

Towards the Generalization of Membrane Structure-Property Relationship of Polyimides and Copolyimides: A Group Contribution Study

Sadiye Velioğlu^a, S. Birgül Tantekin-Ersolmaz^b, Jia Wei Chew^{a,c,*}

^a School of Chemical and Biomedical Engineering, Nanyang Technological University, Singapore, 637459, Singapore

^b Istanbul Technical University, Dept. of Chemical Engineering, Maslak 34469, Istanbul, Turkey

^c Singapore Membrane Technology Centre, Nanyang Environment and Water Research Institute, Nanyang Technological University, Singapore 637141, Singapore

*Corresponding author, e-mail: jchew@ntu.edu.sg

Abstract

While polymeric membranes are conventional for gas separation processes, significant improvements remain possible and thereby the search for novel polymers is still on-going. The present study provides a way to develop structure-property relationship for polyimides and copolyimides, in order to lead new experimental studies with respect to recommendations on tunable monomers with promising transport properties for specific applications. This method advances the group contribution study based on molar volume contributions of subunits proposed by Robeson et al. [1] for the prediction of He, H₂, O₂, N₂, CO₂ and CH₄ permeability parameters and O₂/N₂, CO₂/CH₄, H₂/CO₂, H₂/CH₄, CO₂/N₂, and He/N₂ perm-selectivities of 490 polyimide and copolyimide structures. The database is screened to identify the high-performing subunits among the 107 considered, then the defined permeability contributions and volume ratios of such subunits are used to predict the gas separation performance (i.e., selectivity and permeability) of the resulting copolyimides. Firstly, the results indicate enhanced agreement between experimental and predicted transport properties, presumably due to the division of the polymer structure into large subunits, the definition of volume quantities of subunits, the expanded database and the consideration of a specific polymer class (namely, polyimides and copolyimides). Secondly, the CO₂/N₂ and He/N₂ gas separation properties cannot be further improved beyond the selectivity-permeability trade-off bound even with a judicious coupling of high-performing subunits, but separations of other gas pairs can exceed the existing upper bound by the incorporation of subunits with sulphone or side methyl groups, used as precursors of thermally rearranged polymers, or with spiro-centered or bridged bicyclic features. One of the key contributions of this study is the recommendation for the synthesis of the polymers

represented by the predicted data points above the trade-off bounds to further enhance gas separations.

Keywords: *Membrane-based gas separation; Copolyimide; Permeability and selectivity; Volume-based group contribution method; Structure–property relationship.*

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1. Introduction

Due to the advantages of membrane-based separation processes such as lower capital, operation and maintenance costs, smaller environmental footprint and ease of process integration compared to the traditional separation techniques, there is growing interests in the membrane-based purification of commercially relevant gases. However, at present, material performance is a key bottleneck, limiting the widespread implementation of membrane processes for gas separation in the industry [2-7]. Therefore, in the last decade, efforts dedicated towards developing superior polymeric membranes that enable high permeability and selectivity, as well as good mechanical and thermal resistance, have escalated. Unfortunately, customizing all these interconnected and occasionally counteracting properties simultaneously is incredibly challenging and time-consuming experimentally, which necessitates tools that allows for the determination of structure-property relationships and enables rapid screening of a large number of polymeric structures.

Polyimides, and the associated high-performance aromatic polymers, have emerged as prominent membrane materials for industrial gas separation processes [7-9]. Such polymers are superior to other polymers for three primary reasons: (i) exhibit structural rigidity and high glass transition temperature, hence offer desirable physical properties under the typical operation conditions of membrane separation processes; (ii) high separation performance approaching towards the upper limit of the permeability-selectivity trade-off relationships for many gas pairs; and (iii) it is possible to modify the performance of such polymers by engineering slight modifications in their chemical structures. Regarding (iii), unfortunately, a small chemical change may result in significant, often unexpected, and not necessarily advantageous alterations. For instance, polyimides constituted from the 6FDA dianhydride and pDiMPD, mTrMPD and pTeMPD diamines display carbon dioxide (CO₂) permeability of approximately 40, 550 and 450 Barrer, respectively [10-14], which clearly indicates the sensitivity of the performance to the constituent groups. In particular, the only difference leading to the order-of-magnitude difference in permeability is merely the number of methyl side groups attached to the benzene ring in the diamine structure. Correspondingly, the development of structure-property relationships for polyimides is crucial to enable the ability to predict permeability and selectivity from polymeric structural units, and provide guidelines for designing optimized membrane candidates with desirable end-use properties. Towards this end, the group contribution method has become a prominent tool for the fast screening of possible compositions, especially in the design of novel polyimides or monomers, or the selection of the continuous phase for mixed-matrix membranes [1, 15-19]. The relationship between the parameters adopted in the method and

the separation properties of the resulting polymeric membrane is of great interest towards the aim of enhancing predictive capability.

