

1 **An Integrated Silicon Photonic Chip Platform**
2 **for Continuous-Variable Quantum Key Distribution**

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1 **To realize a miniaturized and low-cost quantum key distribution (QKD)**
2 **system on an integrated photonic chip is challenging yet highly coveted for the**
3 **development of quantum networks¹⁻³. Continuous-variable QKD (CV-QKD) is**
4 **particularly suitable for cost-effective photonic integration due to its compatibility**
5 **with existing fiber optical communication technology⁴. In this paper, an integrated**
6 **silicon photonic chip that implements the Gaussian-modulated coherent state**
7 **protocol for CV-QKD^{5, 6} is demonstrated. All required components, except the laser,**
8 **are integrated on the silicon photonic chip. Our proof-of-principle chip-based CV-**
9 **QKD system is capable of producing a secret key rate of 0.14 kbps (under collective**
10 **attack) over a simulated distance of 100 km in fiber, offering new possibilities for low-**
11 **cost, scalable and portable quantum networks.**

12 Quantum key distribution (QKD) is an emerging technology that applies
13 fundamental quantum mechanic theories to realize unconditional communication security¹,
14 ². QKD has been successfully demonstrated in various platforms such as fiber optical
15 communication, free-space communication and satellite². Silicon photonic technology
16 enables on-chip QKD with many unprecedented advantages^{3, 7}. Over the past few years,
17 different substrates have been explored for chip-level integration of QKD³. Indium
18 phosphide (InP)⁸, lithium niobate (LiNbO₃)⁹ and potassium titanyl phosphate (KTP)¹⁰ have
19 been used to fabricate on-chip lasers and fast modulators. Silica^{11, 12} offer low-loss delay
20 line and fiber-chip coupler, but lack rapid modulation. Silicon relies on well-established
21 microfabrication techniques and is ideally suited for both on-chip photonic components.

22 There are two major categories of QKD systems, namely discrete-variable (DV-
23 QKD) and continuous-variable QKD (CV-QKD). Fiber-based DV-QKD has been

1 demonstrated up to around 400-km ultra-low loss fiber^{13, 14}. The key rate is around kbps
2 level at 100 km distance, as reported in ref¹⁴. Several DV-QKD protocols, including
3 encoding on photon polarization¹⁵, spatial dimension¹⁶ and time bin¹⁷, have been
4 demonstrated on silicon wafers. To detect photons on-chip, superconducting nanowire-
5 based single-photon detectors with detection efficiencies up to 90% are integrated on chip¹⁸.
6 ¹⁹. Compare to DV-QKD, CV-QKD is more suitable for photonic chip integration due to
7 its compatibility with existing telecom technologies^{20, 21}. A fiber-based CV-QKD system
8 showed a secure key rate of about 1 kbps at 80 km transmission distance in 2013²², and the
9 distance was further pushed to over 100 km by controlling the excess noise²³. Very recently,
10 several on-chip quantum entropy sources based on the detection of phase-fluctuation²⁴⁻²⁶
11 and vacuum fluctuation²⁷ were reported. The chip-based homodyne detector showed a gain
12 of 4.5 kV/A with 150-MHz bandwidth²⁷.

13 In this paper, we report a Gaussian-modulated coherent states CV-QKD protocol
14 on an integrated silicon photonic chip. The on-chip integration increases the stability and
15 scalability of all optical components, reduces the cost, and extends the applicability of
16 photonic chip to CV-QKD and potentially other quantum communication protocols.

17 Figure 1 shows the schematics of the silicon photonic CV-QKD chip. In the
18 transmitter chip (Alice), a 1550-nm continuous wave (CW) laser is coupled into the
19 waveguide with a grating coupler. The first modulator serves as an attenuator to control
20 the input laser intensity. A 1:99 directional coupler splits the input laser into two paths,
21 with the weaker one as signal and the stronger one as the local oscillator (LO). The signal
22 path is modulated with an amplitude modulator (AM) and a phase modulator (PM) to
23 generate a series of coherent state $|x_A + ip_A\rangle$, where x_A and p_A are random numbers with a

