

1 **A novel metal organic framework (MOF) - mediated interfacial polymerization for**
2 **direct deposition of polyamide layer on ceramic substrates for nanofiltration**

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21 Keywords: reactive-seeded growth, MOF-mediated, interfacial polymerization, organic-
22 inorganic composites

23
24 Abstract

25 A facile metal-organic framework (MOF)-mediated interfacial polymerization (IP) method has
26 been developed to prepare a polyamide (PA) layer directly on the ceramic substrate for
27 nanofiltration. MOF was introduced to connect ceramic substrate and PA layer via chemical
28 bonding, resulting in a robust separation layer. The optimization of IP could be controlled by
29 MOF growth process via tuning the surface roughness as well as hydrophilicity. This method
30 would provide a new way for the preparation of next generation of organic-inorganic composite
31 membranes.

32 Ceramic membranes have drawn increasing attention due to their excellent chemical
33 and physical properties. Meanwhile, they have been considered as an attractive alternative to
34 polymer membranes when considering the social sustainability^[1,2]. However, the limitation on
35 selectivity for ceramic membranes results in their application restricted to microfiltration and
36 ultrafiltration^[3]. It is still a challenge to fabricate a robust ceramic membrane for nanofiltration
37^[4,5].

38 On the other hand, polyamide (PA) membrane, which could be formed via interfacial
39 polymerization (IP), has shown high stability and selectivity in reverse osmosis^[6,7]. Up to now,
40 lots of work have been finished to fabricate a PA selective layer on polymeric support for water
41 treatment^[8-11]. However, limited studies have been focused on preparing thin selective layers
42 via IP on porous ceramic substrates^[12,13], which might be caused by the relatively rough surface
43 of ceramic membranes as well as the weak interaction between organics and inorganics.
44 Generally, an inter-grown polymeric intermediate layer would be needed to facilitate the IP
45 fabrication on ceramic substrates^[12,14]. However, the weak physical connection between the
46 substrate and the selective layer makes the membrane not stable nor robust, especially in high
47 pressure filtration system, like nanofiltration. It would be a great opportunity to grow a robust
48 PA layer on ceramic substrate as the next-generation composite membrane for the high-pressure
49 filtration application.

50 When organic-inorganic composites were taken into account, metal-organic
51 frameworks (MOFs) is surely to be one good example in which organic and inorganic structures
52 are well-connected^[15]. MOFs are usually synthesized by combining a hydrated metal salt and
53 organic linker using hydrothermal or solvothermal method^[16]. Therefore, it is possible to link
54 the MOF layer and the ceramic substrate by chemical reaction followed by PA layer formation
55 via IP.

56 Our hypothesis for this work is to synthesize a robust PA selective layer on Al₂O₃
57 ceramic substrates via chemical bonding. It could be achieved by direct IP process with the

58 assistance of a well-known Al-based MOF structure MIL-53 (Al) ($\text{Al}(\text{OH})(\text{C}_6\text{H}_4(\text{COO})_2)$) as
59 the intermediate connection layer (**Figure 1**). The chemical bonding between MIL-53 and PA
60 layer could be formed via hydrogen bond and dehydration condensation (**Figure S2**). The
61 chemical connection of the composite membrane was investigated and the membrane
62 performance (pure water flux and rejection) was tested. This method would provide a new idea
63 to make organic-inorganic composite membranes for water treatment.

64 To investigate the MIL-53 growth mechanism, the particles prepared at different
65 hydrothermal hours were collected and characterized. XRD patterns (**Figure S4**) show that at
66 the seed growth stage (Stage I), the organic linker could be re-crystalized and is identified as
67 H₂BDC ($\text{C}_8\text{H}_6\text{O}_4$, benzene-1,4-dicarboxylic acid, Entry No. 00-021-1919). At the MIL-53
68 growth stage (Stage II), pure MIL-53 crystals could be generated, all peaks in the XRD patterns
69 can be matched well with the simulated patterns (Entry No. 00-067-0849, **Figure S5**). Even
70 the hydrothermal growth time has no significant effect on the crystal structure, it does affect
71 the morphology and the crystal size of MIL-53 powders observed from FESEM images (**Figure**
72 **S6**).

73 The XRD patterns and FTIR spectra (**Figure 2 g and h**) of M-4 show that MIL-53 layer
74 was successfully formed on Al₂O₃ substrate. Meanwhile, the insignificant signal difference
75 between M-4 and PA/M-4 membrane may indicate an ultrathin PA layer was formed during IP
76 process, which could be further estimated from FESEM image (**Figure S7**). Moreover, the XRD
77 pattern and FTIR spectra of M-4 show that it contains a full MIL-53 phase comparable with the
78 pure MIL-53 powder (**Figure S4**). To further confirm the successful formation of PA layer on
79 MIL-53 surface, the MIL-53 particle instead of MIL-53 membrane was characterized (**Figure**
80 **S8**). The new peak at 19° in XRD patterns can be identified as polyamide and the vibration at
81 2800-2900 cm⁻¹ in FTIR could be caused by CH₂ stretch in polyamide. Furthermore, the XPS
82 wide scan confirmed the existence of N in PA/MIL-53 (Al), evidencing the PA layer formation
83 on MIL-53 (Al) surface.

84 The effect of hydrothermal growth hours of MIL-53 on morphology of M-X was
85 investigated (**Figure 2**). Results showed that the surface morphology as well as hydrophilicity
86 of the substrates can be controlled by tuning the MOF growth process, which can also be
87 verified by previous research ^[17]. The seed particles with small size are evenly distributed on
88 the surface of the support due to the connection between H₂BDC and Al on the substrate surface
89 (**Figure S9**). The initial membrane (M-control) shows a porous surface (**Figure 2a**). The M-2
90 still shows a porous surface and some MIL-53 crystals are observed on the membrane surface
91 (**Figure 2b**). With increasing the hydrothermal time, the crystals grow bigger on the Al₂O₃
92 substrate surface, resulting a less-porous and smoother surface (M-4). However, when the
93 hydrothermal growth time was further increased, the growth of the MIL-53 crystals became
94 random and promoted the formation of irregular shaped crystals (**Figures 2c-f**), producing a
95 much rougher surface (**Figure S10**). The relatively rough surface might be not favorable for the
96 IP process due to the lack of a smooth and continuous surface. Meanwhile, the cross-sections
97 of MIL-53 (Al) membranes show that a high degree of inter-grown MIL-53 layer which is well
98 bonded with the Al₂O₃ substrate was obtained (**Figure S11**). Compared with the MIL-53
99 powders prepared at the same conditions, the morphology on the membrane surface changes
100 due to the energy distribution difference.

101 **Figure 3** shows the surface morphologies of PA/M-X membranes. It is quite difficult to
102 form a PA layer directly on the Al₂O₃ membrane surface (PA/M-control) (**Figure 3a**) because
103 of its large pore size as well as high roughness. While, even the porous surfaces were still
104 observed in M-2 (**Figure 2b**), the PA/M-2 membrane shows a dense surface, indicating that the
105 PA layer formed on the M-2 surface (**Figure 3b**). Similar results can be observed in PA/M-X
106 (X=4, 6 and 8) with increased surface roughness. For M-12, no continuous PA layer could be
107 formed on the surface (PA/M-12) because of the discontinuous interface caused by its high
108 roughness. The results show that the surface roughness is a critical parameter on the PA layer
109 formation in IP process and it could be controlled by the hydrothermal growth time of MIL-53

110 layer. Another reason for the unsuccessful IP process for M-12 might be the hydrophobic
111 surface. The M-X membranes gradually become more hydrophobic with extended MIL-53
112 crystal growth duration. The tested contact angles are 62°, 89°, 107°, 116° and 127° for M-2, M-
113 4, M-6, M-8 and M-12, respectively (**Figure 2**). In a standard IP process, the MPD ($C_6H_8N_2$,
114 *m*-phenylenediamine) solutions could uniformly distributed on the substrate surface and a
115 continuous polyamide could thus be formed at the interface between the aqueous and organic
116 phases ^[18,19]. Nonetheless, MPD tends to aggregate at the M-X membrane surfaces with
117 increasing surface hydrophobicity during the air gun purging process, thus resulting higher
118 possibility of polyamide failures, or more defects are expected during polyamide formation ^[20].

