

# Improved Light Attenuation Method for 2D Data Acquisition of Sediment Depths

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## Abstract

An improved light attenuation method (LAM2D – Light Attenuation Method for Two-Dimensional Data Acquisition) to quantify two-dimensional (2D) sediment depths with higher accuracy is developed in the present study. The working principle is to relate attenuated light intensities with depths of the sediment layer. Traditionally, calibration has been performed with the scraper method with either multiple constant depth sediment profiles or a slope with incremental depth profile. This method works well for coarse sediment, but is shown to be inaccurate for fine sediment with shallow sediment depth in the near-zero limit regime. In the present study, a new method is established for the calibration of shallow sediment depth by utilizing the correlation of particle plume deposition profiles. The practical application of

26 LAM2D to determine sediment deposition profiles from a laboratory simulation of barged  
27 sediment disposal was demonstrated with both approaches. The errors in the overall  
28 determination of sediment mass were found to be significantly reduced with the current  
29 approach.

30

## 31 **Introduction**

32 In the laboratory study of sediment transport, environmental hydraulics and coastal  
33 engineering, the investigation of sediment deposition and bathymetry changes require the  
34 accurate measurements of sediment distribution over the affected area. Previous measurement  
35 techniques to achieve this objective had been summarized in details by Munro and Dalziel  
36 (2005). They included the ultrasonic depth profiler and stereo-photography which have limited  
37 spatial resolution, and also the laser three-dimensional (3D) scanner which has high accuracy  
38 but is expensive with long acquisition time (Lague et al. 2003). Alternatively, Rooij et al.  
39 (1999) employed an array of electrodes on the bottom of the tank to determine the sediment  
40 depth based on the resistance induced through the sediment layer. This method enables real  
41 time measurements, but is limited by the range of sediment depths as the voltage signal quickly  
42 saturates in a deep sediment layer. In addition, the measurement extent is restricted by the  
43 coverage of the electrodes. Munro et al. (2004) developed a novel technique by comparing the  
44 reference image (image of undisturbed sediment layer) with the new image after the  
45 redistribution of sediment particles. Through a pattern-matching algorithm, high-resolution  
46 particle redistribution measurements were obtained. However, this technique was found to be  
47 impractical in terms of real time measurements. Subsequently, Munro and Dalziel (2005)  
48 proposed instead a light attenuation method (LAM) to resolve the temporal displacement of  
49 particles, which shall be reviewed in details in the following.

50 Light attenuation methods have been successfully applied to a wide range of studies  
51 involving single-phase flows. Holford and Dalziel (1996) used this method for the visualization  
52 and quantification of baroclinic instability of a two-layer rotating fluid system. Cenedese and  
53 Dalziel (1998) and Kikkert (2006) applied LAM to measure the depth-averaged concentration  
54 of a single-phase buoyant convective flow. Besides single-phase flows, LAM had also been  
55 used to investigate two-phase flows (i.e. air-water, solid-water flows), e.g. measuring the void  
56 fraction of micro bubbles (Leppinen and Dalziel 2001), gravity currents (Yuan et al. 2011), and  
57 the particle displacement or deposition in aqueous environments (Munro and Dalziel 2005;  
58 Sutherland and Dalziel 2014).

59 A potential additional application of LAM includes the measurement of oil spill  
60 thickness. The thickness of oil slicks can range from 0.1  $\mu\text{m}$  to 10 mm (Fingas and Brown  
61 2014). Several techniques have been employed by using acoustic wave, infrared, laser, radar,  
62 light (reflection or refraction) and visual inspection. The quantification of oil spreading  
63 thickness from the attenuation of backlighting is worth exploring, but the preparation of  
64 calibration samples is a challenge. The technique in LAM2D can be applied to generate the  
65 desired and accurate oil thicknesses for calibration. Another application for laboratory study is  
66 to determine the concentration of suspended sediments (e.g., in a sediment thermal or sediment  
67 clump). The calibration curve can be obtained by using a particle plume (or jet) with known  
68 concentration distribution (Azimi et al. 2011), and measuring the attenuated light intensity  
69 across the plume (or jet). The existing calibration method used a container filled with sediment-  
70 water mixture, and recorded the attenuated intensity (Wu et al. 2014). This process was  
71 repeated by changing the concentration of sediment in the mixture until a curve was obtained.  
72 The limitations of the existing method are that it is time consuming and the container must  
73 have the same width as the model tank.

74 In terms of measuring sediment depths, the principle of LAM involves the attenuation of  
75 light intensity transmitted through the sediment layer, and the sediment depth is then  
76 determined based on the attenuated intensity. In this case, the two most important parameters  
77 are the reference ( $I_{ref}$ ) and attenuated ( $I$ ) intensities without and with the presence of the  
78 sediment layer, respectively (Fig. 1). Upon transmitting through the sediment layer, the  
79 incident light is absorbed and reflected/refracted. The transmission ratio can be calculated as  
80 the ratio of attenuated intensity to the incident intensity. Nine ratios between 0 and 1 can be  
81 identified to account for the absorption (i.e.  $C_a$ ,  $C_w$ ,  $C_g$ ,  $C_p$ ) and reflection/refraction losses (i.e.  
82  $C_{a-g}$ ,  $C_{g-w}$ ,  $C_{w-a}$ ,  $C_{g-p}$ ,  $C_{p-w}$ ). The subscripts  $a$ ,  $g$ ,  $w$  and  $p$  represent the media of air, glass, water  
83 and particles, respectively. The interfaces between the media are noted with hyphen (-). Thus,  
84  $I_{ref}$  can be expressed in the following equation (Kikkert 2006):

$$I_{ref} = C_a \times C_w \times C_g \times C_{a-g} \times C_{g-w} \times C_{w-a} \times I_{source} \quad (1)$$

85 where  $I_{source}$  is the source intensity, while  $I$  can be represented as

$$I = C_a \times C_w \times C_g \times C_{a-g} \times C_{g-w} \times C_{w-a} \times C_p \times C_{g-p} \times C_{p-w} \times I_{source} \quad (2)$$

86 Hence,

$$I/I_{ref} = C_p \times C_{g-p} \times C_{p-w} \quad (3)$$

87 Thus, the ratio of attenuated to reference intensity is dependent on the characteristics of the  
88 particles (i.e.  $h_s$  and  $d_{50}$ , where  $h_s$  is the sediment depth and  $d_{50}$  is the median particle size).  
89 Equation (3) can be formulated as

$$I/I_{ref} = f(h_s, d_{50}) \quad (4)$$

90 with each particle size having its own unique calibration curve, and the same type of particle  
91 shall be used for both the calibration and actual tests. It should be noted that the formulation of  
92 Equations (1) to (4) might vary depending on the experimental apparatus and the features of  
93 the target to be measured.

94

## 95 **Previous Calibration**

96 Calibration is required to establish the functional form of Equation (4) (i.e. calibration curve).

97 Munro and Dalziel (2005) used sediment particles with  $d_{50} = 0.25$  mm, and prepared calibration

98 profiles by scraping the sediment to a constant depth or a linearly slope depth and measuring

99 the attenuated intensity,  $I$ , of the profiles. The scraping method worked adequately for sediment

100 depth  $h_s > 2$  mm or  $h_s/d_{50} > 8$  if  $d_{50} = 0.25$  mm. By plotting the normalized attenuated intensity,

101  $I/I_{ref}$  with the sediment depth,  $h_s/d_{50}$ , they observed an exponential decay when  $h_s/d_{50} > 18$  as

102 expected from Beer-Lambert's law, and called this region the self-similar regime. An

103 exponential fit of the data was performed in this regime as

$$\frac{I}{I_s} = \exp \left\{ b \left( \frac{h_s - h_c}{d_{50}} \right) \right\}, h_s > h_c \quad (5)$$

104 where  $I_s$  is the intensity at  $h_s = h_c$ , where  $h_c$  is the critical  $h_s$  determined to be  $18d_{50}$ , and  $\beta$  is the

105 empirical coefficient. The regime with  $h_s/d_{50} < 18$  was termed the near-zero limit regime, and

106 the attenuation did not follow Beer-Lambert's law. In this regime, they performed a least square

107 fit with the following equation chosen for empirical convenience:

$$\frac{I}{I_{ref}} = \exp \left\{ a \left( \frac{h_s}{d_{50}} \right)^g \right\} \quad (6)$$

108 where  $\alpha$  and  $\gamma$  are the empirical coefficients that fitted with all the data (including the data in

109 self-similar regime) but constrained to  $I/I_{ref} = 1$  at  $h_s/d_{50} = 0$  and  $I/I_{ref} \rightarrow 0$  when  $h_s/d_{50} \rightarrow \infty$ .