1 Gaussian distribution. The information is encoded by modulating the continuous light
2 signal on the sideband ranging from 1-10 MHz^{28,29}. A digital filter and demodulator extract
3 the information from one of the sideband frequencies. To keep the relative phase between
4 the signal path and the LO path after transmission, the modulated signal and LO are
5 multiplexed into two orthogonal polarization states with a two-dimensional (2D) grating
6 coupler. After the signal is transmitted over a line with a transmittance T , the receiver (Bob)
7 first compensates the polarization drift with a polarization controller followed by
8 demultiplexing of the signal and the LO with another 2D grating coupler. Unlike previous
9 protocols which requires an ultra-high (60-80 dB) intensity difference between the signal
10 and the LO^{22,30}, our design only requires a 35-dB extinction ratio because the information
11 is encoded on the sideband frequency which is the AC component of the signal light.
12 Finally, Bob arbitrarily measures quadrature x or p with the homodyne detector and filters
13 out the required frequency. The security of CV-QKD is guaranteed by the Heisenberg
14 uncertainty principle between the x and p quadratures. Because the two quadratures do not
15 commute, eavesdropper's (Eve) attempt to measure one quadrature would result in noise
16 in the other, which implies that the amount of information leaked to Eve is bound by the
17 noise level detected by Alice and Bob.

18 Figure 2a illustrates the Mach-Zehnder interferometer (MZI) structure designed as
19 the amplitude modulator. The photo of the transmitter chip packaged with PCB is shown
20 in Figure 2b. Figure 3a demonstrates that the amplitude and phase modulators have a 90%-
21 switching time of 2.5 ns, which corresponds to a 200-MHz modulation frequency. Limited
22 by the detector bandwidth, the system is designed to operate between 1-10 MHz, right
23 within the range of the modulator.

1 The displaced coherent state is measured by the balanced homodyne detector,
2 integrated on the receiver chip. The homodyne detector consists of a 50 : 50 beam splitter
3 (BS) and two photodiodes (PD) as shown in Figure 2c. The signals from the two PDs are
4 subtracted and amplified using a two-stage transimpedance amplifier operating at 1-10
5 MHz, which defines the bandwidth of the homodyne detector. The transimpedance gain is
6 10^5 V/A. The homodyne detector must be able to distinguish the shot noise of the LO light
7 from the electronic background noise, because CV-QKD uses the constant shot noise as a
8 reference to normalize the signals and detect potential eavesdroppers. The total noise of
9 the homodyne detector is measured as a function of LO power at 1 MHz and 3 MHz bands
10 as shown in Figs. 3b and 3c, respectively. The fitted shot noise has a linear relationship
11 with the LO power. When the LO power is higher than 10 mW, the shot noise is at least 5
12 dB higher than the electronic background noise. This difference is referred to as the shot
13 noise clearance (SNC). The homodyne detection efficiency is calculated as $\eta =$
14 $\eta_{PD}\eta_{vis}^2 = 0.498$, where η_{PD} is the quantum efficiency of photodiode and η_{vis} is the
15 visibility.

16 The QKD transmitter chip is calibrated using an off-chip detector with a fiber
17 polarization control. The quadrature selection is achieved by maximizing the cross-
18 modulation peak-to-peak difference. Both the output signal and the input signal for x and
19 p quadrature modulation are recorded, and the data are collected for 4 ms with a sampling
20 frequency of 25 MHz. The output signal on Bob's side is synchronized with Alice's
21 modulation signal by measuring their cross-correlation. Figure 4a shows the normalized
22 cross-correlation measurement between the homodyne detector output and the
23 corresponding modulation signal. Figure 4b shows the cross-correlation between the

1 homodyne detector output and the other modulation signal. The differences between the
2 two cross-correlations are more than 10-fold. The small correlation with the different
3 quadrature is due to the phase noise between the signal and the LO, which is one of the
4 main contributions of the excess noise. All signals are synchronized based on the cross-
5 correlation and passed through a digital bandpass filter between 2.8 and 3.2 MHz. Next,
6 the filtered signals are demodulated and downsampled to 0.8 Mbps to generate a set of
7 correlated Gaussian key, that are shown in the insets of Figure 4a and 4b with Alice's key
8 as x -coordinate and Bob's key as y -coordinate. These plots confirm that Bob's key only
9 correlates to one of Alice's keys with the same measured quadrature. Information
10 reconciliation is then applied to the correlated Gaussian key (see Methods).