119 As shown in **Figure S12**, the surface roughness decreased from around 450 nm (PA/M-
120 Control) to 340 nm for PA/M-4, which means a smoother polyamide layer was formed on the
121 substrate surface. However, when the hydrothermal time increased from 6 h to 12 h, the surface
122 roughness increased from 431 nm (PA/M-6) to 607 nm (PA/M-12), even higher than the initial
123 one. The results show that the hydrothermal growth time is curial to control the crystal size as
124 well as the surface roughness.

125 The pure water permeability as well as Rhodamine B (molecule weight of 479) rejection
126 were tested in a home-made dead-end membrane filtration system (**Figure S3**). For PA/M-X
127 membranes, the pure water flux decreases from 57 to 1 LMHB with increasing X from 2 to 12
128 h (**Figure 3g**). The water permeability primarily depends on the membrane structure including
129 pore size and membrane thickness as well as the surface hydrophilicity ^[21]. With increasing the
130 hydrothermal growth time, the thickness of MIL-53 layer increases (**Figure S11**)
131 accompanying with the decreasing of pore size, resulting the dramatically decrease of pure
132 water flux (**Figure S13**). Meanwhile, after the formation of PA layer, the flux of PA/M-X
133 membrane were slightly decreased compared with M-X (**Figure 3g**). In the meantime, with the
134 prolonged hydrothermal time, the flux change can be ignored for $X \geq 4$. The results show that
135 the decreased flux was caused by the formation of dense MIL-53 layer on the Al_2O_3 surface.

136 On the other hand, in the rejection experiment, PA/M-4 shows the highest rejection ratio
137 (>99%), while PA/M-12 only shows a 3.5% rejection, meaning the rejection was caused by the
138 PA layer on the surface, which further confirmed the unsuccessful formation of PA layer on M-
139 12. The color changes of RhB in the permeate side is shown in **Figure 3h**. Furthermore, PA/M-
140 4 also shows a rejection rate of 50.3 % and 20.2 % for MgSO₄ and NaCl (**Figure S14**). **The**
141 **long-term test of PA/M-4 was investigated in a 90 min continuous filtration, in which the permeate**
142 **flux decreased dramatically from around 30 to less than 4 LMHB while the rejection for 100**
143 **mg L⁻¹ RhB solution maintained at > 99%. The decrease of flux could be caused by the RhB**
144 **cake layer formation on the membrane surface. The high separation performance was**
145 **comparable with reported study [21], while the chemical bonding in the as-prepared composite**
146 **membrane make it more robust and stable.**

147 To further verify the versatility of this method, another Al-based MOF (MIL-96) was
148 investigated. The preparation is similar compared with the MIL-53 except H₃BTC (**C₉H₆O₆,**
149 **benzene-1,3,5-tricarboxylic acid**) was used as the organic linker instead of H₂BDC and the
150 hydrothermal temperature was set at 210 °C. The results showed the continuous formation of
151 PA layer on the surface could be controlled by the growth of MIL-96 layer (**Figure S15**).
152 Therefore, the idea using MOF as the connected inter-layer would open possibilities for
153 preparation of a thin organic layer onto inorganic substrate. The MOF layer works as a perfect
154 hybrid material to change the pore size and hydrophilicity of the ceramic membrane, forming a
155 surface densified layer and promoting wetting properties for the IP process. Meanwhile, it can
156 form the robust separation layer because of the chemical connection between MOF layer and
157 the substrate. Results showed that the surface roughness which is critical for the IP process
158 could be controlled during the MOF layer growth process. The water permeability was
159 controlled by the formation of MOF layer while the high rejection was enabled by the PA
160 selective layer.

161

162 **Experimental Section**

163 All chemicals used in the experiment are listed in **Text S1**. The schematic of the MOF-
164 mediate IP method is shown in **Figure 1**. To grow a uniform seed layer of MIL-53 (Al), Al₂O₃
165 ceramic substrate instead of Al(NO₃)₃•9H₂O was firstly chosen as the Al source. The sample
166 holder (**Figure S1**), which was used to fix the substrate, was put into the autoclave in which the
167 polished surface was faced up followed by the adding of H₂BDC (0.36 g) and DI water (25 g).
168 The autoclave was heated at 220°C for 12 h for the seed growth, in which the organic linker of
169 H₂BDC would react with Al on the substrate surface to form a uniform and thin seed layer
170 (Stage I). After the seeding growth, MIL-53 layer was grown under the similar condition
171 whereby Al(NO₃)₃•9H₂O (0.82 g) was added as the Al source followed by the addition of 0.18
172 g H₂BDC and 25 g DI water (Stage II). In the MIL-53 growth process, the substrate surface
173 roughness as well as crystal size would be controlled by changing the hydrothermal growth
174 time (2-12 h). After the MOF layer growth, the as-prepared MIL-53/Al₂O₃ membranes were
175 named as M-X, where X represents the growth hours of MIL-53 layer. After the formation of
176 MIL-53 layer on the Al₂O₃ substrate, the M-X membranes were washed with DI water and dried
177 at 100°C overnight for the following IP process. The powders were also collected from the
178 mother solution for the later characterization.

179 During the IP process, M-X membranes were firstly immersed in the as-prepared
180 aqueous phase (2 w.t% MPD in DI water) for 2 min, after removal of the excess aqueous
181 solution on the membrane surface via air gun purging, the wet membranes were immersed in
182 the as-prepared organic phase (0.1 w.t% TMC in *n*-hexane) for 30 s followed by curing at 60°C
183 for 2 min. The resulted membrane was named as PA/M-X, where X indicates the growth time
184 of MIL-53 layer. After the MOF layer growth, the hydroxyl group (-OH) on the MOF surface
185 can react with amine group (-NH) in MPD via hydrogen bond. Meanwhile, the carboxyl group
186 (-COOH) on residual H₂BDC allows covalent functionalization with -NH by a dehydration

187 condensation reaction followed by the polyamide formation on the interface (**Figure S2**). To
188 confirm that the synthesis of PA layer on the MOF-53 (Al) surface, direct IP on MOF-53 (Al)
189 powders was conducted.

190 The as-prepared PA/M-X membranes were characterized (**Text S2**) and the
191 performance was evaluated in a dead-end membrane filtration system (**Text S3**).

