than the removal through photocatalytic degradation. R2, R4, and R6 membranes showed a higher removal through adsorptive-retention as compared with its R1, R3, and R5 counterparts respectively. Incorporation of Ag in all sub-layers of R2, R4, and R6 caused RhB to pass through the more tortuous path of the membrane smaller porous architecture.

When compared with Plu D, the Ag-TiO<sub>2</sub> membrane showed (with the exception of R3) a higher specific RhB removal which was attributed to the Ag-enhanced photocatalytic activity. The incorporation of Ag could enhance the overall photocatalytic activity of the membrane by acting as an electron sink at the Schottky barrier formed at the Ag-TiO<sub>2</sub> interface. It was found that all the treated solutions showed a final TOC concentration < 1 mg L<sup>-1</sup>, after 8 h, which was the detection limit of the equipment. This finding indicated > 88% TOC removal in the RhB solution (from the theoretical TOC concentration of 8.4 mg L<sup>-1</sup> for 25 μM solution).



**Figure 6.6** Specific RhB removal of Ag-TiO<sub>2</sub> photocatalytic membrane (the numerical values depict kinetic value based on initial RhB removal rate within 1<sup>st</sup> hour in mg m<sup>-2</sup> h<sup>-1</sup>).

Fouling control is an important property of any membrane process. The overall values of flux decline over the treatment duration of 480 min were listed in Table 6.3. The Ag-TiO<sub>2</sub> membrane suffered only a small fraction (up to 17 %) of flux decline over the duration of 480

min treatment of RhB. The higher initial decline of the flux could be contributed by the adsorption of RhB molecules onto the membrane. After which, the steady state flux was reached.

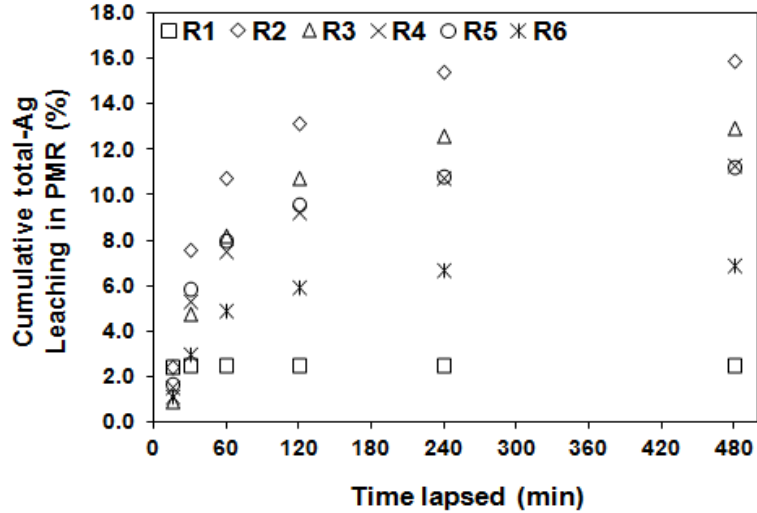
**Table 6.3** Performance of TiO<sub>2</sub> photocatalytic ceramic membrane in terms of its photocatalytic activity (PCA) and adsorptive-membrane retention (Ads-MR) after 8 h of operation and percentage of initial flux retained after 4 cycles of treatment

Types	Removal (mg m <sup>-2</sup> )			Removal (%)		Flux Decline (%)
	PCA	Ads-MR	Total	PCA	Ads-MR	
<b>R1</b>	2048 ± 52	331 ± 26	2379 ± 29	86.1	13.9	13.9
<b>R2</b>	2169 ± 35	351 ± 22	2520 ± 13	86.1	13.9	15.1
<b>R3</b>	1999 ± 56	407 ± 11	2406 ± 46	83.1	16.9	16.4
<b>R4</b>	2048 ± 71	558 ± 23	2606 ± 74	78.6	21.4	16.8
<b>R5</b>	2252 ± 30	486 ± 29	2738 ± 52	82.2	17.8	16.0
<b>R6</b>	2203 ± 52	577 ± 56	2780 ± 29	79.2	20.8	17.1
<b>Plu D</b>	2025 ± 24	329 ± 13	2354 ± 18	86.0	14.0	13.8

#### 6.3.4 Total Ag leaching of Ag-TiO<sub>2</sub> membranes

The usage of Ag nanoparticles as an anti-bacterial agent might release a significant amount of Ag into the treated water. Significant Ag<sup>+</sup> ions release would also have an adverse effect on the aqueous ecosystems and shorten the overall life-span of the Ag-TiO<sub>2</sub> membrane. The time-dependent Ag leaching profiles of the Ag-TiO<sub>2</sub> membranes are studied (Tables 6.4). Total Ag releases of R1 and R3 are small (2.0 and 1.5 µg L<sup>-1</sup> respectively) which could be attributed to their relatively small Ag content at the top-most layer of the membrane. Generally, the membranes with Ag incorporated in all their sub-layers showed a higher total Ag release. Membrane R4 released more Ag<sup>+</sup> than R2 (despite the same amount of Ag loading on their sub-layers) because of its tighter porous structure, thus more Ag

nanoparticles were concentrated near the surface of TiO<sub>2</sub> clusters. The highest Ag concentration leached out from the Ag-TiO<sub>2</sub> membrane (i.e. R6 of 27 µg L<sup>-1</sup> after 168 h of immersion) was still 4 times lower than the highest tolerable Ag concentration in drinking water of 100 µg L<sup>-1</sup> as prescribed by USEPA regulation and WHO guideline (USEPA 2009, WHO 2011). This showed that the Ag-TiO<sub>2</sub> membrane possessed a good chemical stability.