11 The secure key rate at a longer distance is calculated based on the assumption of
12 individual attack and collective attack under the trusted device scenario, which means an
13 eavesdropper cannot access the noise from Bob's lab²⁰. The total losses consist of the losses
14 on the transmission line and Bob's equipment while the losses on the Alice side do not
15 affect the final security key. The homodyne detection efficiency is measured to be $\eta =$
16 0.498. The 5-dB loss of Bob's chip is considered as an additional 68.3% drop in efficiency.
17 The total excess noise is $\varepsilon = 0.0934$ SNU at a modulation variance of $V_{mod} = 7.07$ SNU and
18 $T = 1$. Detector electrical noise is $v_{el} = 0.0691$ SNU. Symbol rate is $SR = 0.8$ Mbps. With
19 these data, the secure key rate of the current CV-QKD system is estimated. The Shannon
20 raw key rate and Holevo raw key rate are given as the dashed line in Figure 5. Considering
21 a more practical situation, the reconciliation efficiency $\beta = 0.98$ and 0.99 is chosen^{31, 32},
22 which represents the case we have achieved and the state-of-the-art case. The

1 corresponding Shannon effective key rate and Holevo effective key rate are shown as the
2 solid line in Figure 5.

3 We performed an experiment to demonstrate CV-QKD over a 2-m fiber link. To
4 generate secret keys, the slice reconciliation and low-density parity check (LDPC) error
5 correction are performed on the measured data. The resulting secret key rate is 0.25 Mbps,
6 which is shown as a solid dot in Figure 5. Furthermore, to prove the capability for long-
7 distance CV-QKD, we simulated the total noise χ_{tot} and obtain that SNR = 0.028 (see
8 Methods), by considering a 16-dB loss (equivalent to 100 km ultra-low-loss fiber with 0.16
9 dB/km). In such a low SNR, we developed a rate-adaptive reconciliation protocol based on
10 multidimensional reconciliation and multi-edge type LDPC codes (see Supplementary). A
11 high reconciliation efficiency of 97.99% was achieved, and the expected secret key rate is
12 0.14 kbps, which is indicated as a circle in Figure 5. Our system is comparable to the state-
13 of-the-art DV-and CV-QKD systems in terms of performance and has a smaller size and
14 potential for chip-integration and mass production.

15 In conclusion, this is the first time that the silicon photonic chip has been used for
16 CV-QKD. All components except the laser source, including the modulators, multiplexers
17 and homodyne detectors, are integrated on a silicon photonic chip. Future demonstrations
18 will focus on full-system integration with on-chip laser source. Well-Characterized noise
19 sources and careful modeling may mitigate the impact of excess noise from experimental
20 imperfection and improve the secret key rates^{23, 33}. Some recently developed self-
21 referenced CV-QKD protocols suggest that the LO could be generated locally at Bob's
22 side, which would significantly improve the security of current CV-QKD system³⁰. Our

1 robust and inexpensive photonic chip can promote real-world applications of on-chip
2 hybrid quantum-classical communication for advanced communication network.

3

4 **Methods**

5 **Experimental setup.** The source was a 1550-nm laser with 12 dBm power from Santec
6 TSL-510 tunable laser. After a polarization controller, the laser was coupled to the photonic
7 chip. The AM and PM were then performed by applying two white noise signals from HP
8 33120A arbitrary waveform generator. The white noise frequency could reach up to 10
9 MHz. For the current proof-of-principle testing, the LO phase tuning was also conducted
10 on the same chip. An off-chip homodyne detector was used to assist the measurement of
11 excess noise and modulation variance from Alice’s chip. A Peltier device together with a
12 Thorlab TED200C temperature controller was used to stabilize the temperature of the
13 entire chip, which would reduce the noise from environment heat fluctuation and heat
14 crosstalk on the chip. The output from the homodyne detector was monitored in both time
15 and frequency domains on a Tektronix MDO4104B-3 oscilloscope. The data were
16 analyzed offline using Matlab.