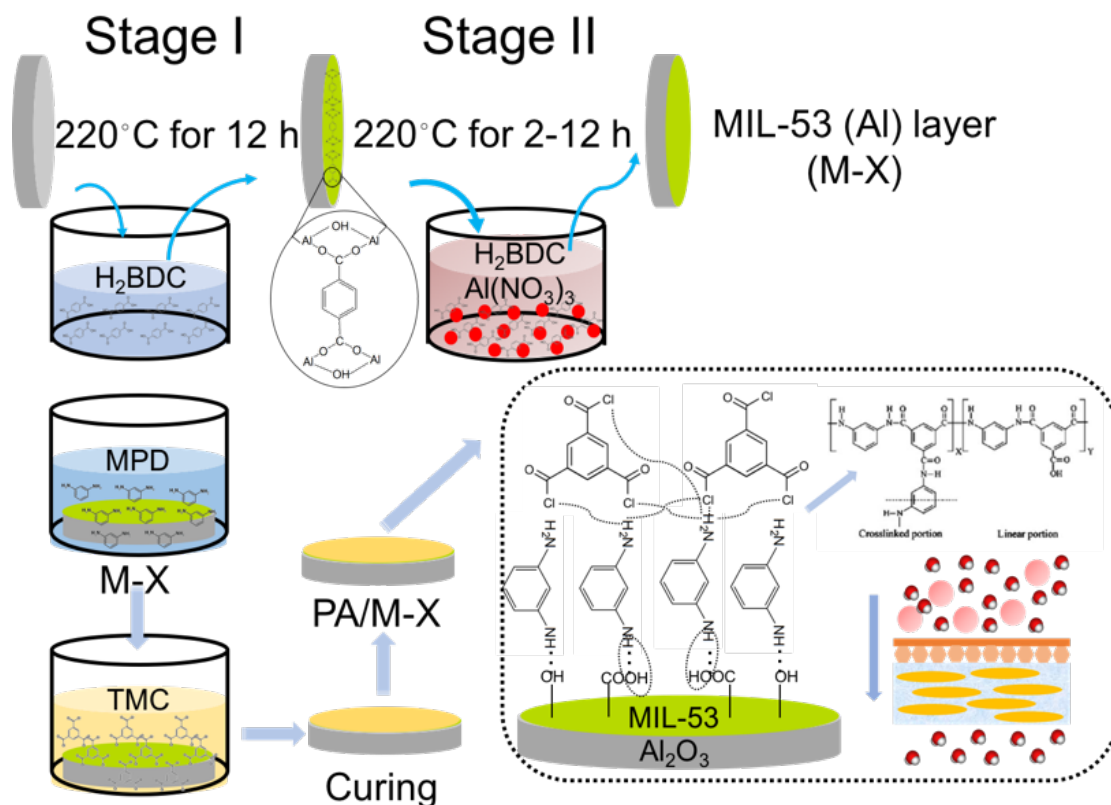
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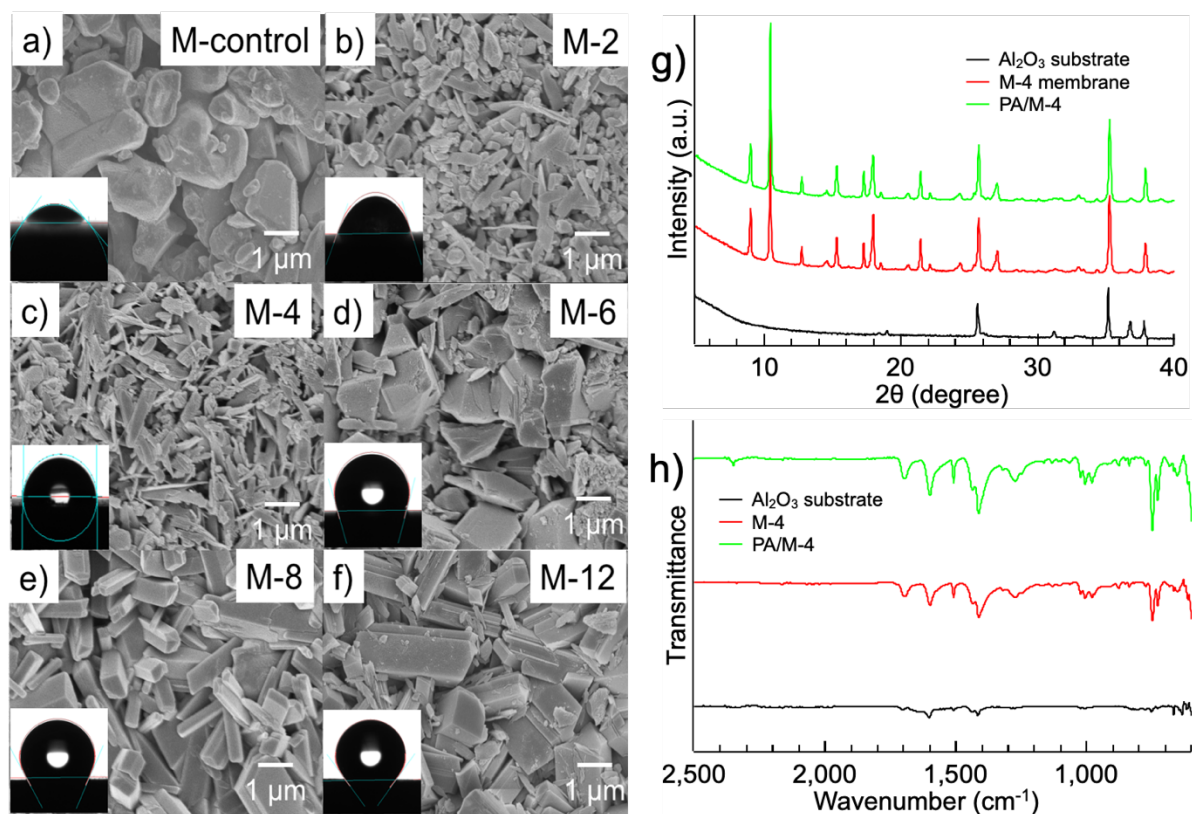
Figure 1. Schematic diagram of preparation of PA layer on Al_2O_3 substrate via a MOF-

233 mediated IP method (X = the hydrothermal growth hours). M-X means MOF membrane at X

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h and PA/M-X means PA layer on MOF membrane at X h.

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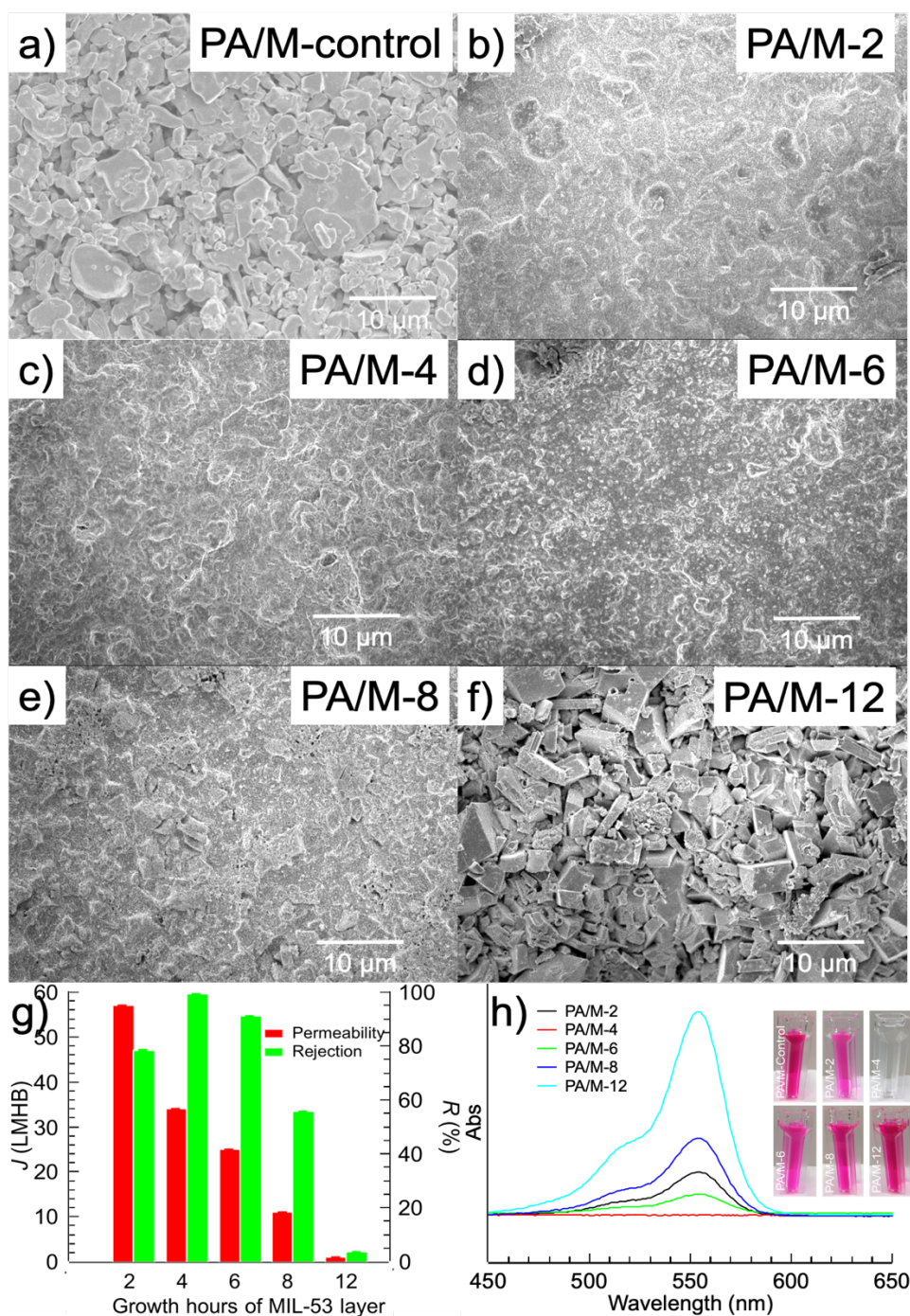


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237 **Figure 2.** Characterization of M-X and PA/M-X membranes. (a-f, FESEM images of MIL-53238 (Al) membranes (M-X); g) XRD patterns and h) FTIR spectra of the Al₂O₃ substrate, M-4 and

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PA/M-4.