**Figure 6.7** Cumulative total-Ag leached from Ag-TiO<sub>2</sub> membrane operated in the PMR.

Total-Ag leaching experiments were also performed in the PMR. Most of the Ag (a maximum of 8 µg L<sup>-1</sup> for R6) was leached out from the membrane within the first 120 min of membrane operation (Table 6.4 and Fig. 6.7). It was evident that the additional amount of Ag leachate for the last 360 min of operation was marginal (about one-fifth of the amount released in the first 120 min) indicating the chemical stability of the membrane (Fig. 6.7). The release of Ag<sup>+</sup> ions was governed by the diffusion rate of both Ag<sup>+</sup> ions and water. At the early stage of the test, the Ag release was mainly contributed from the dissolution of surface Ag nanoparticles into water and the possibility of dislodgment of Ag nanoparticles from the membrane. After which, the rate of release was slower. The slower release of the Ag

nanoparticles located inside the TiO<sub>2</sub> matrix could be attributed to the slow diffusion rate inside the pores (Ma et al. 2011).

**Table 6.4** Time-dependent total-Ag leaching of Ag-TiO<sub>2</sub> membrane reported in (a) % of initial Ag loading and (b) in µg L<sup>-1</sup>

(a)							
Types	Ag loading (µg)	Cumulative time-dependent total-Ag leaching (%) in batch reactor			Cumulative total-Ag leaching (%) in PMR		
		24 h	96 h	168 h	30 min	120 min	480 min
<b>R1</b>	0.47 ± 0.03	3.30 ± 0.02	6.78 ± 0.09	12.79 ± 0.23	2.45 ± 0.02	2.46 ± 0.02	2.47 ± 0.03
<b>R2</b>	1.36 ± 0.22	2.27 ± 0.04	5.02 ± 0.08	7.29 ± 0.03	7.56 ± 0.13	13.16 ± 0.22	15.84 ± 0.26
<b>R3</b>	0.76 ± 0.01	2.46 ± 0.03	4.16 ± 0.09	5.74 ± 0.05	4.75 ± 0.08	10.73 ± 0.18	12.95 ± 0.24
<b>R4</b>	1.85 ± 0.28	12.37 ± 0.25	19.52 ± 0.18	26.59 ± 0.21	5.28 ± 0.04	9.21 ± 0.11	11.24 ± 0.15
<b>R5</b>	1.53 ± 0.16	3.64 ± 0.01	15.53 ± 0.20	24.53 ± 0.15	5.86 ± 0.09	9.54 ± 0.12	11.23 ± 0.17
<b>R6</b>	4.09 ± 0.61	6.31 ± 0.02	13.10 ± 0.27	19.82 ± 0.59	2.94 ± 0.04	5.88 ± 0.08	6.91 ± 0.11

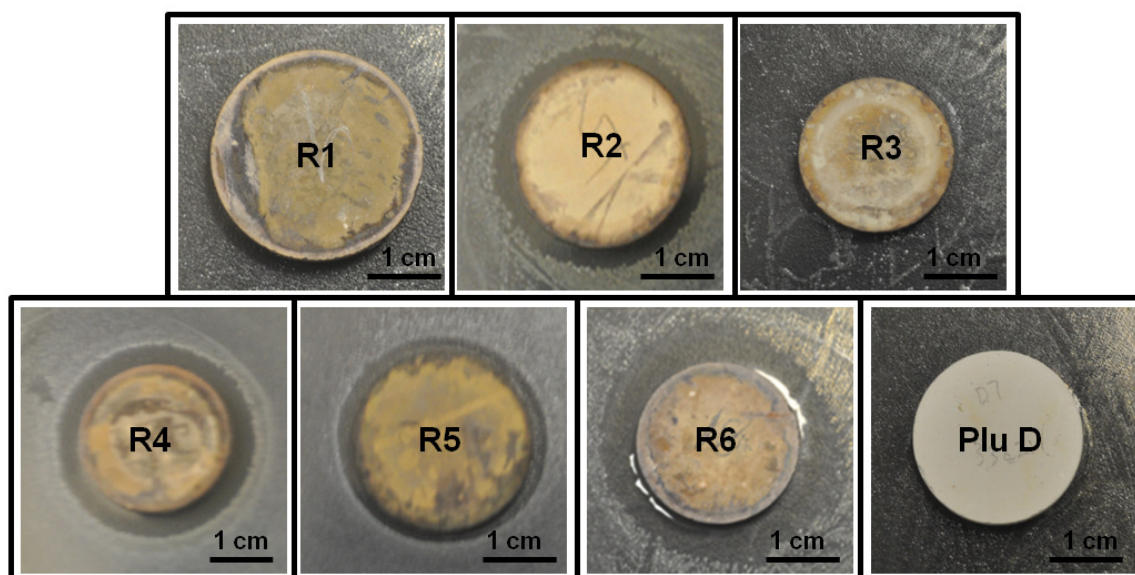
(b)							
Types	Cumulative time-dependent total-Ag leaching (µg L <sup>-1</sup> ) in batch reactor			Cumulative total-Ag leaching (µg L <sup>-1</sup> ) in PMR			
	24 h	96 h	168 h	30 min	120 min	480 min	
<b>R1</b>	0.52 ± 0.01	1.07 ± 0.01	2.03 ± 0.04	2.14 ± 0.02	3.84 ± 0.03	4.66 ± 0.05	
<b>R2</b>	1.03 ± 0.02	2.27 ± 0.04	3.30 ± 0.01	3.42 ± 0.06	5.95 ± 0.10	7.16 ± 0.12	
<b>R3</b>	0.62 ± 0.01	1.05 ± 0.02	1.45 ± 0.01	1.20 ± 0.02	2.71 ± 0.05	3.27 ± 0.06	
<b>R4</b>	7.62 ± 0.16	12.02 ± 0.11	16.37 ± 0.13	3.25 ± 0.03	5.67 ± 0.07	6.92 ± 0.10	
<b>R5</b>	1.86 ± 0.01	7.92 ± 0.10	12.52 ± 0.07	2.99 ± 0.04	4.87 ± 0.06	5.73 ± 0.08	
<b>R6</b>	8.61 ± 0.02	17.87 ± 0.37	27.04 ± 0.80	4.00 ± 0.05	8.02 ± 0.10	9.42 ± 0.15	