Copolyimides allows for the optimization of the separation properties by the coupling of two different polyimides with different permeability and selectivity properties. This provides an opportunity for the synthesis of novel polymers with desired properties. Considering the structural complexity of the copolyimides, the experimental analysis of the separation properties of all the copolyimide structures to identify the best one is a tedious and time-consuming task. Fortunately, using the group contribution method, hundreds of different copolyimide structures made up by combining monomers that have not been coupled before can be evaluated to identify suitable pairs that can exceed the selectivity-permeability trade-off bound for different gas separations. Considerable progress has been made in the modeling of the transport properties of glassy polymers of various structures since the first in 1986 [20]. A well-established approach was set up by Robeson et al. [1, 18] for permeability predictions of aromatic polymers based on the molar volume (instead of empirical factors [15]) as a normalization parameter and the permeability contribution of each subunit. Subsequently, Alentiev et al. [16] proposed the use of larger subunits and molar fraction (rather than molar volume) that reduced the error in the predictions for polyimides. Velioglu and Tantekin-Ersolmaz [17] extended the method of Alentiev et al. [16] to copolyimides and further improved on the accuracy by accounting for the ratio between the pairs of dianhydride or diamine. Later, Ryzhikh et al. [19] used the bond contribution method for permeability and diffusivity predictions using a large database of polymers, obtaining more accurate predictions than their earlier work based on modified atomic contributions. Although group contribution predictions for a range of polymer types has been reported, a focus on polyimides and copolyimides is needed in view of the prominent applications in gas separations. Accordingly, based on the group contribution method, the present study attempts to screen through monomers available in literature to identify the high-performing ones, then combine them into new copolyimides with potentially superior separation properties. This would provide insights towards the understanding and also synthesis of new structures to enhance gas separation.

In this study, we focus on advancing the development of the incremental group contribution method of Robeson et al. [1] for the prediction of the gas transport parameters of polyimides and copolyimides. Specifically, the group contribution method of Robeson et al. [1] is revisited using a much enlarged set of structures with larger sub-units (dianhydrides and diamines) to predict the permeability of helium (He), hydrogen (H₂), oxygen (O₂), nitrogen (N₂), carbon dioxide (CO₂) and methane (CH₄), and the selectivity of gas pairs O₂/N₂, CO₂/CH₄, H₂/CO₂, H₂/CH₄, CO₂/N₂, and

He/N₂. The objective is twofold: (i) prove the applicability and the effectiveness of this new approach in getting the representative parameters for dianhydrides and diamines; and (ii) assess the possibility of exceeding the upper bound limit based on the trade-off between selectivity and permeability via the judicious choice of monomer combinations. In doing this, we will take advantage of molecular simulations in the calculation of molar volumes of the subunits.

2. Group Contribution Method

The group contribution studies differ insofar as whether they consider van der Waals volume or molecular mass of the elements in the parameter predictions. Group contribution methods are generated based on three assumptions. Firstly, the structure of the polymer is divided into several representative subunits that collectively yield the property of the polymer. Secondly, the properties of the subunits are presumed constant for all polymeric structures. Finally, the polymeric properties are accounted for as a sum of the corresponding subunits factored with the adopted weight factors, such as, volume, molar, etc. [2].

The development of efficacious methods for predicting the transport properties of polymeric membranes is of paramount importance to facilitate the development of high-performance membranes. The group contribution method proposed by Robeson et al. [1, 18] for several types of aromatic polymers is one such method which enables quick screenings of a large number of polymer structures. In this study, the group contribution is applied specifically for polyimide and copolyimide membranes.