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241 **Figure 3.** Characterization and performance evaluation of PA/M-X membranes (a-f, FESEM

242 images of PA/MIL-53 (Al) membranes (PA/M-X); g, Pure water permeability and RhB

243 rejections of PA/M-X; h, UV-Vis absorption spectra of permeate treated with different

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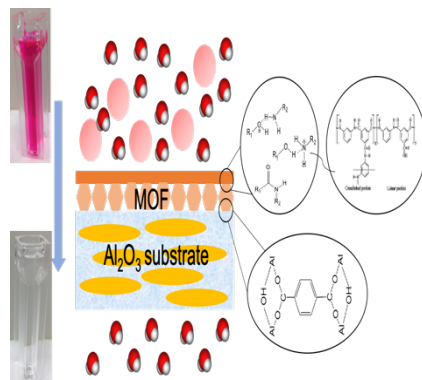
membranes.

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 249 **A novel metal organic framework (MOF) - mediated interfacial polymerization for direct**
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254 Supporting Information

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256257 **A novel metal organic framework (MOF) - mediated interfacial polymerization for**
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263 **Text S1.** The details on materials used in the experiment.

264 Aluminum nitrate nonahydrate ($\text{Al}(\text{NO}_3)_3 \cdot 9\text{H}_2\text{O}$), benzene-1,4-dicarboxylic acid
265 ($\text{C}_8\text{H}_6\text{O}_4$, H_2BDC), benzene-1,3,5-tricarboxylic acid ($\text{C}_9\text{H}_6\text{O}_6$, H_3BTC), powder Al_2O_3 (100
266 mesh, 99%), *m*-phenylenediamine ($\text{C}_6\text{H}_8\text{N}_2$, MPD), trimesoyl chloride ($\text{C}_9\text{H}_3\text{O}_3\text{Cl}_3$, TMC), *n*-
267 hexane and Rhodamine B ($\text{C}_{28}\text{H}_{31}\text{ClN}_2\text{O}_3$) were purchased from Sigma-Aldrich. Sodium
268 chloride (NaCl) and magnesium sulfate (MgSO_4) were from Merck. All chemicals were of
269 reagent grade or higher and were used without further purification. All solutions were prepared
270 in deionized (DI) water (18.2 $\text{M}\Omega\cdot\text{cm}$ at 25°C) from a Milli-Q purification system.

271 Porous Al_2O_3 ceramic substrates used in the experiments were provided by Nanjing
272 Shuyihui Scientific Instruments CO., LTD (Nanjing, China). The substrates are disc-shaped
273 with a pore size of ~100 nm. The diameter of the substrate is 22 mm and the thickness is 2 mm.
274 One side of the ceramic substrate was polished by SiC sandpaper and washed with DI water
275 before being used for the growth of MOF layer.

276

277 **Text S2.** Characterization techniques.

278 A field emission scanning electron microscope (FESEM, JSM-7600F, JEOL) was used
279 for the evaluation of membrane morphology and the membrane surface roughness was
280 measured by atomic force microscopy (AFM, Cypher S, Asylum Research). The vibrational
281 absorbance and structural characteristics of as-prepared composites were investigated by
282 Fourier transformed infra-red spectrometer (FTIR, Perkin Elmer). The mineralogy and crystal

283 structures of composites were analysed using X-rays diffractometer (XRD, Bruker D8
284 Advance) with a monochromatic high intensity Cu-K α ($\lambda = 1.54 \text{ \AA}$) radiation over a 2θ range of
285 $5\text{-}40^\circ$ at a step size of 0.02 combined with a rotation speed of 15 rpm. The chemical bonding
286 analysis was conducted by X-ray photoelectron spectroscopy (XPS) on a Kratos Axis Supra
287 spectrophotometer (Shimadzu) equipped with a dual anode monochromatic K α excitation
288 source ($h\nu = 1486.7 \text{ eV}$).

289

290 **Text S3.** The details for home-made membrane filtration tests.

291 The membrane filtration tests are conducted in a home-made dead-end membrane
292 filtration system (shown as **Figure S3**). The transmembrane pressures (TMP) in clean water
293 permeate flux experiments were varied in the range of 1-10 bar. The mass of permeate was
294 measured and converted to permeate flux according to the **Equation. S1**.

$$295 \quad J = V / A t \quad (\text{S1})$$

296 where J represents permeate flux (LMH, $\text{Lm}^{-2} \text{ h}^{-1}$), V is volume of permeate (L), A is effective
297 membrane surface area (m^2), t represents the filtration time (h), ΔP means the transmembrane
298 pressure (TMP, Pa)

299 In the rejection test, the applied trans-membrane pressure is 10 bar and the feed (RhB,
300 MgSO_4 and NaCl) concentration is 100 mg L^{-1} . The stabilization time is 2 hours before
301 sampling. And the concentration of RhB, MgSO_4 and NaCl in the permeate side was determined
302 by UV-1800 spectrophotometer (Shimadzu, Japan) and conductivity meter (Myron L).

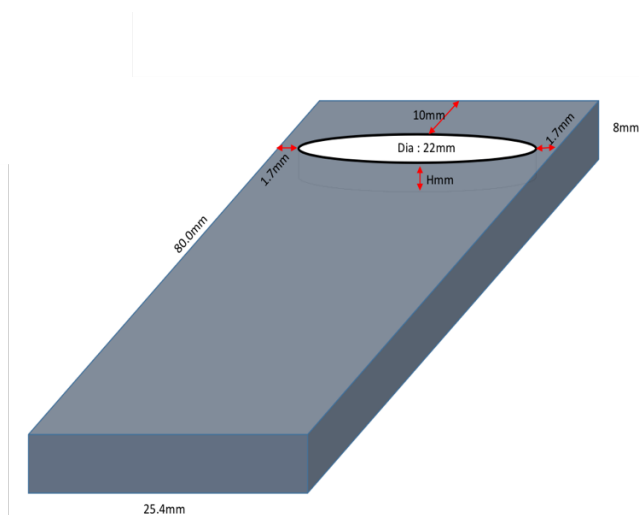
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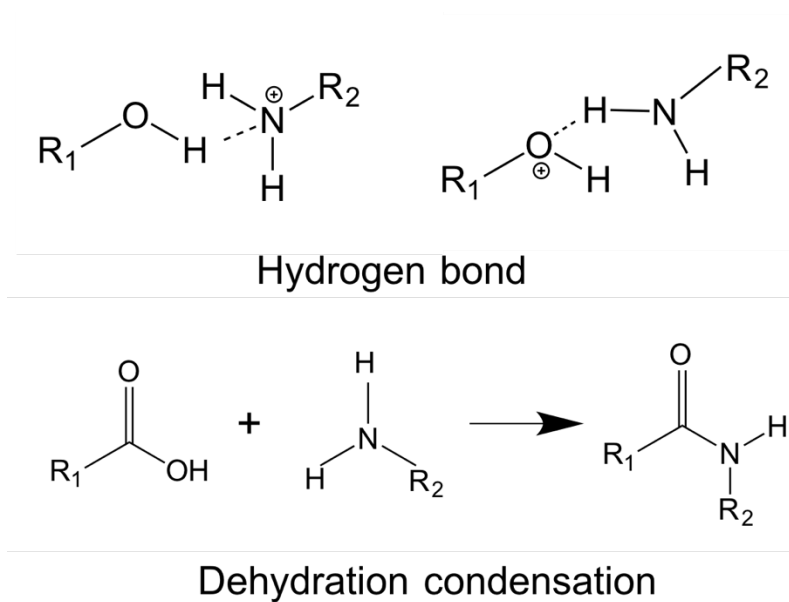


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Figure S1. The sample holder of ceramic substrates for seed growth.

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Figure S2. The chemical reactions between -OH/-COOH in MIL-53 (Al) and -NH₂ in MPD

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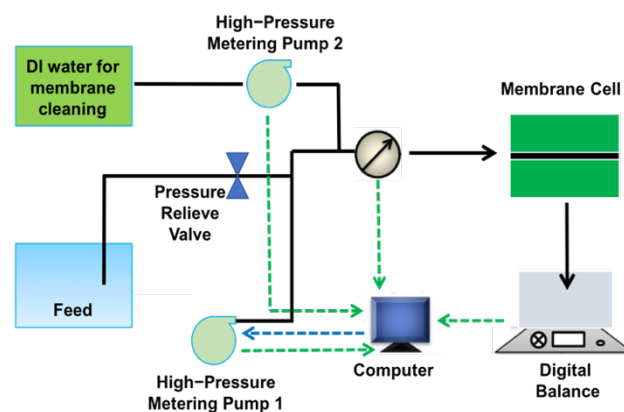
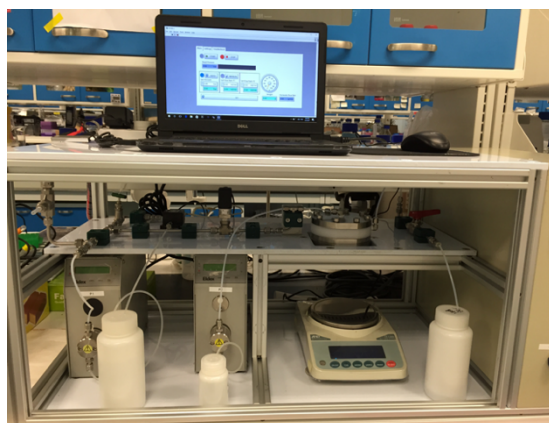
via hydrogen bond and dehydration condensation.