### 6.3.5 Anti-bacterial performance of Ag-TiO<sub>2</sub> membranes

#### 6.3.5.1 Diffusion inhibition zone test

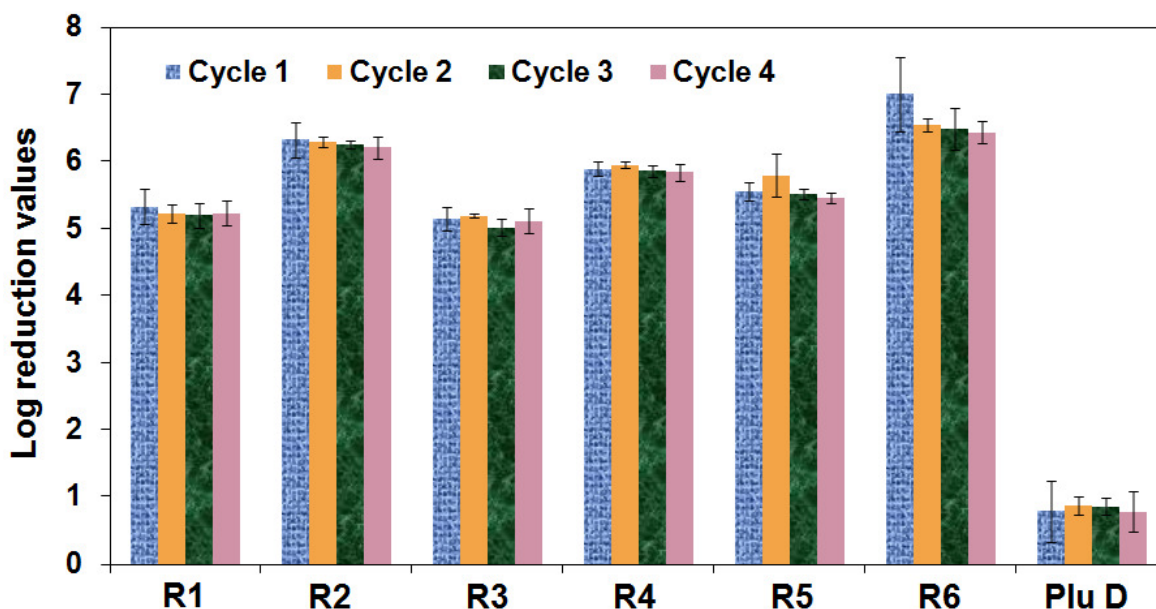
Diffusion inhibition zone of various Ag-TiO<sub>2</sub> membranes with different hierarchical architectures were performed according to a standard Kirby-Bauer approach (Bauer et al. 1966) and are presented in Fig. 6.8. Ag-free Plu D membrane did not show any apparent inhibition effect against the growth of *E. coli*. R1 and R3 membranes showed a small

inhibition zone due to its smaller Ag content while R5 membrane showed an observable inhibition zone (diameter of 27 mm) which highlights the significant of Ag content on the thin photoactive layer of the membrane. R2, R4 and R6 membranes which contained Ag in all of its 6 sub-layers, showed the most prominent inhibition effect with diameter of the inhibition zone measured to 36, 31, and 38 mm respectively. R2 membrane showed a larger inhibition zone as compared to R4 membrane which could be attributed to more  $\text{Ag}^+$  ions leaching due to its larger porous structure. R6 membrane showed the largest inhibition zone owing to its largest Ag content hence more  $\text{Ag}^+$  ions diffusion into the agar plate that restrained the bacteria growth. It was understood that diffused  $\text{Ag}^+$  ions possessed more effective anti-bacteria property as compared with Ag nanoparticles (Lv et al. 2009b)



**Figure 6.8** Diffusion inhibition zones of Ag-TiO<sub>2</sub> photocatalytic membrane against *E. coli* after 24 h incubation.

### 6.3.5.2 Anti-bacterial performance using batch reactor



**Figure 6.9** *E. coli* log reduction value of Ag-TiO<sub>2</sub> photocatalytic membrane showing its reusability over 4 cycles (duration of 8 h each cycle) of operation in a batch reactor. Error bars represent one standard deviation of at least three replicates of experimental runs.