2.1 Preliminary preparation

We utilize the database available on the website of the Membrane Society of Australasia [21] for polymeric gas separation membranes, and also include recent literature that identifies newly synthesized polyimides. All 490 polyimide and copolyimide structures available are used for the predictions. Three notes are worth indicating. Firstly, to ensure data reliability and compatibility, pure gas permeability data obtained above 10 atm are filtered out specifically for carbon dioxide (CO₂) measurements because the plasticization effect at high pressure is known to increase permeability and decrease selectivity by promoting inter-segmental mobility and fractional free volume (FFV). Secondly, while the compiled database contains primarily the permeability coefficients of polymers measured at 35 °C, minor corrections are made for sources at different temperatures using available correlations for activation energies of glassy polymers [1, 22]. Thirdly,

other classifications associated with the solvent type used in the film preparation, residual solvent amount and membrane preparation are not factored into the data compilation.

The subdivision of the repeat unit of the polymer into subunits or fragments is a basic principle in the group contribution methods. Contrary to the study of Robeson et al. [1] which used short subunits, diamine and dianhydride are proposed as subunits in this study per that in Alentiev et al. [16]. So, each repeat unit of the polyimide is represented by two subunits, namely, a dianhydride and a diamine. Notably, while short subunits may be beneficial in the extrapolation of the method to represent different classes of polymeric structures whose data have not been used in the prediction, greater discrepancies can be expected when expanding the applicability domain. Larger subunits such as dianhydride and diamine, as per the study of Alentiev et al. [16], address this shortcoming, since the chemical bonds are more accurately accounted for in the assembly of the polymer.

2.2 Volume calculation via molecular simulation

The group contribution method of Robeson et al. [1] is revisited using an enlarged set of polymeric structures with a total of 107 subunits (i.e., 32 dianhydrides and 75 diamines). Table 1 lists all 107 subunits, along with the chemical structures, van der Waals volumes, and the gas permeability contributions for He, H₂, O₂, N₂, CO₂ and CH₄. Advances in molecular modeling provide the opportunity to more accurately calculate the thermodynamic properties of the species. In order to define the values of volume fraction (ϕ_i), molecular simulation tools are used to predict molar volume of contributions. Molecular dynamic simulations are carried out using Large-scale Atomic/Molecular Massively Parallel Simulator (LAMMPS) [23]. The minimized subunits are subjected to short runs using isobaric-isothermal ensemble at 1 bar and 35 °C for equilibration whereby all molecular interactions are modeled with the cvff force field [24]. Temperature and pressure are maintained to the targeted value by the Nosé–Hoover thermostat and barostat with a coupling time constant of 100 and 500 fs, respectively. The simulation time step is set to 1 fs. Once the detailed atomistic model of the subunits is constructed, the van der Waals volumes via the Connolly task simulation are calculated directly using the Atom Volumes & Surfaces tool in Discovery Studio 2016 [25], instead of using the Bondi method [26]. Therefore, by using large subunits, all possible atomic interactions in the neighborhood of the monomer are included and thereby highly reliable configurations of the subunits are obtained for a better representation of the subunit volume.

2.3 Matrix preparation and solver

In order to find the permeability contribution of the 107 subunits (i.e., 32 dianhydrides and 75 diamines), whose structures are depicted in Table 1, we first construct a matrix. Notably, while some combinations that can be derived from the present subunits do not have corresponding polyimides reported in the literature, some dianhydrides have been repeatedly used in the preparation of polyimides. The different permeability results reported by several authors for the same polyimide are also included as an extra row into the matrix of the system.

To obtain a set of linear equations in which every row corresponds to a certain polyimide or copolyimide, an explicit form of the equation proposed by Robeson et al. [1] (Eq. 1) is expanded as Eq. 2.

$$\ln P = \sum_{i=1}^n \phi_i \ln P_i \quad (1)$$

$$\ln P_m = \phi_1 \ln M_{1m} + \phi_2 \ln M_{2m} + \dots + \phi_n \ln M_{nm} + \phi_{n+1} \ln N_{1m} + \phi_{n+2} \ln N_{2m} + \dots + \phi_{n+k} \ln N_{km} \quad (2)$$

In Eq. 2, M and N correspond to the specific contributions of the dianhydrides and diamines, respectively; the subscripts n and k represent numbers of dianhydride and diamine used to constitute a polyimide and/or copolyimide, respectively; and P, m, and ϕ stand for permeability of a polymer, investigated gas type, and molar volume ratio of subunit. The matrix which involves the set of linear equations is solved by least square fit with the QR solver in Matlab. Specifically, the QR solver is used to find the minimum-norm-residual solution to the linear system $Ax = B$, which can be overdetermined as in our case. For each gas (defined as m in Eq. 7), such as He, H₂, O₂, N₂, CO₂ and CH₄, a new matrix is established to calculate the permeability contributions of each subunit in order to define the polyimide property for every gas. This enables the updating of the polyimide structures in the database established in 2000 [16] as new data for some gases become available for new subunits.