110 Overall, the calibration profiles prepared by Munro and Dalziel (2005) were appropriate for

111 coarse sediments (i.e. large  $d_{50}$ ) as a wide range of  $h_s/d_{50}$  (from near-zero limit to self-similar

112 regimes) could be covered.

113 Our focus on the further development of the LAM method in this study stemmed from our

114 ongoing interest related to the deposition of sediment clouds occurring during open water

115 barged sediment disposal (Er et al. 2016). Typically, the sediment size used in our laboratory

116 experiments was approximately 0.12 mm (fine to very fine sand) as determined from Froude  
117 scaling of field grain sizes (Wang et al. 2015), whereby a small value of  $h_s$  ( $< 2$  mm) would be  
118 expected based on preliminary experimental observations. Hence, although the range of  $h_s/d_{50}$   
119 might be similar to that in Munro's study (from near-zero limit to self-similar regimes), the  
120 values of  $h_s$  that needed to be determined were much shallower (since finer  $d_{50}$  was used) and  
121 could not be suitably prepared using the scraper method.

122 In the present study, an improved light attenuation method (LAM2D) is established, which  
123 uses different techniques to prepare the calibration curves. For deeper  $h_s$  ( $h_s > 2$  mm), the  
124 traditional scraping method was used. For shallower  $h_s$  ( $h_s < 2$  mm), however, an innovative  
125 technique using the deposition profiles produced by a particle plume which had small and  
126 measurable  $h_s$  was used instead. The calibration curves in the two regimes were established  
127 solely with data collected in the respective regime. This improved technique would benefit  
128 laboratory experiments that involve shallow sediment depth or those in which the change in  
129 sediment depth between pre- and post-tests is small. In the following, the experimental setup,  
130 particularly the novel calibration technique developed to calibrate the shallow  $h_s$ , is first  
131 presented. This is followed by the application of LAM2D to the measurement of deposition  
132 profiles from barged sediment disposal, and examination of the improvement over previous  
133 approach.

134

## 135 **Experimental Setup**

136 In the present study, the experiments were conducted in a 2 m (long)  $\times$  0.9 m (high)  $\times$  0.85 m  
137 (wide) water tank. The bottom of the tank was constructed with transparent glass to facilitate  
138 backlighting. Fresh water was used as the ambient fluid with water depth,  $h = 10$  cm. Uniform-  
139 size particles (Ballotini Impact beads, Potters Industries, Inc.) with a density,  $\rho_s$  of 2.5 g/cm<sup>3</sup>  
140 and size,  $d_{50}$  of 0.12 mm were used as the sediment particles for most of the experiments. The

141 particle size ranged from 0.09 to 0.15 mm with the size distribution being determined by Chow  
142 (2004) using sieve analysis.

143

## 144 ***Light Attenuation System***

### 145 ***Light Panel***

146 Fourteen 1.5 m (~5 ft.) long T8 fluorescent tubes were arranged equidistantly covering a width  
147 of 0.85 m in an aluminum rectangular box. The panel was placed horizontally under the glass  
148 tank facing upward as shown in Fig. 1. Several light sources were considered during the design  
149 stage, and fluorescent tubes were finally chosen because the light is emitted in a radial manner  
150 as compared to light-emitting diode (LED) light which is directional, and it has lesser variation  
151 with respect to intensity than halogen and overhead projector (OHP) lights (Kikkert 2006). The  
152 generation of a uniform light source over the measurement domain was a key issue in the  
153 current setup. To achieve this condition, the box cover was fabricated with light diffuser  
154 material (acrylic diffusion sheet). By increasing the panel depth (the distance between tubes  
155 and diffusion sheet), the uniformity of the light source could be greatly enhanced. In addition,  
156 the inner frame of the box was painted with highly reflective paint to promote reflections and  
157 improve the uniformity of the light at the edges of the box.

158 Before the experiments, the light panel was tested for light uniformity as well as  
159 consistency over short (i.e. within an hour) and intermediate (i.e. within weeks) periods of time.  
160 The results showed that the light panel was able to produce a uniform light source with a low  
161 coefficient of variance,  $CV \approx 1.6\%$  over an areal domain of  $1.0\text{ m} \times 0.5\text{ m}$ , which was sufficient  
162 to determine the deposition profiles from barged sediment disposal in the present experiments.  
163 Due to the temperature dependence of the fluorescent tube, the light intensity was expected to  
164 change over time as the temperature increased with prolonged test duration. The variation of  
165 intensity over time was recorded and observed to be stable between 20 to 40 minutes after the

166 light panel was switched on. Note that, the users should examine their light panel beforehand  
167 to reduce the experimental uncertainty induced by the variation of background light intensity.

### 168 **Camera**

169 A Nikon D700 DSLR (Digital Single-Lens Reflex) camera with a color CMOS  
170 (complementary metal-oxide semiconductor) sensor, equipped with a zoom lens (AF-S Zoom-  
171 Nikkor 24-70mm f/2.8G ED) was employed in the setup. The camera was mounted on top of  
172 the water tank, facing vertically downward toward the light panel. The distance between the  
173 camera and the measurement domain (sediment profile) was adjusted to achieve a balance  
174 between the needs to reduce the barrel distortion (i.e. increase in the distance between camera  
175 and target) and to retain a good resolution (i.e. decrease in the distance between camera and  
176 target). Finally, it was determined that the optimal distance was for the camera to be placed 1  
177 m above the bottom of the tank. Each pixel in the captured images corresponded to an area of  
178  $0.34 \text{ mm} \times 0.34 \text{ mm}$ .

179 Previous studies typically used a CCD (charge-coupled device) camera with a global  
180 shutter for the image capturing. Comparatively a CMOS camera usually operates with a rolling  
181 shutter (Konz et al. 2009; Njifenju et al. 2013). Due to the functional principle of the rolling  
182 shutter, the issue of flicker intensity was expected (Yoo et al. 2014) and the flickering was also  
183 observed in the current setup. To mitigate this issue, the camera exposure time,  $t_c$  was increased  
184 to average over the flickering light bands. With the current light panel,  $t_c > 1/40$  was found to  
185 be sufficient. Besides the exposure time, other parameters such as the  $f$ -stop ( $f/n$ ), ISO  
186 sensitivity and white balance were adjusted to achieve  $I_{ref}$  in a range of 240 ~ 250 (8 bits per  
187 pixel, giving integer intensity levels of  $0 \leq I \leq 255$ ). The selection criteria for each parameter  
188 are listed in Table 1. The final set of parameters chosen was:  $t_c = 1/30$ , ISO = 400 and  $f/n = f/22$   
189 with 26 mm field of view. The same set of parameters and format of images should be used  
190 during both the calibration and actual tests.

191 With the color sensor, three-color signals (red, green and blue) were recorded and analyzed.  
192 From the results, the blue signal attenuated the most and hence yield the best intensity  
193 resolution for the calibration curves. In the subsequent analysis, the intensities ( $I_{b\ ref}$  for the  
194 reference intensity and  $I_b$  for the attenuated intensity of the blue signal) were reported and  
195 analyzed.

196

### 197 ***Calibration Experiments***

198 The calibration approach established in the new method required two different calibration  
199 experiments, one for the deep and one for the shallow  $h_s$ , with 2 mm being the critical  
200 changeover value. For deep  $h_s$  ( $h_s > 2$  mm), the traditional scraping technique was used with  
201 multiple constant sediment depths. As our water tank was large, scraping the sediments over  
202 the entire bottom was impractical. A set of rings (termed calibration rings) with constant height  
203 (2 mm) was used instead, and the sediment was scraped within the rings. The ring height was  
204 subsequently increased to 4 and 6 mm by stacking up two or three rings, respectively. Another  
205 technique discussed in the literature was to scrap the sediments along a constant slope was also  
206 attempted. However, we found that the lateral sediment profiles were uneven with this  
207 technique when approaching small  $h_s$ . Moreover, the profiles near this region were highly  
208 sensitive to the disturbance.