17

18 **Information reconciliation.** A full demonstration of CV-QKD including the post-
19 processing was presented. The efficiency of the protocol only depended on the signal-to-
20 noise ratio (SNR) of the transmission. Here, under the pure lossy channel assumption, the
21 SNR of the transmission was defined as

22
$$SNR = \frac{V_{mod}}{1 + \chi_{tot}},$$

1 where V_{mod} is the modulation variance and χ_{tot} is the total added noise between Alice and
2 Bob. Two post processing protocols are implemented to generate the secret key in the
3 second stage. The selection of the protocol is based on the SNR of the transmission. With
4 a high SNR (SNR = 2.20), which corresponded to a 2-m fiber transmission distance, the
5 slice reconciliation and low-density parity check (LDPC) error correction are performed
6 on the measured data. The resulting secure fraction was 0.516 bits/symbol. With a low
7 SNR (SNR = 0.028), which corresponded to a 100-km simulated transmission distance, we
8 had developed a rate-adaptive reconciliation protocol based on multidimensional
9 reconciliation and multi-edge type LDPC codes. A reconciliation efficiency of 97.99% was
10 achieved. The resulting secure fraction was 1.8×10^{-4} bits/ symbol.

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2 **Author contributions**

3 G.Z., L.C.K., and A.Q.L. jointly conceived the idea. G.Z., and H.C. designed and
4 fabricated the silicon photonic chip. G.Z., Y.Z., S.Y., J.W., W.S., F.X and X.Q.Z
5 performed the experiments. J.Y.H., S.M.A., J.F.F and L.C.K assisted with the theory. All
6 authors contributed to the discussion of experimental results. F.X., L.C.K., and A.Q.L.
7 supervised and coordinated all the works. G.Z., F.X., L.C.K., and A.Q.L. wrote the
8 manuscript with contributions from all co-authors.