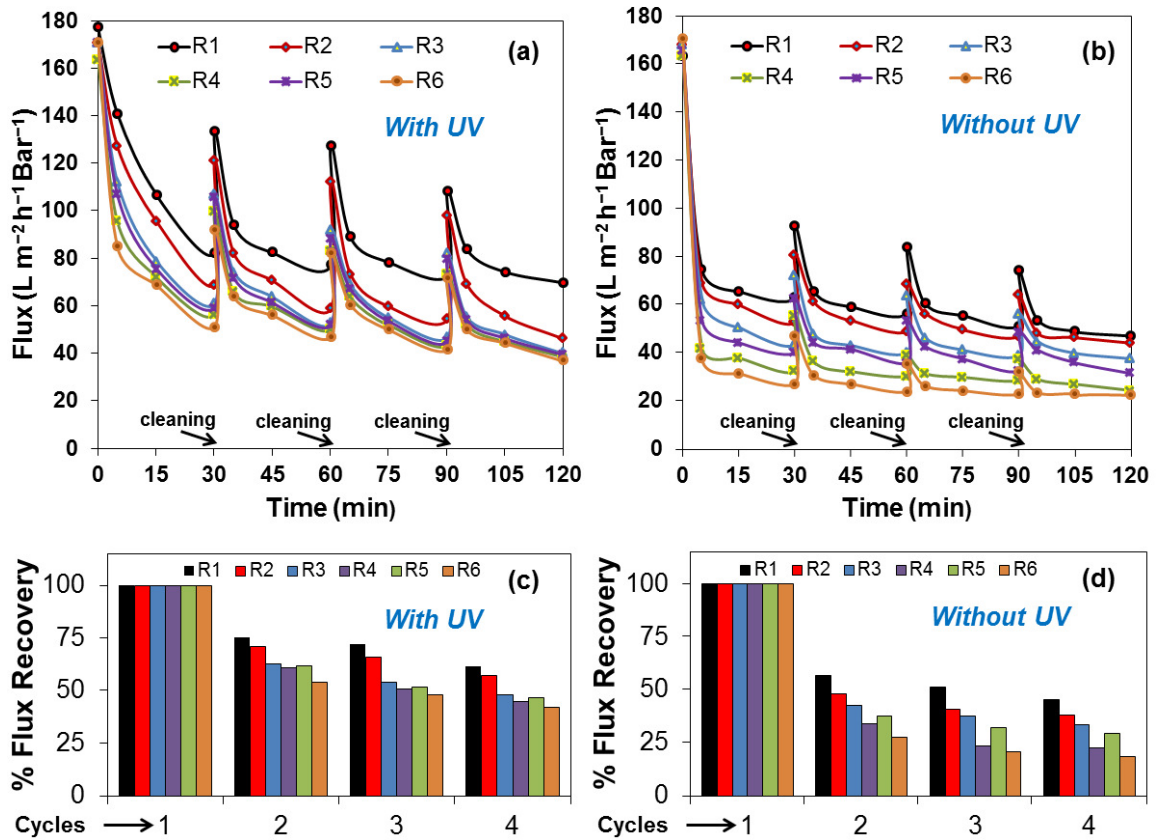
Fig. 6.9 shows log reduction values of *E. coli* suspension when subjected to the Ag-TiO<sub>2</sub> membrane at a batch reactor operating at dark under continuous stirring. The Ag-TiO<sub>2</sub> membranes were able to remove a minimum of 5-logs of *E. coli* from its suspension within 15 min contact time. This suggests that the Ag-TiO<sub>2</sub> membrane exhibited an excellent anti-bacterial activity even when operating in the dark. The overall reduction of *E. coli* was caused by the anti-bacterial activity of Ag. R1, R2, R3, R4, R5, and R6 membranes reduce the *E. coli* viable cells count up to 5.3, 6.3, 5.2, 6.0, 5.8, and 7.0 logs respectively. R2, R4, and R6 showed more *E. coli* removal efficiency due to a higher Ag loading on its sub-layers. This is consistent with earlier observation from the total Ag-leaching study. R1 and R2 showed a slightly higher *E. coli* removal efficiency than its R3 and R4 counterpart. This

could be attributed to their more porous structure that allowed more interaction between Ag species and bacteria cells. 1-log removal of *E. coli* suspension when treated with Plu D suggests that TiO<sub>2</sub>-anatase possesses, to some extent, a bactericidal activity (Kubacka et al. 2009). Repeated usages (up to 4 cycles) of the membrane showed a good consistency of *E. coli* removal efficiency. This suggests a reusability potential of the Ag-TiO<sub>2</sub> membrane.