209 For shallow  $h_s$  ( $h_s < 2$  mm), the correlation of particle plume deposition profiles from two  
210 test types was implemented instead. The two test types were: (i) the depth distribution profile  
211 ( $h_s$  vs.  $r_m$ , where  $r_m$  is the radius measured from the center of the profile) obtained from manual  
212 collection experiments (Test MC); and (ii) the attenuated intensity profile ( $I$  vs.  $r_m$ ) measured  
213 from the light attenuation experiments (Test LA). In Test MC, the collection method described  
214 by Gensheimer et al. (2012) to quantify the deposition of sediment clouds released in ambient  
215 currents was applied; the procedure will be discussed in more detail in the next section. In each

216 case, the deposition profiles were generated by releasing a fixed amount of particles from a  
217 funnel with a round opening. After the release from the opening, the gravity-driven particle  
218 plume descended through the water column and expanded laterally due to entrainment. Upon  
219 impact on the bottom, the particle plume spread horizontally as a gravity current before  
220 depositing. The dynamics of descent and deposition of the particle plumes were similar to that  
221 of the sediment clouds from barge disposal and hence gave an additional motivation for this  
222 calibration in our study.

223 Note that the same sediment profile could not be used for the two test types (i.e. Tests MC  
224 and LA). This was because Test MC required the grids to be printed on the platform/tank to  
225 guide the quantification process, while Test LA required the sediment to be deposited on a tank  
226 clear from marking for better illumination and measurement. Two important criteria were  
227 needed for the generated profiles for calibration: (i) consistent and high repeatability, and (ii)  
228 axisymmetry, so that the depth distribution could be presented as an azimuthal mean depth  
229 profile for analysis to reduce the local variation. Finally, the calibration curve was determined  
230 by correlating the results from these two test types.

231 Two calibration tests with a total 10 replicates were conducted by adopting the same release  
232 conditions. Table 2 summarizes the test conditions. In Test MC, the sediments were manually  
233 collected, dried and weighted to determine the depth distribution profile. On the other hand,  
234 Test LA measured the attenuated intensity profiles with the light panel. In the following  
235 sections, the apparatus and test conditions of the particle plume deposition experiments will be  
236 discussed in detail.

237

### 238 ***Particle Plume Experiments***

239 The particle plumes were generated by continuously releasing a mass of 10 g of sediment from  
240 a funnel with an opening radius of 5 mm. The sediment deposited on a platform with circular

241 grids printed, as shown in Fig. 2. Each replicate included the cumulative of five 10 g releases  
 242 to increase the volume of deposited sediment and hence minimize the local variation. In a  
 243 preliminary study, several alternative release mechanisms were considered, but they were all  
 244 found to be inadequate. For example, the quasi-instantaneous release of the same mass (i.e. 10  
 245 g) of sediment using a cylindrical tube with bigger opening (9 mm radius) that was sealed with  
 246 a layer of latex membrane (Zhao et al. 2014) produced highly inconsistent deposition profiles,  
 247 possible due to the formation of sediment clumps.

248 The 10 cm water depth was measured from the platform to the water surface. After five  
 249 releases, the water was slowly drained out from the tank to keep the deposition profiles  
 250 undisturbed. The sediment layer was then left over night until the excess water was evaporated  
 251 before removing it from the glass tank. Subsequently, the sediment deposited within the same  
 252 circular grid interval was collected with a brush, dried in an oven for two hours at 130 °C and  
 253 weighed. The mass distribution ( $m_s$  vs.  $r_m$ , where  $m_s$  is the mass of sediment) was converted to  
 254 depth distribution ( $h_s$  vs.  $r_m$ ) using the following equation:

$$h_{si} = \frac{V_{si}}{A_i} \text{ with } V_{si} = \frac{m_{si}}{\rho_s(1-n)} \quad (7)$$

255 where the subscript  $i$  represents the  $i$ -th ring from the center of the circular grid (release point),  
 256  $V_{si}$  is the volume of sediment,  $A_i$  is the area of ring, and  $n$  is the void ratio, which was assumed  
 257 to be a constant  $n = 0.44$  based on our previous study (Zhao et al. 2012).

258 In Test LA, before releasing the sediment, the reference intensity,  $I_{ref}$  was measured for  
 259 each replicate to check for consistency and then used for the normalization of  $I$ . Afterward,  
 260 particle plumes with the same release conditions as Test MC were released and deposited  
 261 directly on the bottom of the glass tank (Fig. 3). After five releases, the attenuated intensity  
 262 profile using the light panel,  $I$  vs.  $r_m$ , was determined.

263

## 264 **Results**

265 In this section, the sediment depth distribution and attenuated intensity profiles of the  
266 deposition of particle plumes are discussed. The comparative results are then used to establish  
267 the calibration curves for both regimes. Improvements of current approach over the previous  
268 approach (using scraper method only) are also shown.

269

### 270 ***Particle Plume Deposition Profiles***

271 The radial distributions of the mean depth profiles from Test MC are plotted in Fig. 4, with  $r_m$   
272 = 0 being the center of the funnel. Only three profiles are presented for brevity. When the  
273 experiment was initiated, the sediment particles were observed to descend continuously from  
274 the opening with a ‘thermal-like’ front head. The particle cloud had a typical tadpole shape,  
275 similar to the buoyant starting plume observed by Ai et al. (2006). Upon impact with the  
276 bottom, the momentum of the ‘thermal-like’ front head and the density difference (buoyancy)  
277 drove the collapsed plume to propagate radially as gravity current. The sediment particles then  
278 gradually settled out from the gravity current as it propagated away from the release point.  
279 With the current test conditions, ~ 35 % of the particle deposited in the area within  $r_m < 4$  cm  
280 and ~ 60 % deposited outside the ring area with  $r_m > 4$  cm. The remaining particle (< 5 %)   
281 propagated and settled outside the test region (i.e.  $r_m > 18$  cm). By comparing the profiles in  
282 Fig. 4, the variation among the replicates was found to be very small, which was attributed to  
283 the careful handling which minimized human errors during the measurement process and  
284 randomness in the releases.

285 Fig. 5 illustrates the attenuated intensity profiles from Test LA normalized by the reference  
286 intensity,  $I_{b\ ref}$ . In contrast, Munro and Dalziel (2005) normalized  $I(p,q)$  by  $I_{ref}(p,q)$  recorded  
287 at the beginning of each test, where  $p$  and  $q$  denote the row and column vectors of the pixel  
288 matrix. The pixel-by-pixel normalization could be achieved only when the camera and tank

289 were stationary from pre- to post-tests. In the current experimental setup, the camera had to be  
290 moved for the installation of the funnel or the model barge. Hence, the pixels were not exactly  
291 aligned in the images between pre- and post-tests. In this case, the normalization had to be done  
292 with a mean intensity produced by a uniform light source. From Fig. 5, it is noted that the  
293 attenuation profile had a similar distribution pattern as the sediment depth profile measured  
294 from Test MC (Fig. 4). The variation among the replicates was also insignificant as shown  
295 from the plotted error bars.

296

### 297 **Calibration Curves**

298 A piece-wise continuous calibration curve was established for the current approach and  
299 presented in Fig. 6, with the solid and dashed lines representing the curve in near-zero limit  
300 and self-similar regimes, respectively. A break in the curve at  $h_s/d_{50} = 16.7$  can be identified  
301 which agrees well with the critical  $h_s/d_{50}$  ( $h_c/d_{50} = 18$ ) found by Munro and Dalziel (2005) using  
302 the scraper method. It could be argued that the agreement was coincidental because, for our  
303 chosen  $d_{50} = 0.12$  mm, the break point at  $h_s/d_{50} = 16.7$  occurred at a value of  $h_s = 2$  mm which  
304 was also the dividing line between the scraper method and sediment deposition method. To  
305 verify that the critical value of  $h_s/d_{50}$  was associated with light attenuation rather than the  
306 method of profile generation, several supplemental tests (Test ETs) were carried out using  
307 larger values of  $d_{50}$  as summarized in Table 3. The results are shown in Fig. 7 and again the  
308 break in calibration curves occurred at  $h_s/d_{50} \sim 18$  (vertical dotted line), which was close to the  
309  $h_c/d_{50}$  discussed above.

310 The effect of shallowness is illustrated in Fig. 8, with Fig. 8(a) showing the transmission of  
311 light through a single particle. Due to the spherical shape, the attenuation of light is greater in  
312 the center and weaker at the sides. When the light is passing through a layer of particles with  
313  $h_s/d_{50} = 2$ , the packing of particles is important as illustrated in Fig. 8(b) and (c). However, the

314 packing of particles is less important for thick sediment layer ( $h_s \gg d_{50}$ ) as every light ray  
 315 needs to transmit through similar layers of particles. The attenuation of light may not be  
 316 uniform when the sediment layer is shallow. In this study, the particles are randomly packed  
 317 and averaged values are used. Overall, the results in Fig. 7 suggested that the break in the  
 318 calibration curve was due to the physics of light transmission as discussed above rather than  
 319 the profile generation method.