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10 **Competing interests**

11 The authors declare no competing interests.

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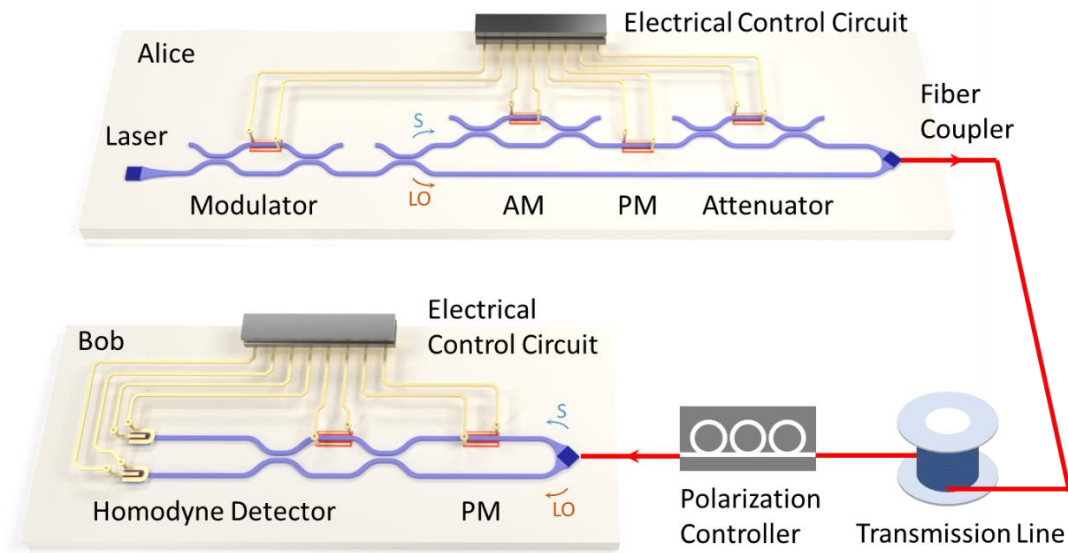