### **6.3.5.3 Anti-bacterial performance using PMR**

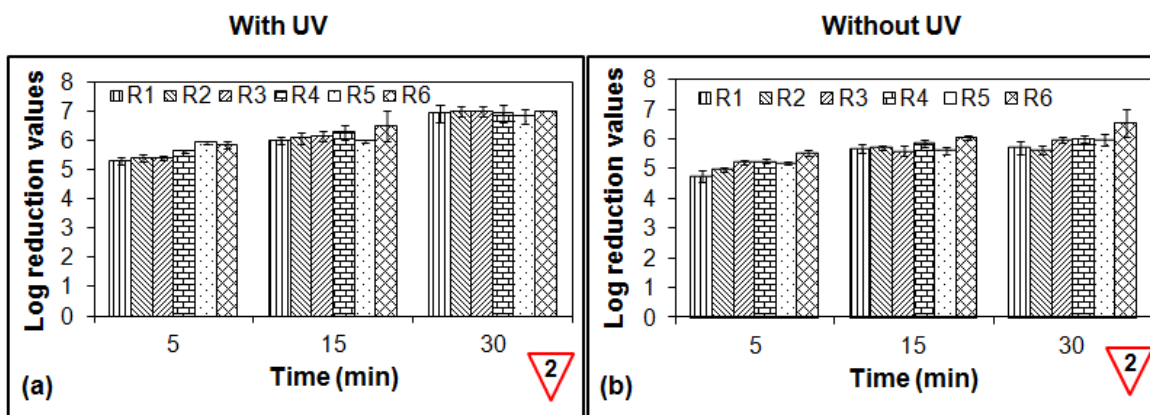
The anti-bacterial performances of the various membranes used in the PMR are illustrated in Figs. 6.10-6.13. Prior to any of the experiments, the PMR was flushed thoroughly with 0.9 wt% NaCl solution. After which, the feed was replaced with *E. coli* suspension. A control sampling was taken regularly at the sampling point 1 (Fig. 1) to ensure that the concentration of *E. coli* suspension entering the membrane cell was the same as the concentration at the feed tank. Upon entering the membrane cell, *E. coli* started to be deposited onto the surface of the membrane. This was evidenced from a declining permeate flux as the experiment progressed (Fig. 6.10a and b). The fouling was expected as the size of *E. coli* cell ( $\pm 1 \mu\text{m}$  length) was much larger than the pore size of the Ag-TiO<sub>2</sub> membrane (between 4–12 nm depending on the amount of P-123 and Ag loading).

The membrane fouling could be caused by the adhesion and accumulation of dead bacteria cells on the membrane surface (Yao et al. 2008). However, as the experiment progressed, the rate of declining flux was progressively reduced. The experiments that were carried out in the presence of UV irradiation exhibited a much smaller flux decline. After 30 min of operation, the feed was replaced by an equal-volume 0.9 wt% NaCl solution and the cross-flow cleaning valve was opened. This was a cross-flow cleaning step that helped to recover the permeate flux by dislodging any deposited dead-bacteria cells.



**Figure 6.10** Flux performance of Ag-TiO<sub>2</sub> photocatalytic membrane in the dead-end filtration mode of PMR with inter-cycle cleaning operating (a) with UV and (b) without UV. Percent flux recovery after each cleaning cycles when operating (c) with UV and (d) without UV.

The percentages of flux recovery after each cleaning cycle are shown in Fig. 6.10c and d. The membranes operated under UV irradiation showed higher flux recoveries. R1 and R2 (possessed more porous structure) exhibited the least flux decline. In general, the membranes with larger porosity exhibited lesser flux decline than their counterparts. From the decreasing rate of flux decline after each operation-cleaning cycle, it could be hypothesized that a steady-state sustainable flux would be achieved after a certain number of operation-cleaning cycles.

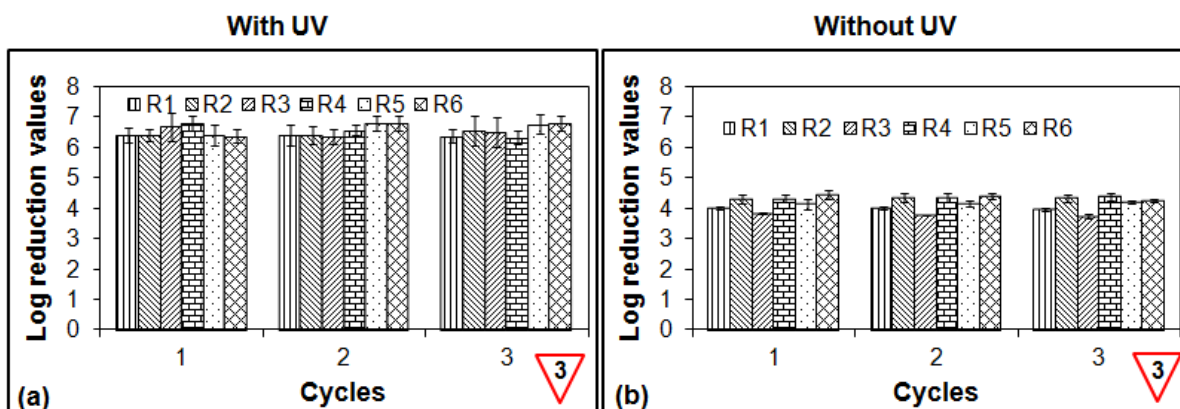


**Figure 6.11** *E. coli* log reduction values of Ag-TiO<sub>2</sub> photocatalytic membrane operating in a photocatalytic membrane reactor: at sampling point (2) when operating (a) with and (b) without UV. Error bars represent one standard deviation of at least three replicates of experimental runs.

The log reduction value of *E. coli* was evaluated during the PMR operation (aliquots taken from the sampling point 2, Fig. 6.11) and after each cleaning cycle (aliquots taken from the sampling point 3, Fig. 6.12). In the presence of UV irradiation ( $\lambda_{\max} = 365$  nm) alone, only  $1.9 \pm 0.2$  log of bacteria cells was killed. Sample aliquots taken from the sampling point 2 during operation should contain a negligible concentration of *E. coli* ( $< 0.002\%$  of the initial feed concentration) as most of the bacteria cells ( $>99.998\%$ ) would be retained or inactivated by the membrane. The membranes operating under UV irradiation generally showed a higher *E. coli* reduction values. Also, the membranes with higher amounts of Ag content showed a higher *E. coli* reduction values.