320 From Fig. 6, in the self-similar regime, the data (filled markers) were measured from the  
 321 calibration rings (scraper method) with three or five replicates. As expected, the attenuation  
 322 followed the Beer-Lambert's law and experienced an exponential decay with the following  
 323 equation:

$$\frac{I_b}{I_{b\ ref}} = c \exp \left\{ -k_1 \left( \frac{h_s}{d_{50}} \right) \right\} \quad (8)$$

324 where  $c$  and  $k_1$  were determined to be 0.966 and 0.027, respectively from the least-square fit.

325 In the near-zero limit regime, the data (open markers) were determined by correlating the  
 326 two profiles discussed in the previous section (i.e.  $h_s/d_{50}$  vs.  $r_m$  and  $I_b/I_{b\ ref}$  vs.  $r_m$  to generate  
 327  $I_b/I_{b\ ref}$  vs.  $h_s/d_{50}$ ). Here, two regions in the depth distribution profile ( $h_s/d_{50}$  vs.  $r_m$ ) were  
 328 identified: (i) the region with  $h_s < d_{50}$ , within which the area was not fully covered by the  
 329 sediment particles and (ii)  $r_m < 4$  cm, where the gradient of  $h_s$  ( $dh_s/dr_m$ ) was steep and current  
 330 grid space was insufficient to accurately acquire the depth profile in this region. Therefore, the  
 331 results in these regions were not included.

332 Fig. 6 suggests that the attenuation is linearly proportional to  $h_s/d_{50}$ , and can be expressed  
 333 as

$$\frac{I_b}{I_{b\ ref}} = a + b \left( \frac{h_s}{d_{50}} \right) \quad (9)$$

334 where  $a (= 1)$  is constrained to yield  $I_b/I_{b\ ref} = 1$  at  $h_s/d_{50} = 0$  and  $b$  was determined to be  $-0.023$   
335 from the least square fit. The calibration curve is only applicable down to  $h_s/d_{50} = 1$  (i.e.  $I_b/I_{b\ ref}$   
336  $= 0.977$ ), below which the pixel area is not fully covered by sediment.

337 As discussed earlier, in the previous approach, the curve was established from the scraper  
338 method and fitted with

$$\frac{I_b}{I_{b\ ref}} = \exp \left\{ -k_2 \left( \frac{h_s}{d_{50}} \right)^\gamma \right\} \quad (10)$$

339 constraining to  $I_b/I_{b\ ref} = 1$  at  $h_s/d_{50} = 0$  and  $I_b/I_{b\ ref} \rightarrow 0$  when  $h_s/d_{50} \rightarrow \infty$  (Munro and Dalziel  
340 2005), with  $k_2 = 0.029$  and  $\gamma = 1$  obtained from the collected data. Fig. 9 compares the  
341 calibration curves in the near-zero limit regime established from current (solid line) and  
342 previous (dashed line) approaches. The variation in the measurements of  $h_s/d_{50}$  with the present  
343 approach was primarily within the range of 0 to 1.2.

344

## 345 **Application – Deposition of Barged Sediment Disposal**

346 Activities such as dredging (with associated dredged material management) and land  
347 reclamation often involve open water sediment disposal. A barge is commonly used to transport  
348 and dispose of the sediments due to its large carrying capacity. From field observations,  
349 Bokuniewicz et al. (1978) identified three phases of the sediment transport upon release: (i)  
350 convective descent phase, during which the flow behavior is dominated by the disposal  
351 conditions and driven by gravity, (ii) bottom collapse phase, during which the disposed  
352 sediments impact the seabed and begin to spread horizontally, and (iii) passive-transport  
353 dispersion phase, when the sediments are passively carried by the ambient currents and  
354 turbulence.

355 In the present study, the laboratory investigation of barged sediment disposal was  
356 conducted in the same water tank, with the same water depth ( $h = 10$  cm) as the calibration

357 tests. A model barge (shown in Fig. 10, made with two rectangular acrylic boxes) was designed  
358 from an actual barge scaled down to dimensions of 20 cm (length,  $L$ )  $\times$  4 cm (width,  $W_b$ )  $\times$  4  
359 cm (depth,  $D_b$ ). Once the experiment was initiated, the two rectangular boxes would rotate in  
360 opposite directions with an angular speed,  $\omega$ , forming an opening (opening width,  $W = 0.8$  and  
361 0.5 cm) in the middle through which the sediment was released. The attenuated intensity profile  
362 of the deposited sediment was taken from a single release of 112 g of sediment particles  
363 (Ballotini Impact beads,  $d_{50} = 0.12$  mm).

364 Upon release, the sediment cloud would descend through the water column and grow in  
365 lateral size due to entrainment. Upon impact with the bottom, gravity currents would be  
366 initiated by the cloud buoyancy to propagate horizontally, as illustrated in Fig. 11. In contrast  
367 to the deposition from a funnel with an axisymmetric round opening, the rectangular opening  
368 of the model barge created a nearly elliptical deposition pattern with the major axis  
369 perpendicular to the barge, as presented in the last photo of Fig. 11. This was due to the fact  
370 that the gravity current initiated by the two-dimensional starting plume, as predicted by BSDM  
371 (Barged Sediments Disposal Model) (Er et al. 2016) based on the present release parameters,  
372 grew primarily in the transverse direction ( $x$ -axis).

373 Figs. 12 and 13 illustrate the sediment depth profiles determined from current (symbols)  
374 and previous approaches (lines) at various cross sections for the two tests with  $L/W = 24$  and  
375 40, respectively. The spreading behavior of the gravity currents along the azimuthal direction  
376 could be explained by comparing the longitudinal profiles ( $h_s$  vs.  $x$ ) at different  $y$ -locations.  
377 The gravity currents had the highest spreading near the center of the barge ( $y = 0$  cm), and  
378 weakened when approaching the edge of the barge ( $y = 10$  cm). This might be attributed to the  
379 minor longitudinal spreading and shear force exhibited on the boundaries of the gravity current.

380 In general, both approaches were able to capture the spreading behavior of the gravity  
381 currents. However, the maximum sediment depths and horizontal extents of the deposition

382 profiles determined from the previous approach were smaller than those of LAM2D. For  
383 instance, in the test with  $L/W = 24$ , measurement from LAM2D showed that the deposition  
384 profiles at  $y = 10$  and  $12$  cm could reach a maximum of  $x = 15$  and  $10$  cm, respectively.  
385 However, the previous approach yielded contracted profiles with the maximum  $x$ -direction  
386 extent at these two cross sections being only  $5$  and  $10$  cm, respectively. Moreover, based on  
387 the transverse profiles ( $h_s$  vs.  $y$ ), the previous approach failed to capture the sediments that  
388 deposited beyond  $x = 20$  cm. Similar conclusions could be drawn when comparing the profiles  
389 from the test with  $L/W = 40$ . Most importantly, the total mass conservation errors,  $\varepsilon_t$  from  
390 LAM2D ( $\varepsilon_{t \text{ cur}} = -9.6\%$  and  $-9.8\%$  for  $L/W = 24$  and  $40$ , respectively) were significantly less  
391 than those of the previous approach ( $\varepsilon_{t \text{ pre}} = -24.4\%$  and  $-21.9\%$  for  $L/W = 24$  and  $40$ ,  
392 respectively). These differences in mass conservation errors between previous and current  
393 approaches are significant when compared with the less than  $2\%$  sediment loss in an  
394 experiment. We could account for  $98.4\%$  of the mass within our measurement domain with  
395 the remaining  $1.6\%$  presumably being transported downstream. The mass conservation error  
396 would generally be negative because some sediment inevitably fell outside the domain. The  
397 reduction in error can be directly attributed to the improved calibration in the near-zero limit  
398 regime with the present approach.

399

## 400 **Conclusions**

401 An improved light attenuation method (LAM2D) was developed in this study using a CMOS  
402 camera and analyzing the blue signal. The approach method used different calibration  
403 techniques for the two ranges of deep and shallow sediment depths, with the traditional scraper  
404 method and the correlation of particle plume deposition profiles (depth distribution and  
405 attenuated intensity profiles), respectively. The calibration curve for each was established with  
406 data only in the respective range to better represent the attenuation behavior. The improved

407 method (LAM2D) was shown to reduce the mass conservation error significantly for shallow  
408 sediment depth (near-zero limit regime), compared with the previous approach with calibration  
409 based only on the scraper method.