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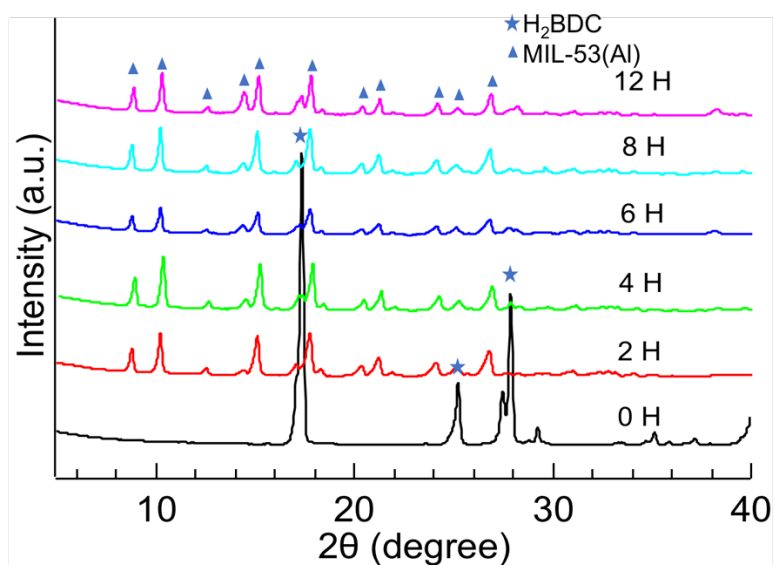
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Figure S3. The home-made membrane filtration system.

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Figure S4. XRD patterns of as-prepared MIL-53 particles with different hydrothermal hours.

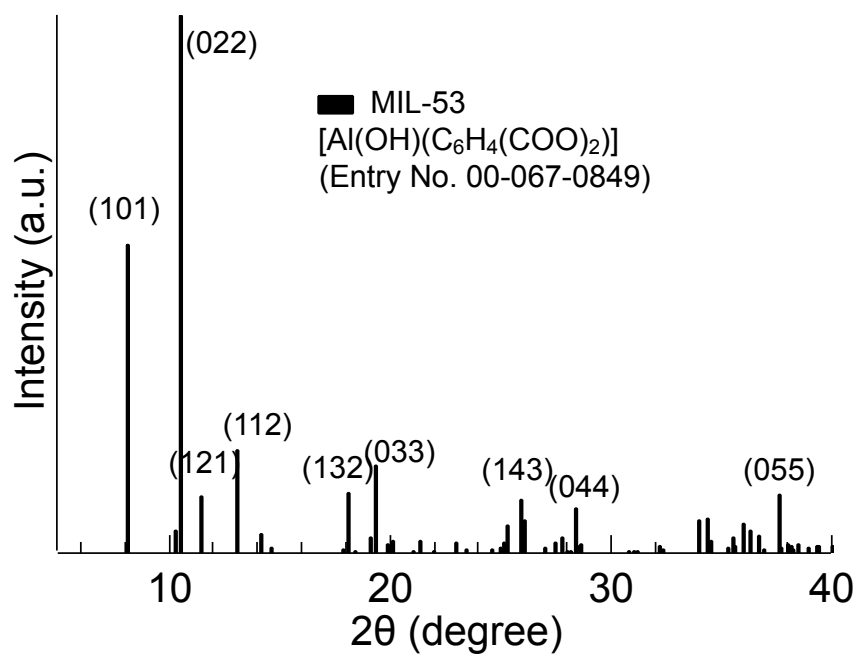
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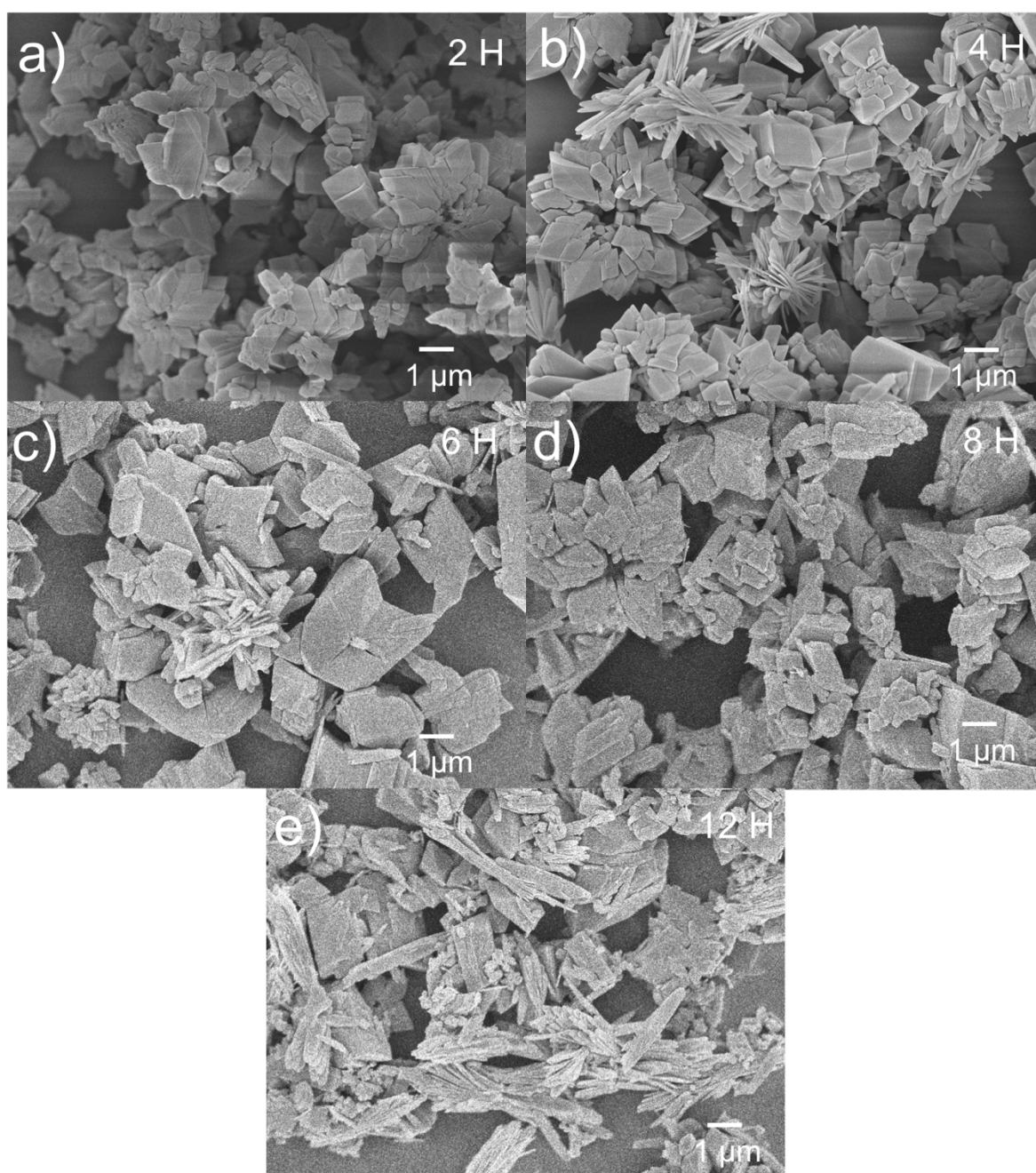
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Figure S5. The simulated XRD patterns for MIL-53 (Al).