Sample aliquots (Fig. 6.12a and b) taken from sampling point 3 (after each cleaning cycle) showed a clearer trend. It can be observed that the membranes operating under UV irradiation showed a higher overall *E. coli* removal. This could be attributed to three synergistic processes that were taking place, i.e. Ag anti-bacteria activity, Ag-enhanced TiO<sub>2</sub> photocatalytic disinfection, and, to the lesser extent, direct UV disinfection. Reduction of

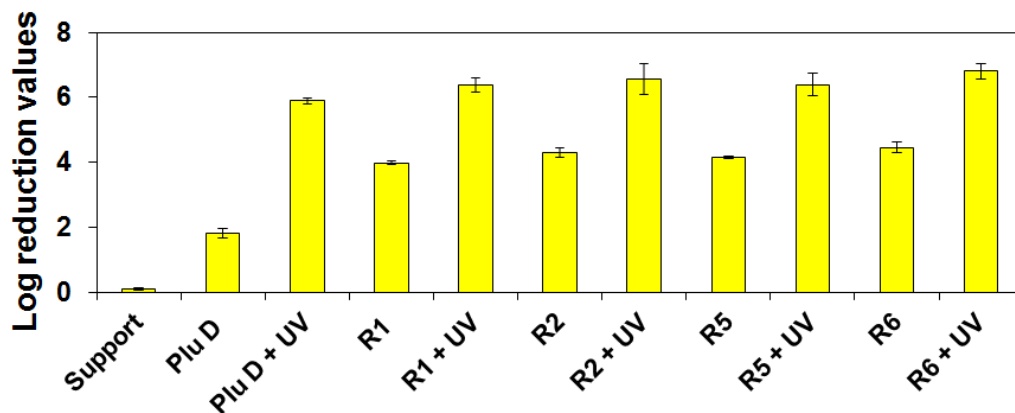
viable *E. coli* counts for experiments that were carried out in the dark could be ascribed to the inherent Ag anti-bacterial activity only.



**Figure 6.12** *E. coli* log reduction values of Ag-TiO<sub>2</sub> photocatalytic membrane operating in a photocatalytic membrane reactor: at sampling point (3) after each cross-flow cleaning cycles when operating (a) with and (b) without UV. Error bars represent one standard deviation of at least three replicates of experimental runs.

#### 6.3.5.4 Anti-bacterial mechanisms of Ag-TiO<sub>2</sub> membranes

In order elucidate the contribution of each anti-bacterial processes, selected results from the PMR experiment (taken at sampling point 3) are tabulated in Fig. 6.13. Alumina support disk show no anti-bacterial capability. Plu D membrane showed some degree of antibacterial capability of TiO<sub>2</sub>-anatase. When operating Plu D under UV irradiation, the synergistic effect of TiO<sub>2</sub> photocatalytic disinfection and direct UV disinfection could be observed (by almost 4-log increase in *E. coli* removal). Same effect was evidenced when different Ag-TiO<sub>2</sub> membrane operating under UV irradiation. Membrane with higher amount of Ag loading, showed higher *E. coli* reduction values (e.g. R2 > R1, R5 > R1, and R6 > R5). This could be attributed to additional process of Ag anti-bacterial activity as well as enhanced TiO<sub>2</sub> photocatalytic degradation.

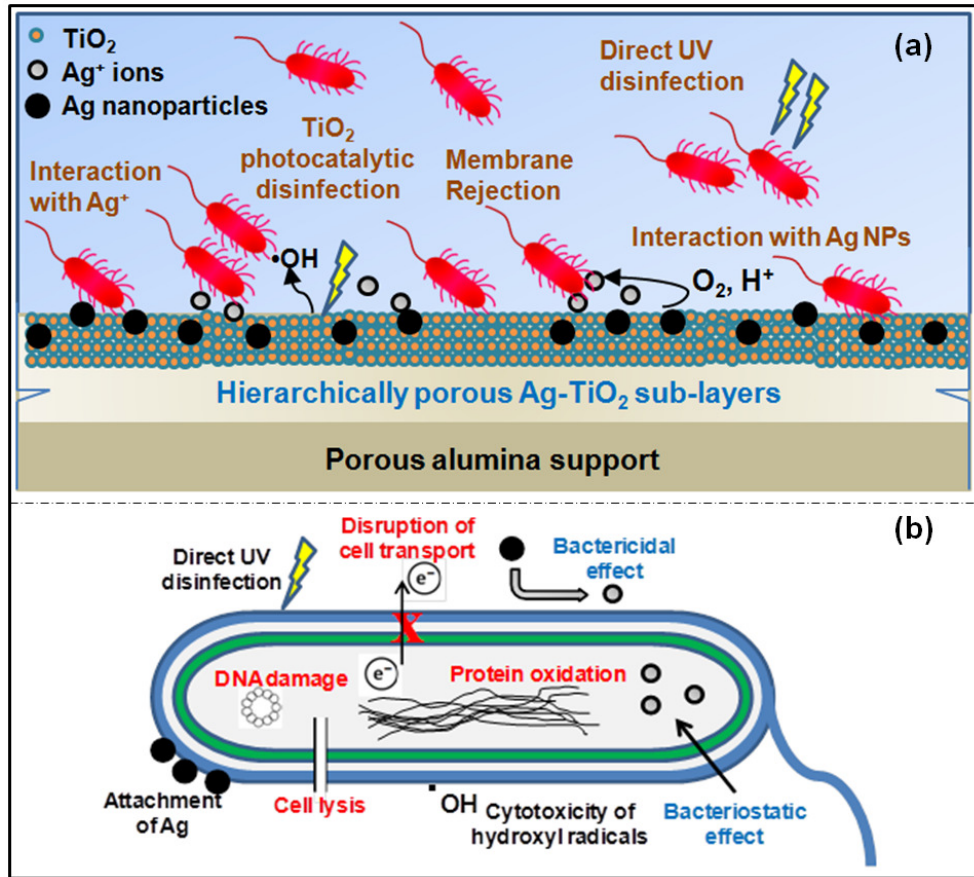


**Figure 6.13** Log reduction values of *E. coli* at sampling point 3 after cross-flow cleaning cycle for various membranes. Error bars represent one standard deviation of at least three replicates of experimental runs.