410 LAM2D, or the light attenuation method in general, has two caveats: (i) the light panel  
411 needs to perform consistently throughout the test, and (ii) changing the setup, i.e. type of  
412 sediment particles, camera or light panel, requires re-calibration. There is also a challenge to  
413 use poly-dispersed particles in LAM as the attenuation varies with particle sizes as illustrated  
414 in Figs. 6 and 7. However, the poly-dispersed particles could be represented with an equivalent  
415 particle size to obtain the calibration curve. It should be mentioned that most laboratory  
416 applications use mono-dispersed, or nearly mono-dispersed particles, lessening the  
417 complications associated with variable grain sizes. With the appropriate adjustment of the  
418 calibration technique, we expect LAM2D could be useful in related applications such as the  
419 measurement of the thickness of oil spreading on the water surface and the quantification of  
420 the suspended sediments concentration in the water column.

421

## 422 **Acknowledgements**

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426

427

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- 491

492 **List of Tables**

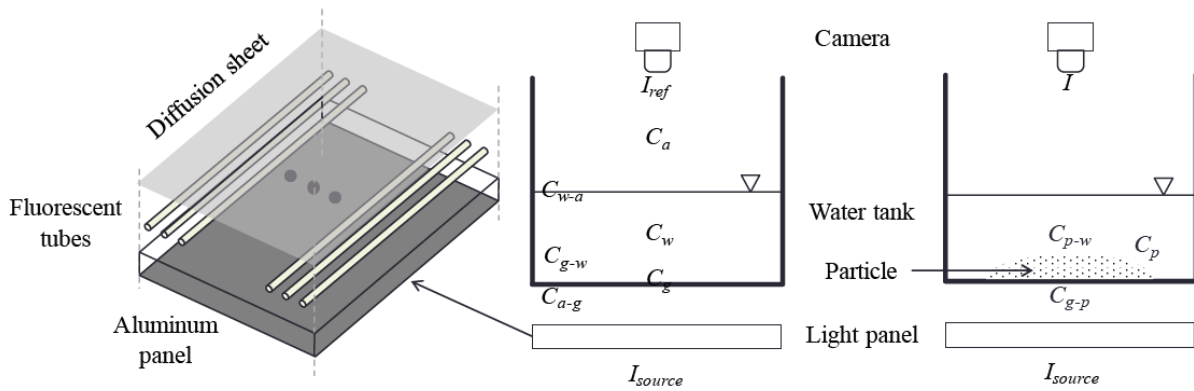
493 **Table 1.** Criteria for the selection of DSLR camera parameters

494 **Table 2.** Experimental conditions for particle plume deposition tests

495 **Table 3.** Experimental conditions for supplemental tests

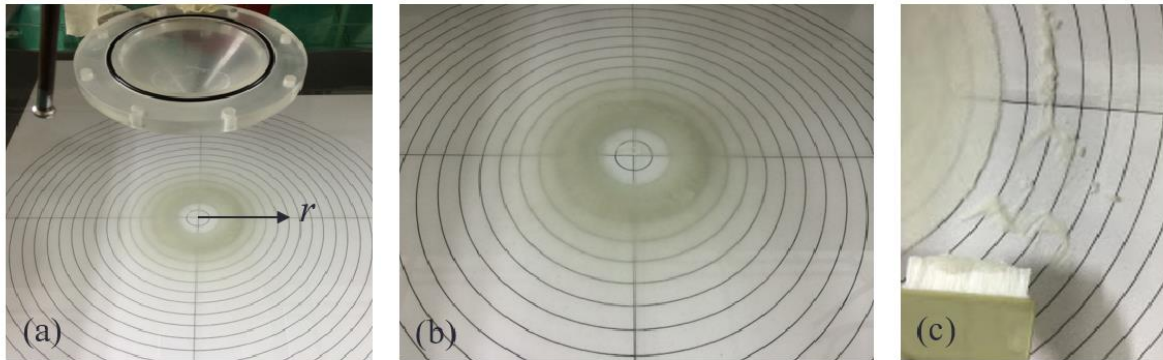
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497 **List of Figures**



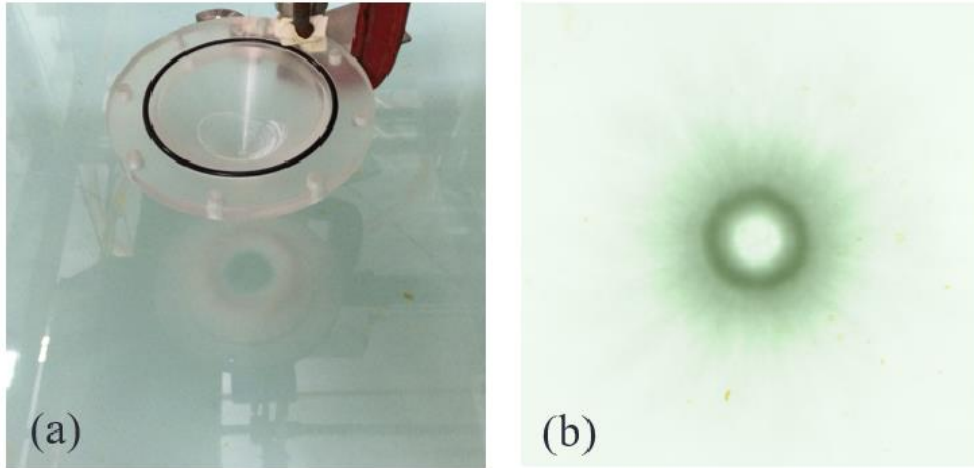
498  
499 **Fig. 1.** Schematic diagram of the principle of LAM2D and experimental setup

500



501  
502 **Fig. 2.** Deposition of particle plume from five releases on a 10 mm grid space circular grid  
503 platform, (a) top view, (b) top view without funnel, and (c) sediment collection  
504 within grid with brush

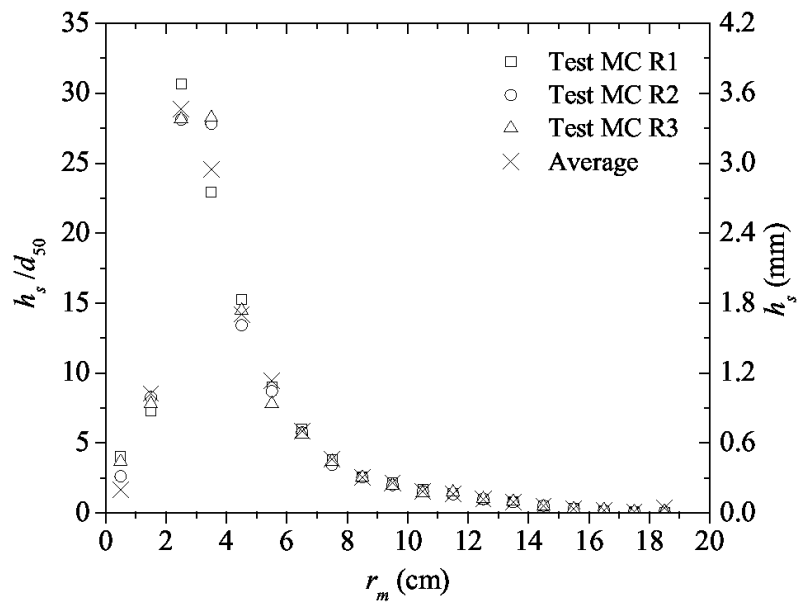
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506

507 **Fig. 3.** Deposition of particle plume from five releases in water tank using backlighting with  
 508 light panel, (a) top view, and (b) top view without funnel