2.4 Proposal of new copolyimides

Following the calculation of the specific contributions of subunits, comparison in terms of the selectivity-permeability plots for O₂/N₂, CO₂/CH₄, H₂/CO₂, H₂/N₂, and CO₂/N₂ separation applications is made. This allows for the identification of the most outstanding diamine and dianhydrides with the best permeability/perm-selectivity values for each gas separation application, and thereby new and better copolyimide structures are proposed for each gas pair. The dianhydride:dianhydride or diamine:diamine ratios are set as 50:50. Permeability-selectivity plots

with upper bounds established in 1991 and 2008 based on the trade-off between permeability and selectivity defined by Robeson [27, 28] are introduced to show the performance of the proposed copolyimide structures and elucidate the limitations for each gas separation.

3. Results and Discussion

3.1 Production of data set for subunits and error analysis

The comparison between experimental and predicted gas permeability coefficients for He, H₂, O₂, N₂, CO₂ and CH₄ for the polyimides and copolyimides made up of 107 subunits is depicted in Figure 1, which are logarithmic plots of experimental versus predicted values. The dashed lines represent one-quarter (± 0.25), one-half (± 0.5) and one (± 1.0) order-of-magnitude of deviations between the predicted and experimental data. Note that one order-of-magnitude implies that the predicted value is ten times greater (+) or smaller (-) than the experimental value. Figure 1 shows that experimental and predicted permeability values agree very well to largely within a quarter of an order-of-magnitude, which is significantly lower than the half an order-of-magnitude of discrepancy by Alentiev et al. [16], and thereby underscores the improved predictions by the volume-based approach with large subunits used here. Notably, the recent group contribution study by Alentiev et al. [19] shows that the discrepancy is more than one order-of-magnitude, presumably due to the consideration of a large number of polymers (namely, 900), and also different types of polymer structures (such as polyimides, polyacetylenes, polyesters, polyethers, polysulfons, etc).