It is not an easy task to pin-point which process has a larger contribution on the overall anti-bacteria/anti-biofouling activity of the Ag-TiO<sub>2</sub> membrane. Some possible anti-bacteria mechanisms are illustrated in Fig. 6.14. They are: direct UV disinfection, membrane rejection, interaction of bacteria cells with Ag<sup>+</sup> ions, direct interaction with Ag nanoparticles, and TiO<sub>2</sub> photocatalytic disinfection.

The important processes could be explained as followed: Ag<sup>0</sup> tends to be lightly bonded to oxygen, which would readily oxidized to Ag<sup>+</sup>, interact with the disulfide or thiol (-S-H) groups enzyme or DNA of the bacteria, while removing H as water. This would cause the formation of R-S-S-R bond that would disrupt respiration and other metabolic processes, interrupt DNA replication, and causing the death of bacteria cells (bactericidal effect) (Feng et al. 2000, Russell and Hugo 1994, Siva Kumar et al. 2004). It was also reported that Ag<sup>+</sup> ions are able to change the permeability of the negatively charged-cell wall, causing cell lysis and the eventual death (Samuel and Guggenbichler 2004). Some surviving bacteria that are already contaminated with Ag<sup>+</sup> ions cannot grow into colonies because their growth signaling

pathway has been disturbed by penetrating  $\text{Ag}^+$  ions (bacteriostatic effect) (Lv et al. 2009b, Shrivastava et al. 2007).



**Figure 6.14** (a) Possible mechanisms of anti-bacterial action inside the photocatalytic membrane reactor: direct UV disinfection (when subjected to a high UV intensity), membrane rejection, interaction with  $\text{Ag}^+$  ions, interaction with Ag nanoparticles, and bactericidal action of  $\text{TiO}_2$  and (b) Summary of different actions of bacteria inactivation.

Ag nanoparticles could directly attached to the surface of bacteria cell membrane, destabilize the outer membrane, disrupt the plasma membrane potential and decrease the concentration of intracellular ATP (Choi et al. 2008, Lok et al. 2006, Sondi and Salopek-Sondi 2004).

Hydroxyl radicals are the cytotoxic agent produced at the surface of  $\text{TiO}_2$  photocatalyst that directly attacks the cytoplasmic membrane of the bacteria and resulting in the leakage of

the intracellular components. A Gram-negative bacterium such as *E. coli* is protected only by a thin peptidoglycan layer (a relatively open polymeric network of N-acetylmuramic and N-acetylglucosamine polysaccharide chains with peptide bridges). However, it is the outer membrane (consist of complex layer of lipids, lipopolysaccharides and proteins) that hinders the passage of hydroxyl radicals (Huang et al. 2000, Lu et al. 2003, Page et al. 2007).

Finally, the ability of bacteria to undergo repair after photocatalytic disinfection were investigated both in the dark and in the presence of UV irradiation. Bacteria cells could repair themselves either through dark repair or photo-reactivation (Rincón and Pulgarin 2004) after irradiation to light with wavelength of 300-500 nm (Kashimada et al. 1996). No bacterial growth could be detected after the bacterial repairing period for both tested solutions. This suggests that photocatalytic disinfection caused a permanent damage to the bacterial cells unless a provision of favorable conditions for bacteria repair were given (Dunlop et al. 2002).

## **6.4 Conclusions**

Ag-TiO<sub>2</sub> photocatalytic membranes have been fabricated using P-123 as the pore forming and structure-directing agent. The different membranes possessed their unique hierarchical architectures that were achieved by multilayer coating of Ag-TiO<sub>2</sub> of different porous structures. Ag incorporation enhanced the photocatalytic activity of TiO<sub>2</sub> by hindering the recombination of photo-generated electrons and holes. Furthermore, the incorporation of Ag imparted anti-bacterial functionality to the membranes. The Ag-TiO<sub>2</sub> membrane possessed a multi-functionality of membrane retention, Ag-enhanced TiO<sub>2</sub> photocatalytic activity and multiple anti-bacterial actions. The reusability potential of the Ag-TiO<sub>2</sub> membranes has been demonstrated both in the batch and flow-through PMR which would reduce the overall operating cost of the treatment system.

## CHAPTER 7 CONCLUSIONS AND RECOMMENDATIONS

### 7.1 Conclusions

Different types of TiO<sub>2</sub> layers with controllable porous structure were prepared by acid-catalyzed sol-gel method employing P-123 as the SDA. TiO<sub>2</sub> sols were dip-coated on a macroporous alumina ceramic membrane support. Layer-by-layer coatings were performed to obtain a hybrid TiO<sub>2</sub> photocatalytic ceramic membrane with a hierarchical porous architecture. Extensive characterization of the resulting membrane has been carried out. The membrane displayed a photo-induced super-hydrophilicity. Plu D membrane with 3-2-1 layers configuration was found to display an optimum membrane and photocatalytic degradation of RhB performances.