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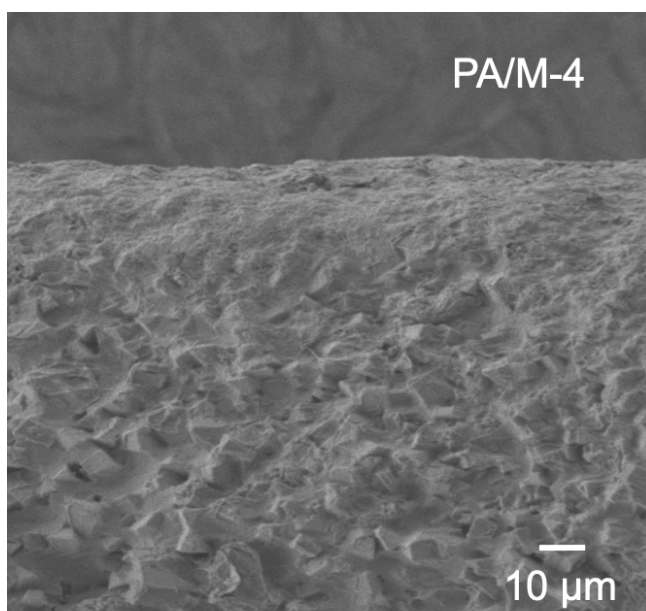
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Figure S6. FESEM of MIL-53 powders prepared under different hydrothermal hours
(2 h-12 h).



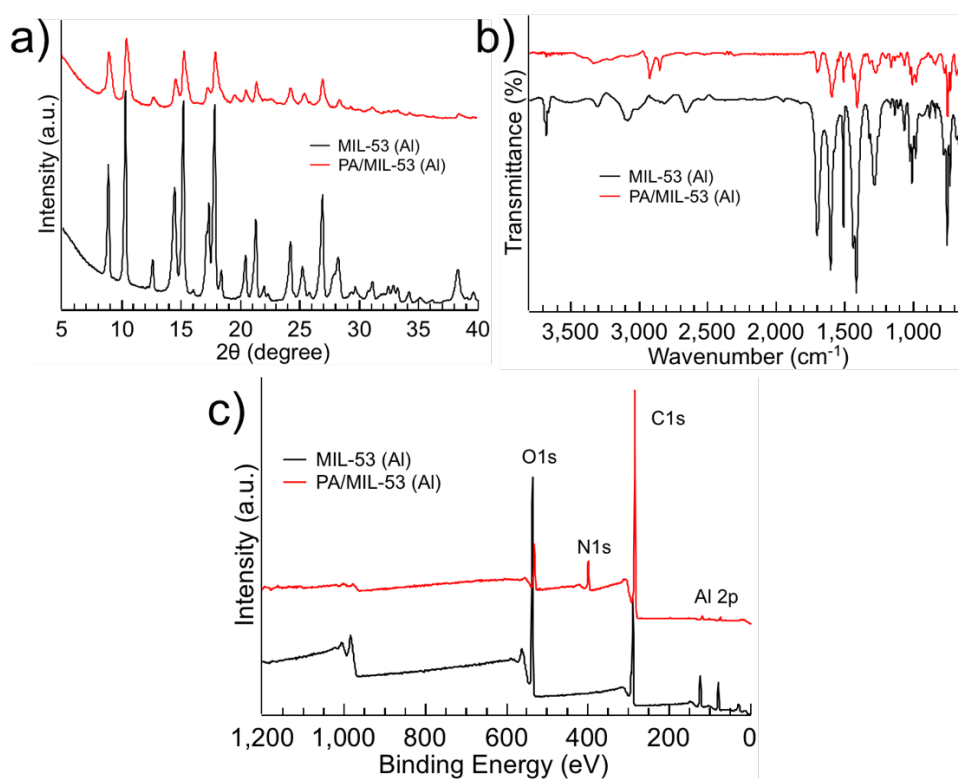
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Figure S7. FESEM image of cross sections of PA/M-4.

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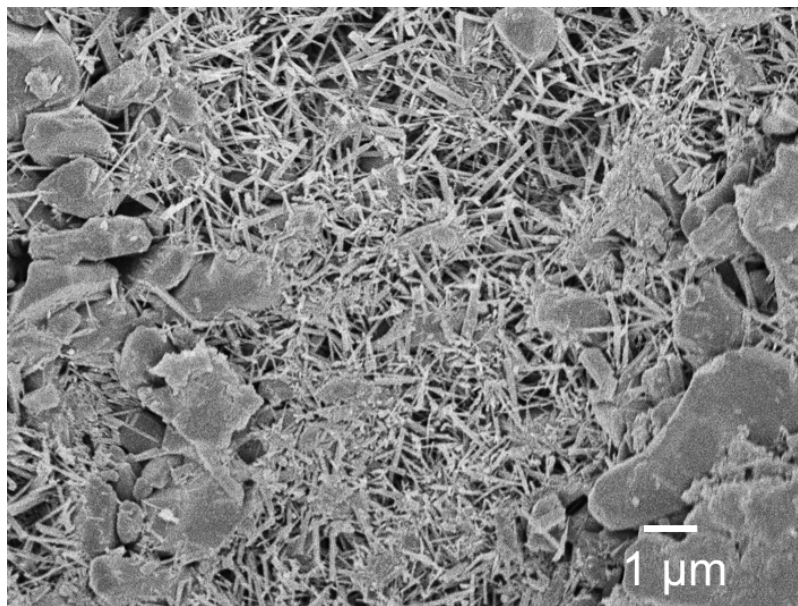
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Figure S8. XRD patterns (a), FTIR spectra (b) and XPS wide scan (c) of MIL-53

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powder (prepared at 12 h) and PA/MIL-53.



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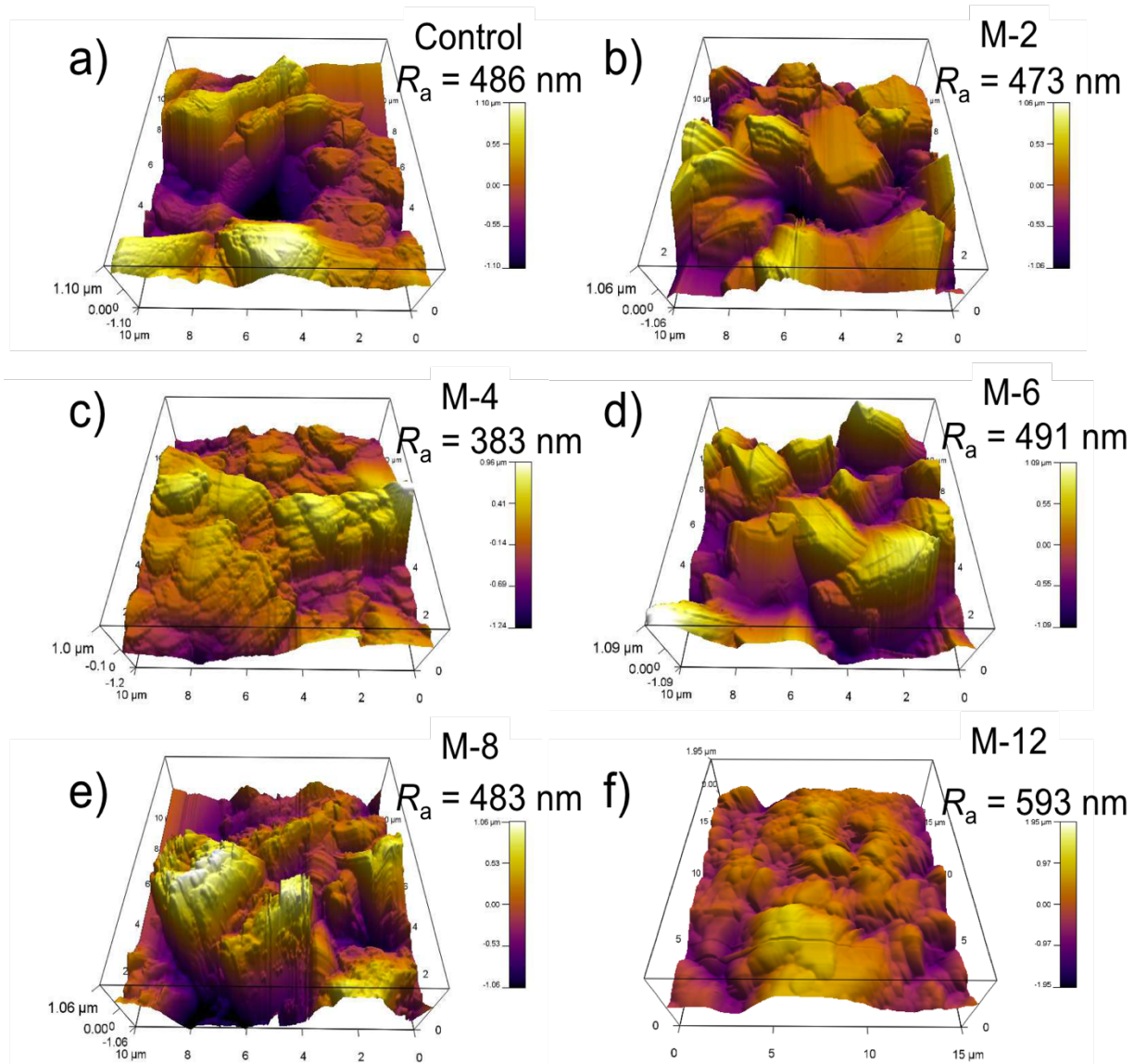
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Figure S9. FESEM of seed layer on the Al_2O_3 surface.