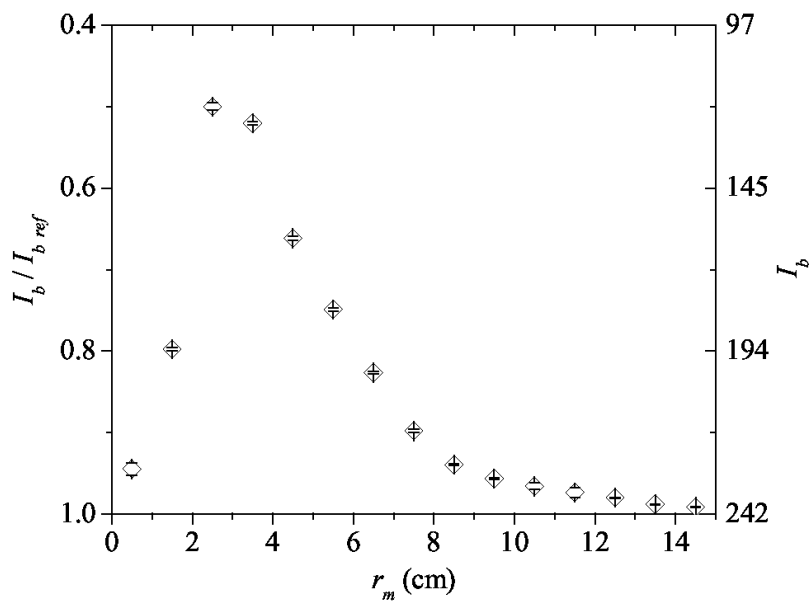
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511 **Fig. 4.** Relationship between sediment depth,  $h_s/d_{50}$  and radius,  $r_m$  for three replicates of Test  
 512 MC (symbols) and averaged value (cross)

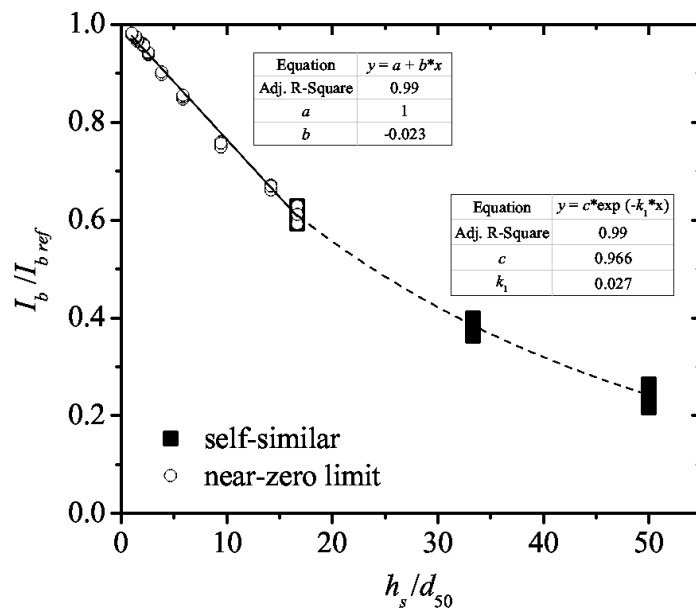
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515 **Fig. 5.** Relationship between attenuated intensity,  $I_b/I_{b\ ref}$  and radius,  $r_m$

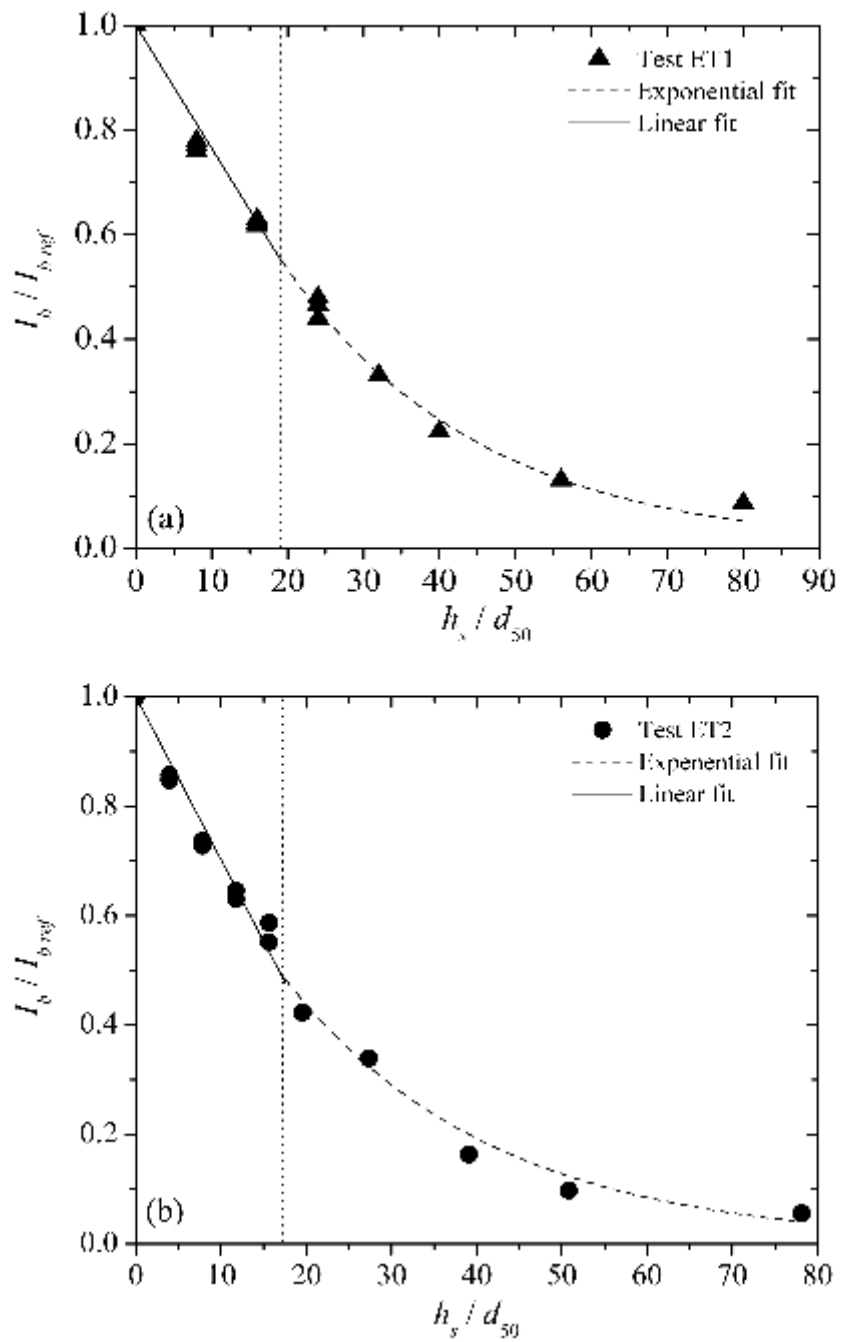
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517

518 **Fig. 6.** Overall calibration curve

519



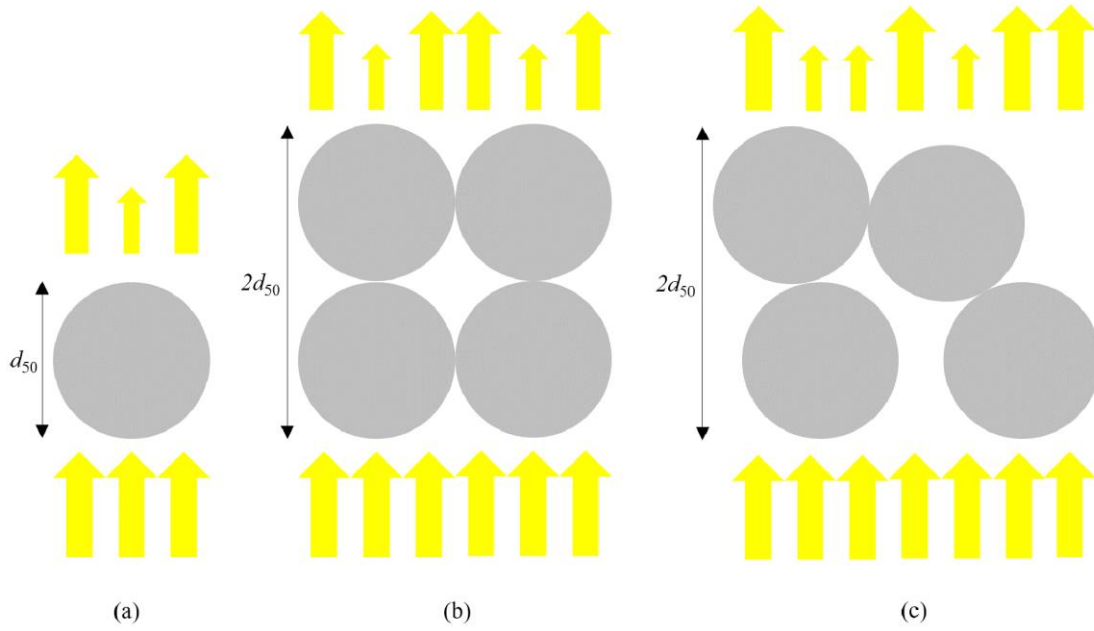
520

521 **Fig. 7.** Calibration curves from Tests (a) ET1 and (b) ET2. Note that, for smaller values of