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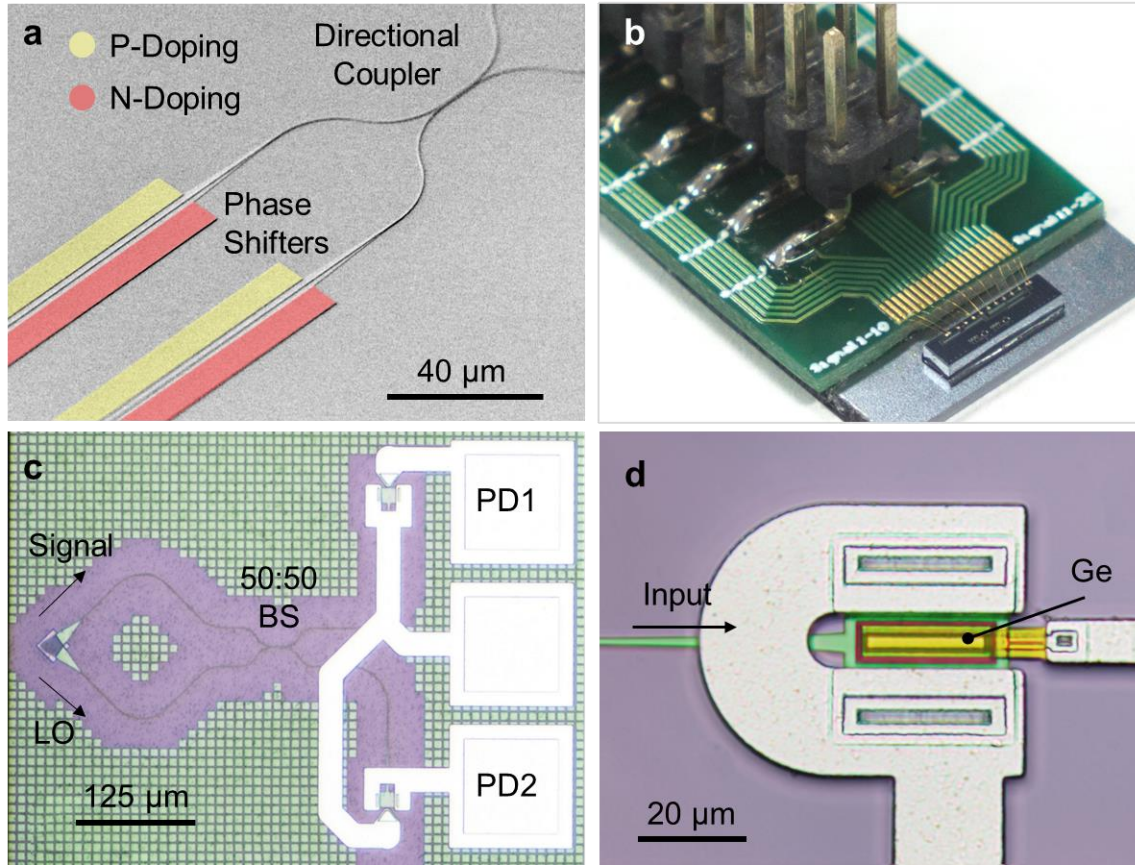
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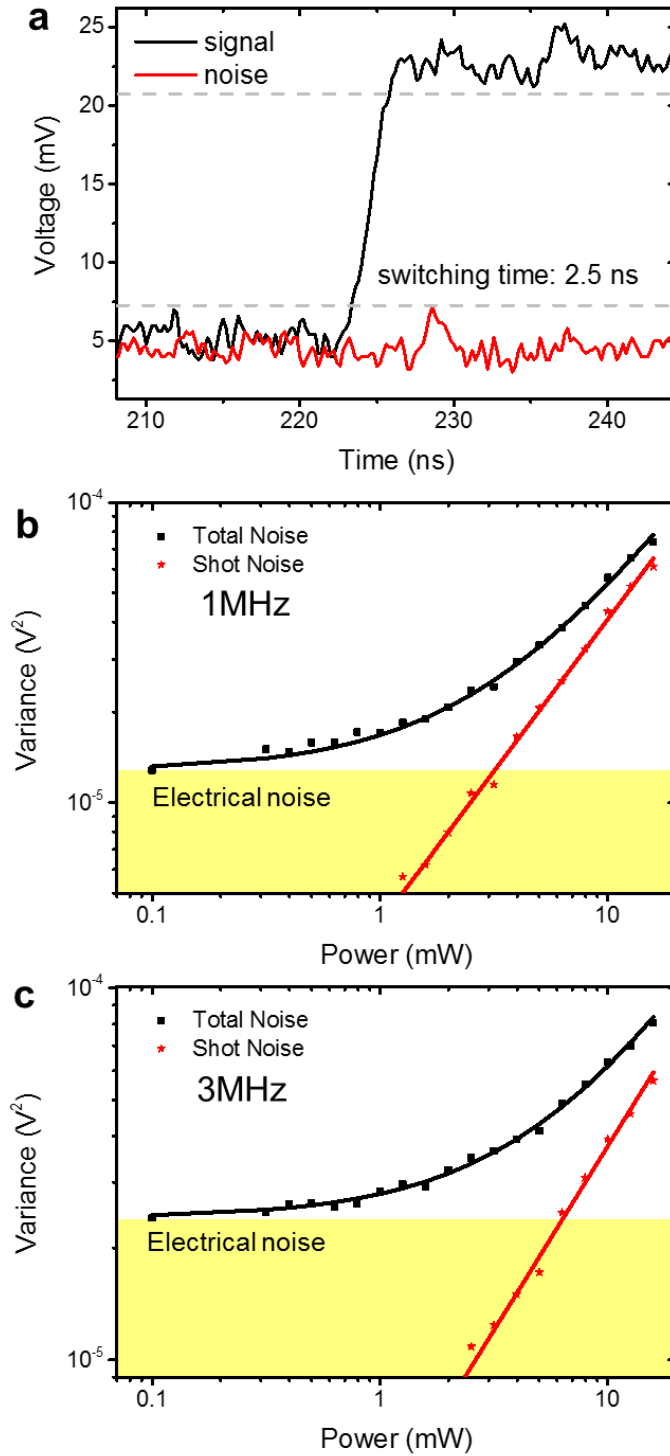