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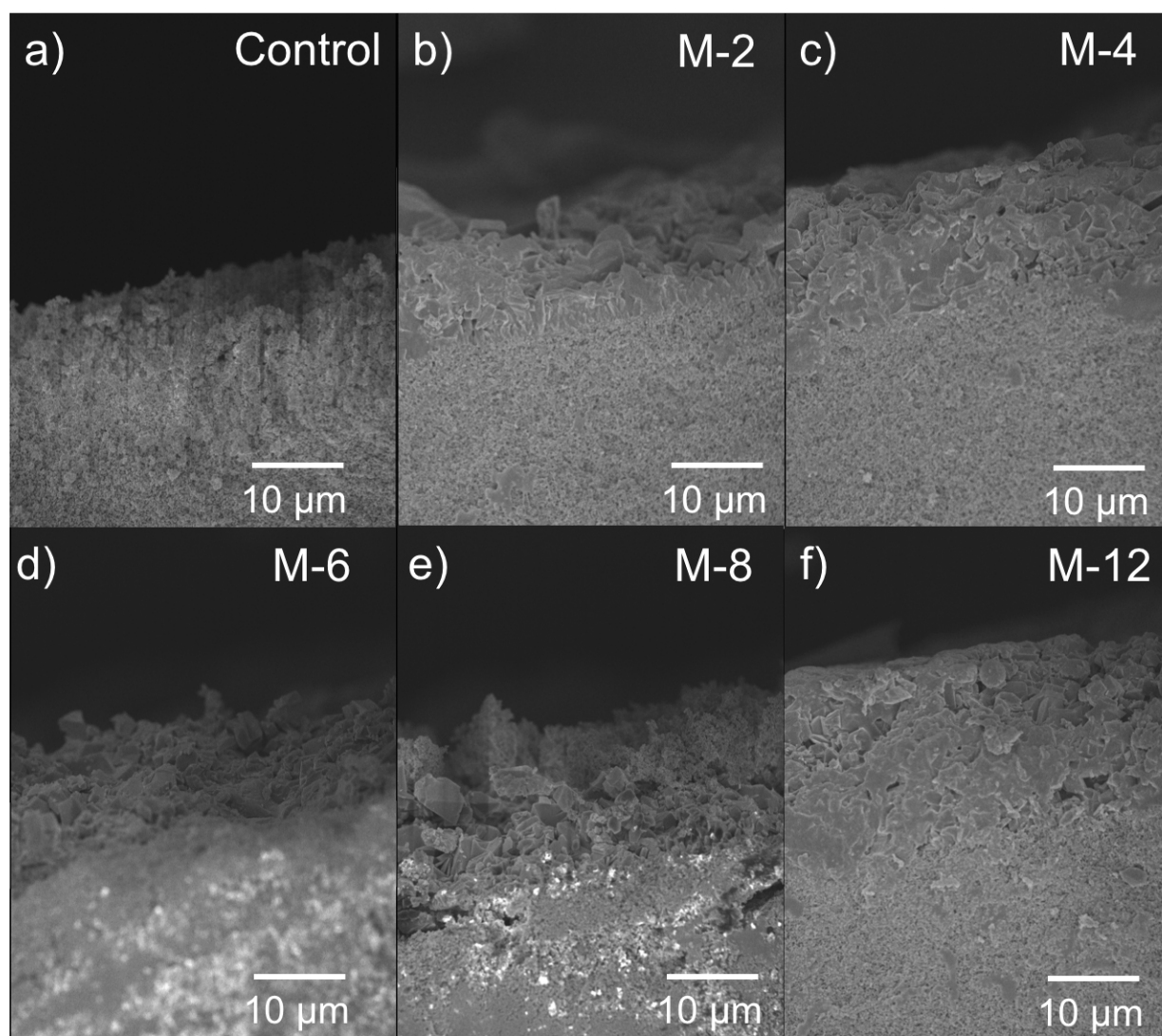
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Figure S10. AFM of M-X prepared with different hydrothermal hours (X=2, 4, 6, 8

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and 12).

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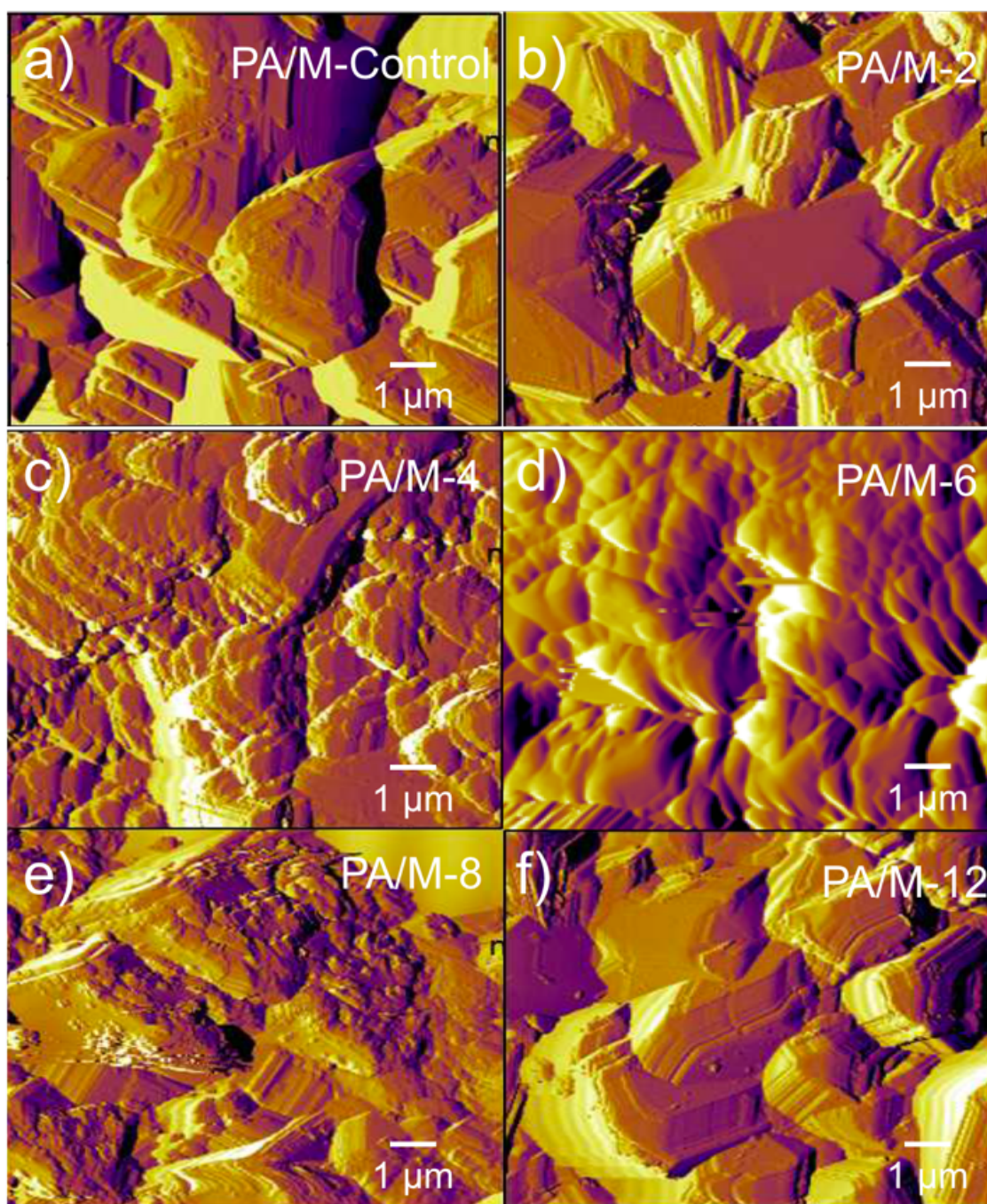
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Figure S11. FESEM images of cross sections of M-X prepared with different hydrothermal hours (X=2, 4, 6, 8 and 12).