Four types of SDAs were employed to fabricate a hierarchically porous TiO<sub>2</sub> photocatalytic membrane. TiO<sub>2</sub> layers prepared using different SDAs could be used in the composite membrane fabrication without any compatibility issue. This allow flexibility of constructing a membrane that exhibit favorable operating parameters such as high permeability, good membrane separation, good photocatalytic degradation capability, or any combination of the parameters.

Ag-decorated hierarchically porous TiO<sub>2</sub> photocatalytic membrane has been fabricated. The amount of Ag incorporated, together with the amount of SDA (P-123), could be used to control the porosity structure of the resulting Ag-TiO<sub>2</sub> layer. Membranes with different configurations (different porosities and location of Ag doping) were fabricated. The incorporation of Ag had caused enhancement in the photocatalytic activity of TiO<sub>2</sub> and introduced an additional anti-bacterial functionality. The anti-bacterial functionality of the Ag-TiO<sub>2</sub> membrane was tested against *E. coli*, a common water-borne pathogen. Multiple anti-bacterial actions have also been postulated.

The integration of TiO<sub>2</sub> photocatalysis, membrane separation, and Ag-induced anti-bacterial actions has offered a multi-functional one-stop treatment system with simpler configuration and smaller overall footprint. The hybrid membrane displayed a great potential to be used in water and wastewater treatment and many other potential environmentally important applications.

## 7.2 Recommendations for future research

To further enhance and extend the potential application of the hierarchically porous TiO<sub>2</sub> photocatalytic ceramic membrane for wastewater treatment and water reclamation, several recommendations for the future research are proposed:

1. Hierarchically porous TiO<sub>2</sub> photocatalytic membrane
  - A more versatile techniques can be developed for the preparation and coating of the TiO<sub>2</sub> sol onto the ceramic disk support. Different ceramic supports (e.g. supports that made of macroporous ZnO or TiO<sub>2</sub>) can be considered to enhance the functionality of the composite membrane.
  - A more thorough investigation of TiO<sub>2</sub> photocatalytic membrane can be carried out to fully understand the microstructure of the photocatalytic layer
  - An intermediate molecular sieve layer can be introduced to enhance the molecular size-selectivity and permeability of the composite membranes.
  - To prepare a hybrid membrane with top layer having a smaller pore sizes (in the NF range or down to ~1 nm) to investigate the efficacy of the hybrid membrane in treating small recalcitrant molecules.
  - Some analytical techniques could be employed to investigate the generation of reactive oxygen species, to fully elucidate the mechanism of photocatalytic

degradation reaction (i.e. electron paramagnetic resonance (EPR), electron spin resonance (ESR), cyclic voltammetry, etc).

- The possibility of up-scaling the operation of TiO<sub>2</sub> photocatalytic membrane can be considered. Several ideas for the up-scaling include fabrication of a larger composite membrane, simultaneous operation of the parallel PMRs, etc.

## 2. Metal/non-metal decorated TiO<sub>2</sub> photocatalytic membrane

- The possibility of exploiting surface plasmon resonance induced by Ag-TiO<sub>2</sub> can be investigated for operation of Ag-TiO<sub>2</sub> membrane using a visible light as the irradiation source.
- Ag<sup>+</sup> leaching in a continuous flow through setup can be monitored for a longer period to study the temporal Ag<sup>+</sup> leaching from the membrane.
- The possibility of incorporation of other metal (e.g. Er, Si, Zn, Zr, etc) or non-metal (e.g. C, N, S, etc) dopants or co-dopants into the TiO<sub>2</sub> matrix can be investigated.

## 3. Hybrid photocatalytic membrane reactor

- The configuration of the PMR can be adjusted to provide insight of the effect of various operation parameters (such as different irradiation sources, different operation modes, different flow rate, etc) to the efficiency of the treatment process.
- The possibility of introducing a more versatile irradiation source can be considered (e.g. through the use of fiber optics) to overcome the challenge of PMR reactor design.
- The setup and control of the automated PMR can be enhanced to allow continuous operation. The safety feature can be enhanced to minimize

interruption of the continuous operation. Round-the-clock operation of the PMR can provide interesting insight onto the real-scale operation of the TiO<sub>2</sub> photocatalytic membrane.

- The removal efficiency of TiO<sub>2</sub> photocatalytic membrane can be evaluated against a wider range of pollutants as well as possibility of treating a real wastewater. Different parameters such as pH of the solution and the effect of various aqueous matrix species can be studied.
- Various pre-treatments can be considered to be operated in tandem with PMR system to allow a wider range of application for wastewater treatment.
- Various membrane operation parameters such as critical flux determination and the effect of backwashing can be investigated to enhance the understanding of the operation of TiO<sub>2</sub> photocatalytic membrane in the PMR.
- The economy of the treatment process (including fixed and operating cost) can be evaluated for comparisons with other similar treatment system.

#### 4. Anti-bacterial action of Ag-TiO<sub>2</sub> membrane

- The effect of pH and inorganic matrix species on the anti-bacterial action against *E. coli* can be investigated.
- Various operating parameters such as different constant fluxes, irradiation sources, operation modes, etc can be investigated to understand the extent of the anti-bacterial action of Ag-TiO<sub>2</sub> membrane.
- The efficacy of the anti-bacteria property of the membrane can be tested against other type of bacteria including gram positive bacteria (e.g. *S. aureus*).

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