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 3 **Figure 1 | Schematics of the CV-QKD system.** The system built on silicon photonic
 4 chips contains two parties, Alice and Bob, which are used as the transmitter and receiver.
 5 Alice side consists of several amplitude modulators (AM), phase modulators (PM),
 6 attenuators and grating couplers, which can modulate the signal (S) and multiplex signal
 7 with the local oscillator (LO) in two orthogonal polarization states. Bob demultiplexes and
 8 detects the signal with the receiver chip.

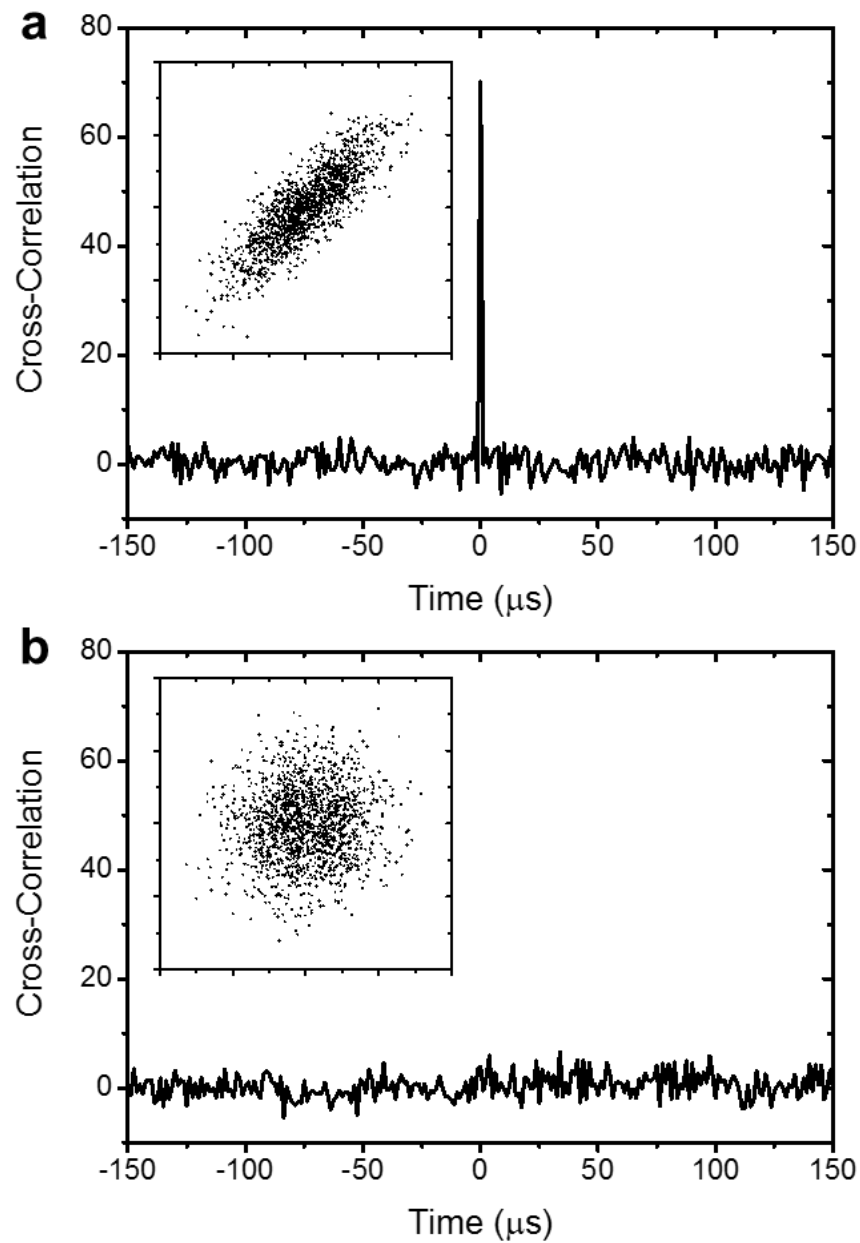


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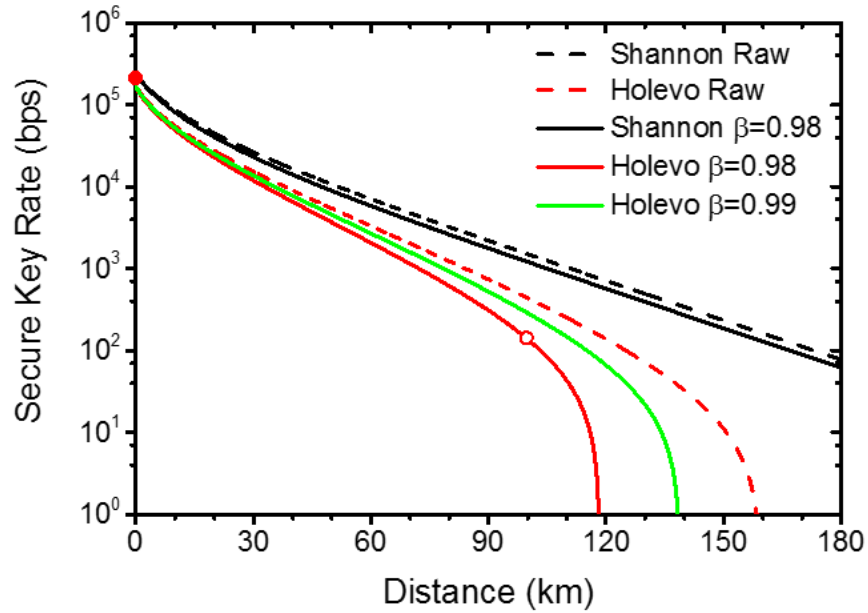
2 **Figure 2 | SEM and microscopic photos of the QKD chip.** (a) SEM of part of the
 3 amplitude modulator structure, including the p-i-n phase shifter and directional couplers.
 4 (b) QKD chip packaging with PCB board. (c) Microscopic photo of the on-chip homodyne
 5 detector, which is also the receiver chip. The signal from two photodiodes (PD) is
 6 subtracted and amplified. (d) Enlarged microscopic photo of the on-chip germanium PD.



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 2 **Figure 3 | Chip performance analysis.** (a) Switching speed of the modulator. (b) Total
 3 noise variance and fitted shot noise for the homodyne detector with different input LO
 4 power level at the 1 MHz band and (c) 3 MHz band.



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 2 **Figure 4 | Key distribution test.** Cross-correlation result of Bob's measurement result
 3 and Alice's modulation on (a) corresponding quadrature (b) different quadrature. The inset
 4 shows the correlated gaussian key in two different situations.



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2 **Figure 5 | Secure Key rate analysis.** The secure key rate under individual attack (black
 3 line) and collective attack (red line). Considering a practical case, the reconciliation
 4 efficiency of 0.98 and 0.99 is used to calculate the effective key rate after the reconciliation
 5 process. The solid dot near 0 km represents the experimental key rate with a 2-m fiber link,
 6 while the circle at 100 km represents the simulated key rate with a high-efficiency
 7 reconciliation protocol.

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