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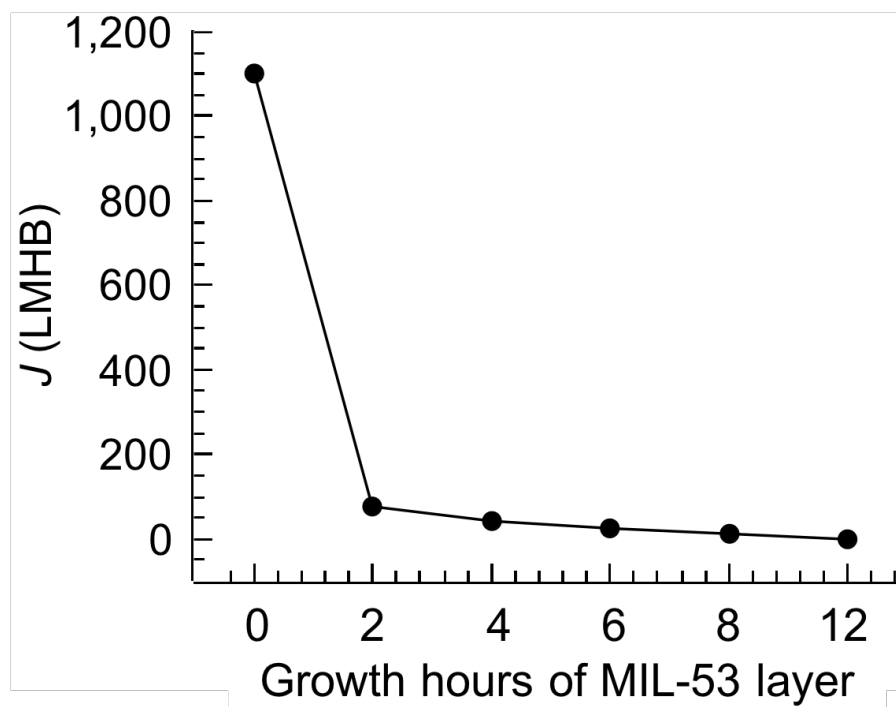
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Figure S12. AFM images of PA/M-X (X means the growth hours).



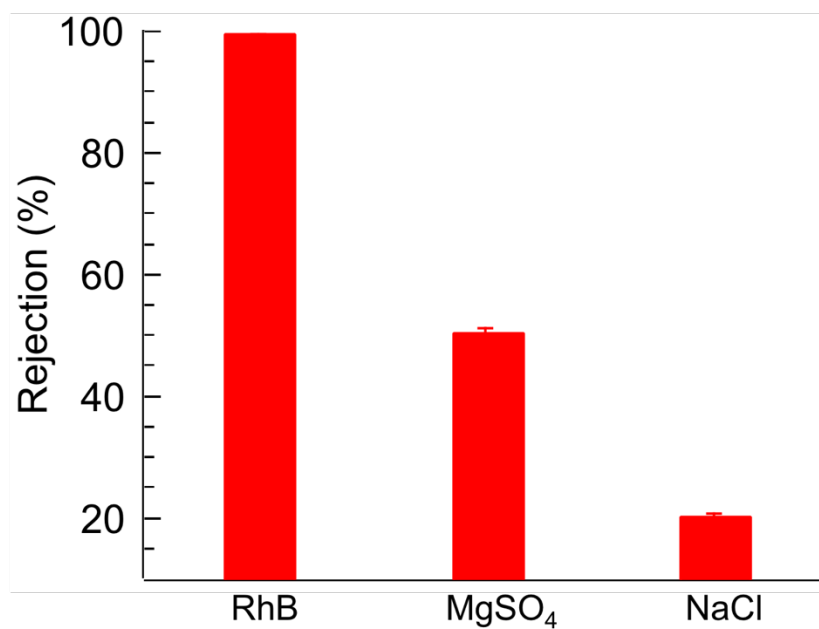
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Figure S13. Pure water flux of M-X (X means the growth hours).

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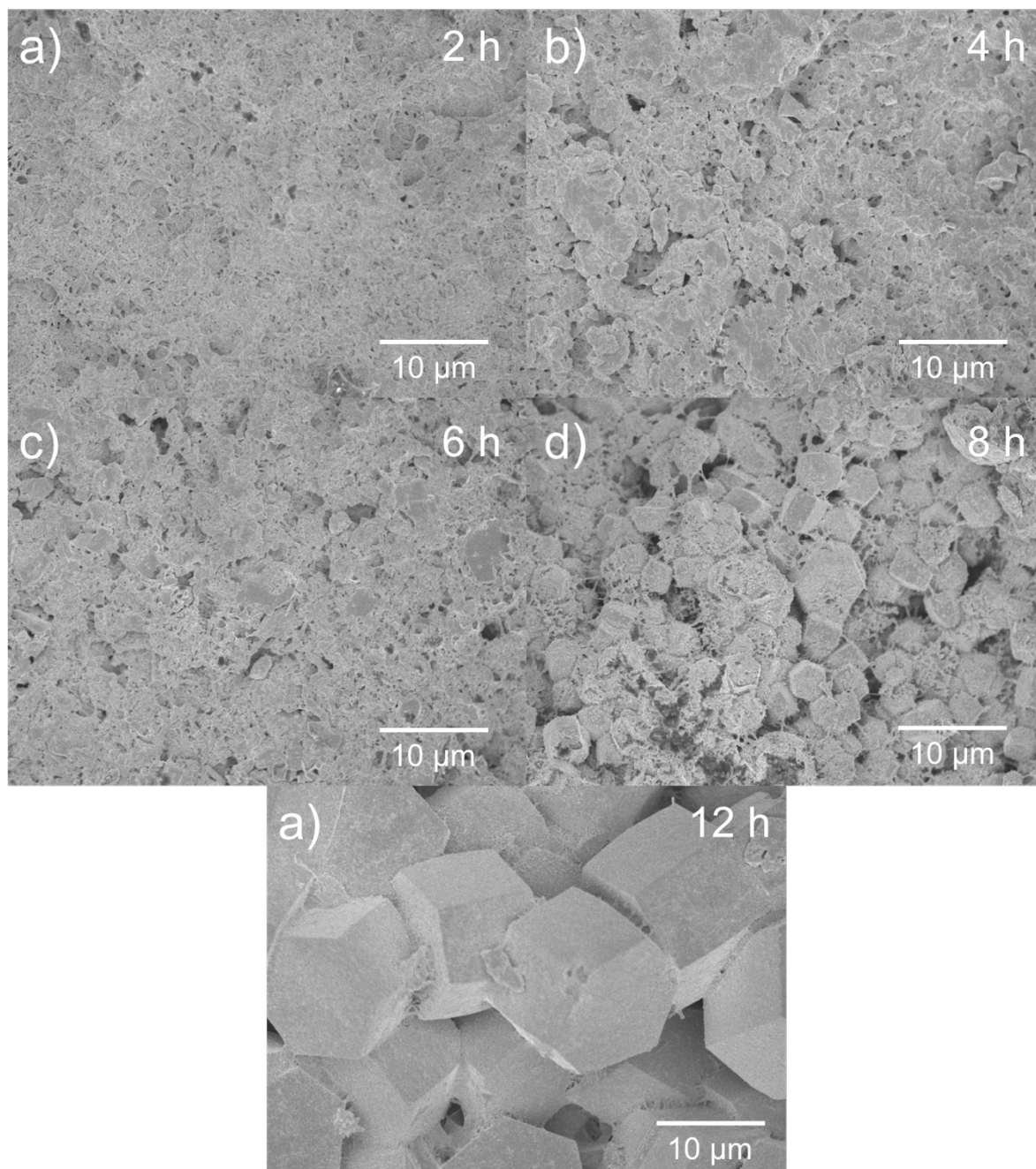
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Figure S14. The rejection on different feed solution for PA/M-4.



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Figure S15. FESEM images of polyamide layer on MIL-93 modified ceramic substrates with different hydrothermal hours (X=2, 4, 6, 8 and 12).