522  $h_s/d_{50}$ , up to three replicates were conducted in anticipation of greater experimental

523 variability in measurements at small  $h_s$

524



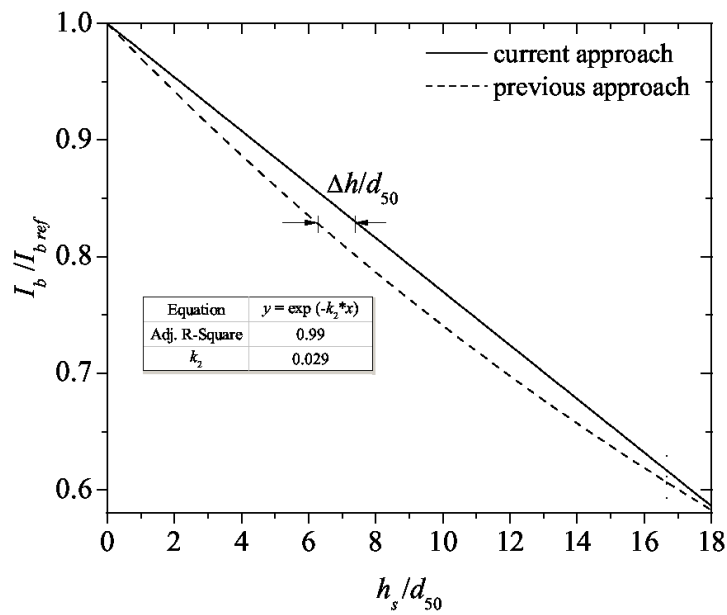
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526 **Fig. 8.** Schematic diagram of light passing through (a) a single particle, and two layers of

527 particles with different packing configurations in (b) and (c). The size of arrows

528 represents the intensity of light

529

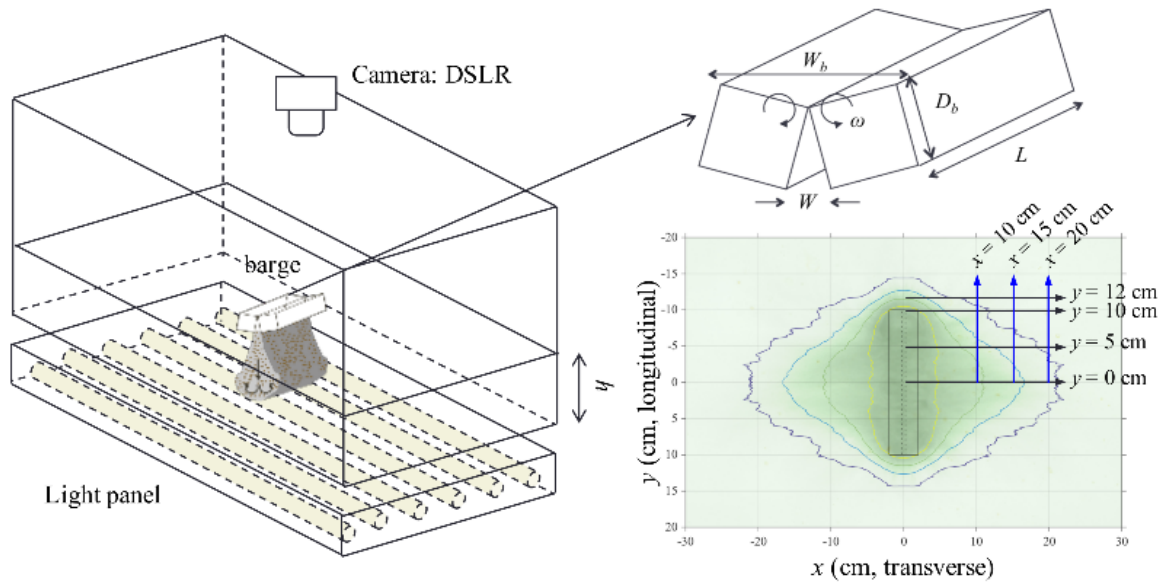


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531 **Fig. 9.** Comparison of calibration curves in near-zero limit regime from current and previous

532 approaches

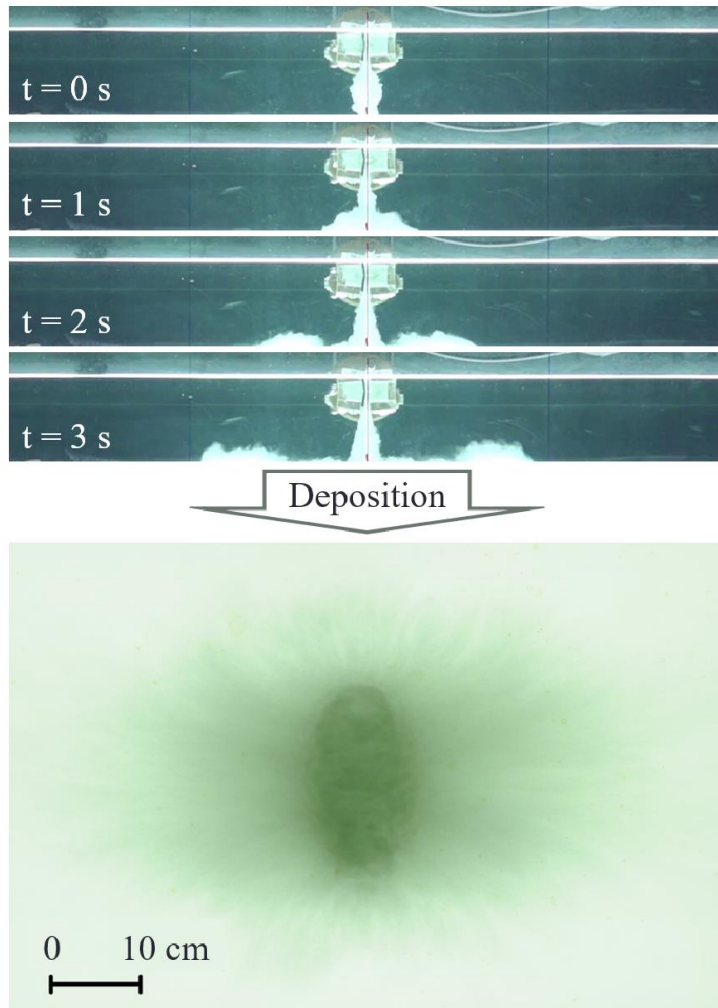
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535 **Fig. 10.** Schematic diagram of model barge and illustration of deposition profiles at different  
536 cross-sections (lower right)

537

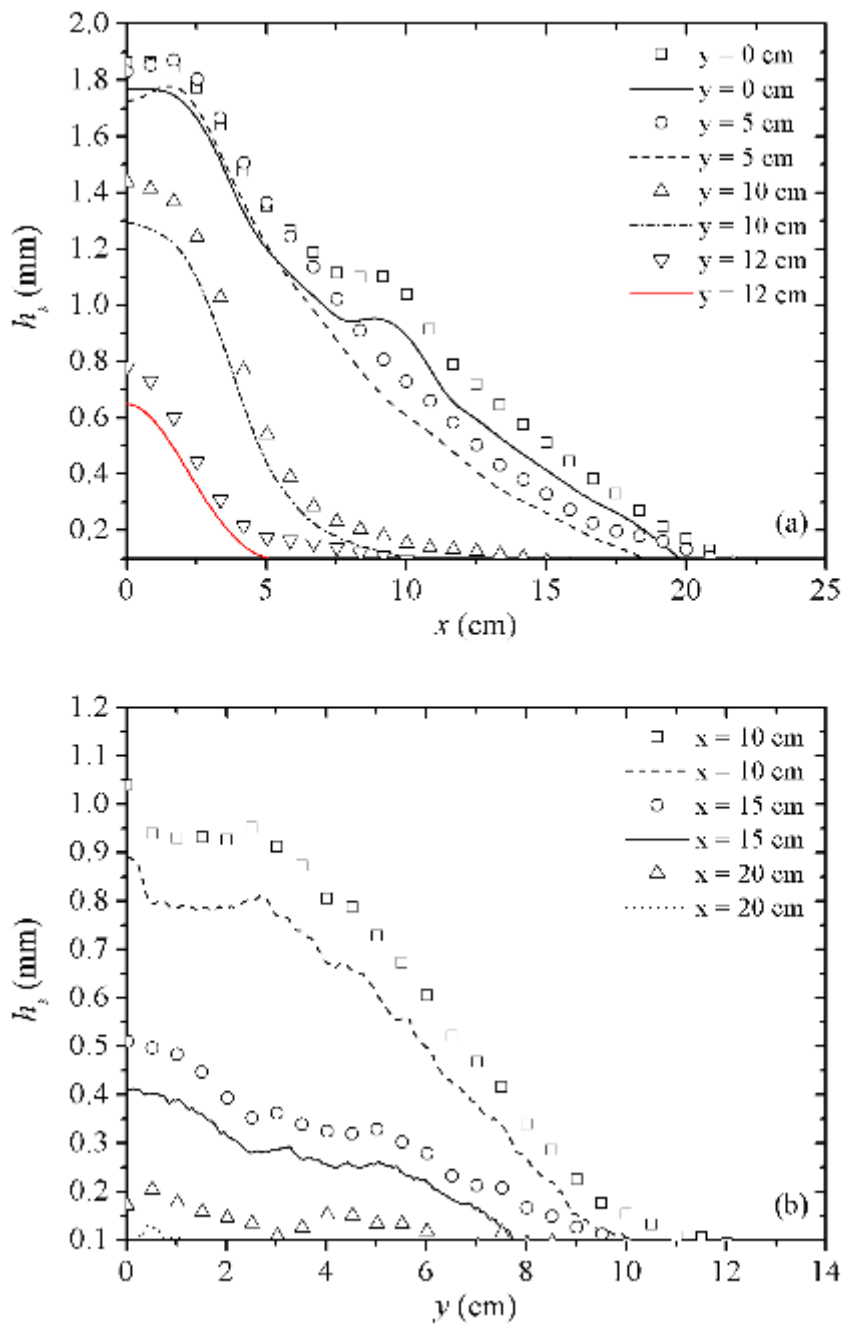


538

539 **Fig. 11.** Development of gravity currents and the deposition profile from barged sediments

540 disposal

541



542

543 **Fig. 12.** Deposition profiles from barged sediment disposal ( $d_{50} = 0.12\text{mm}$ ,  $L/W = 24$ ) at (a)

544

$y = 0, 5, 10$  and  $12$  cm (longitudinal profile) and (b)  $x = 10, 15$  and  $20$  cm

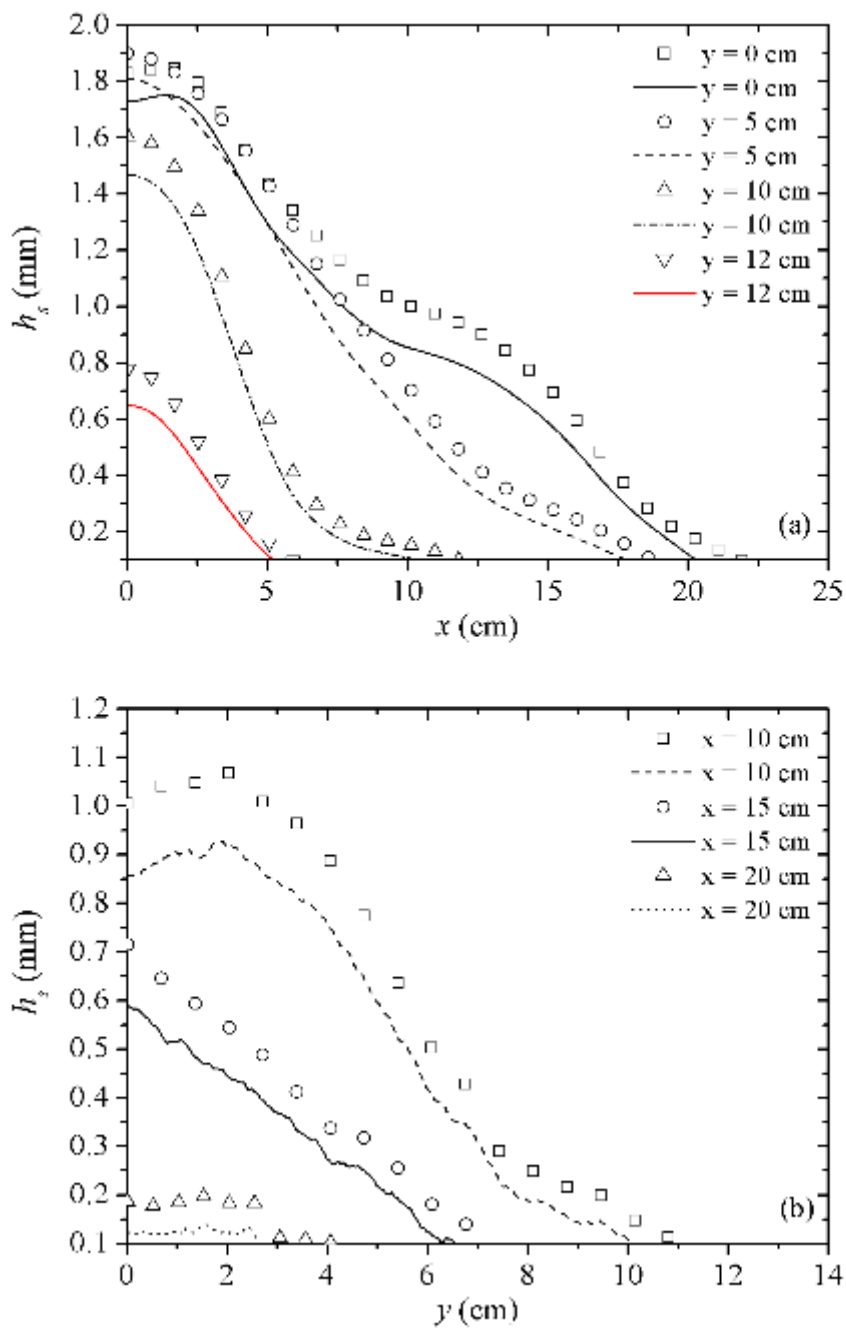
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(transverse profile). Symbols denote current approach and lines denote previous

546

approach

547



548

549 **Fig. 13.** Deposition profiles from barged sediment disposal ( $d_{50} = 0.12\text{mm}$ ,  $L/W = 40$ ) at (a)

550  $y = 0, 5, 10$  and  $12$  cm (longitudinal profile) and (b)  $x = 10, 15$  and  $20$  cm

551 (transverse profile). Symbols denote current approach and lines denote previous

552 approach

553

554 **Tables**

555 **Table 1.** Criteria for the selection of DSLR camera parameters

Parameter	Description & Criteria
Exposure time, $t_c$	Duration of camera shutter opening to expose the sensor to the light. $t_c$ to be higher than 1/40 to mitigate flicker
ISO Sensitivity	Ability of the sensor to capture light and convert into electrical signals for processing. Lowering the ISO value reduces the noise and hence is preferable for LAM2D
$f$ -stops, $f/n$	Opening size of the aperture blades, which controls the amount of light entering the camera and affects the depth of field. Large $n$ value is preferable to increase the depth of field
White Balance	Adjustment of the image color to match the real color, so that the color of the photo matches that observed visually

556

557

**Table 2.** Experimental conditions for particle plume deposition tests

Test	Mass per release (g)	Replicates	No. of releases	Remarks
MC	10	5	5	-
LA	10	5	5	R1 & R2 – day 1 R3 & R4 – day 2 R5 – day 3

558

559

**Table 3.** Experimental conditions for supplemental tests

Test	Size range (mm)	$d_{50}$ (mm)	$h_s$ (mm)	Range of $h_s/d_{50}$
ET1	0.21 ~ 0.30	0.25	2, 4, 6, 8, 10, 14, 20	8 – 80
ET2	0.43 ~ 0.60	0.51	2, 4, 6, 8, 10, 14, 20, 26, 40	4 – 78

560 Note: The number of replicates differed with  $h_s$  (varied from one to three), with thicker  $h_s$   
561 needing fewer replicates because experimental observations showed that variability decreased  
562 when  $h_s$  increased