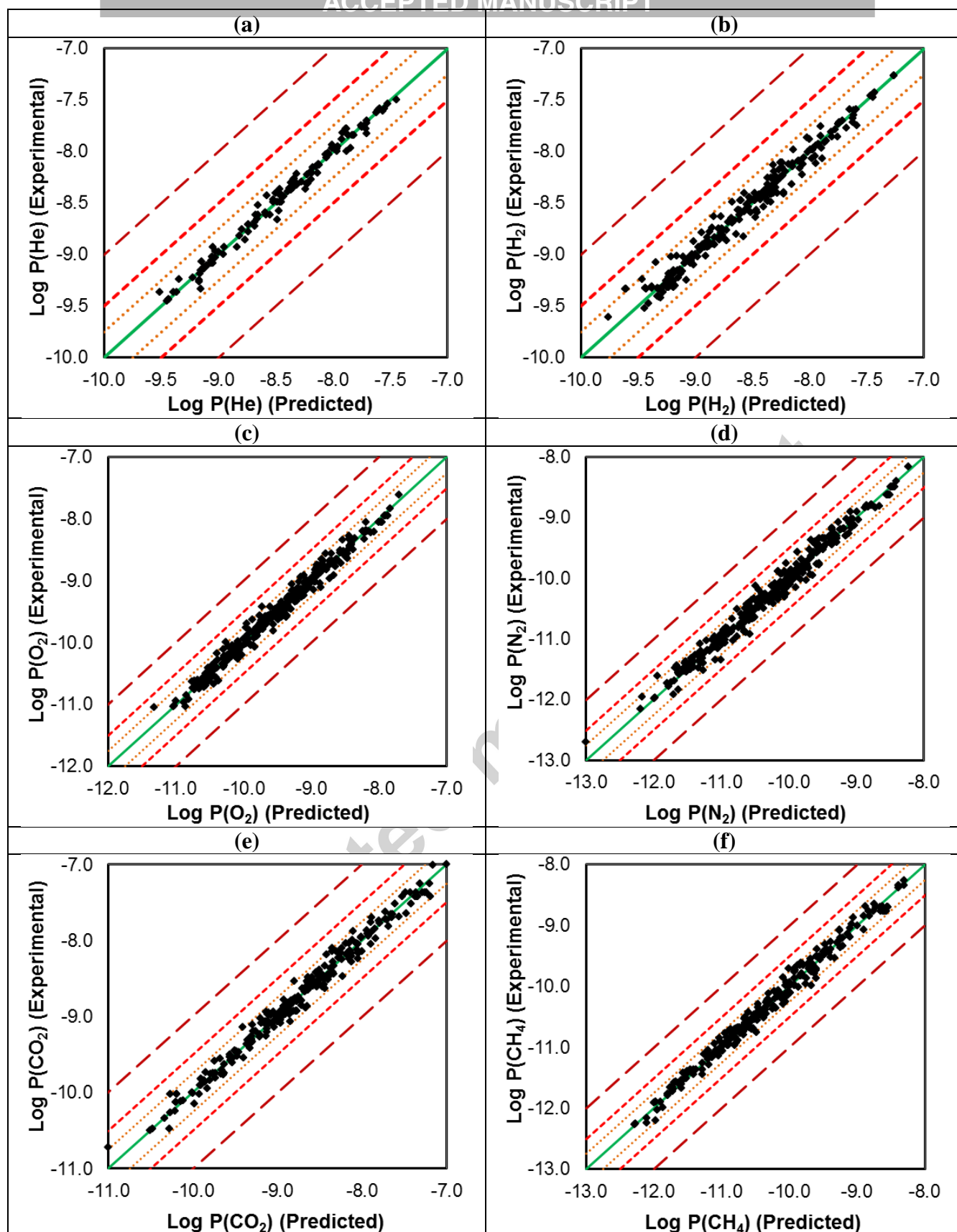


Figure 1. Comparison of experimental and predicted permeability coefficients calculated from the subunit contributions defined here for (a) He, (b) H₂, (c) O₂, (d) N₂, (e) CO₂, and (f) CH₄. (Figure displays the lower left quadrant of the Cartesian coordinate system)

Table 2. Error analysis of the permeability coefficients calculated by the proposed method in this study as well as other methods whose error analyses are available.

σ (standard deviation) ^a	0.14	0.26	0.30	0.29	0.24	0.23	
E (average error %) ^b	9.22	17.2	20.9	21.2	16.9	17.4	This study
Number of polymers	115	235	345	337	324	268	
σ ^a	0.11	---	0.18	0.21	0.22	0.25	Robeson et al. [1, 18]
E ^b	---	---	---	---	17.3	19.9	
Number of polymers	65	---	65	65	87	87	
E ^b	21.6	26.1	37.3	34.8	38.7	39.1	Park and Paul [15]
Number of polymers	79	63	102	101	101	102	

$$^a \sigma = \sqrt{\frac{\sum_{i=1}^n (\ln P_i(\text{predicted}) - \ln P_i(\text{experimental}))^2}{n}}$$

$$^b E = \sum_{i=1}^n \left| \frac{P_i(\text{experimental}) - P_i(\text{predicted})}{P_i(\text{experimental})} \right| * 100/n$$

Table 2 further quantifies statistically the error associated with the permeability coefficients for the gases investigated (namely, He, H₂, O₂, N₂, CO₂ and CH₄) in terms of standard deviation (σ) and average percent relative error (E); the statistics are presented for the method used here as well as that by others [1, 15, 18] whose error analyses are available. Two observations warrants highlighting. Firstly, Park and Paul [15] gives significantly higher E values despite the molar volume based approach, which is presumably because of the wide variety of polymers (such as polysulfones and polycarbonates) considered. This underscores the dominance of other parameters in the calculation protocol (e.g., definition of molar volume and subunits) in the accuracy of the predictions for the group contribution method. Secondly, the σ and E values for the current method are similar to those by Robeson et al. [1, 18], in spite of a much larger number of polymers considered in this study, which affirms the reliability of the subunit contribution derived by this method.

Addressing the risk of error escalation in predictions of selectivity between gas pairs is among the most important challenges, since the ideal selectivity is calculated as the ratio of the permeability coefficients. Accordingly, the comparisons between the experimental and predicted ideal selectivity values, calculated from the ratio of the permeability coefficients, for the gas pairs of O₂/N₂, CO₂/CH₄, H₂/CO₂, CO₂/N₂, H₂/CH₄ and He/N₂ are shown in Figure 2. Similar to Figure 1, the dashed lines in Figure 2 represent one-quarter (± 0.25), one-half (± 0.5) and one (± 1.0) order-of-magnitude deviation of the predictions from experimental data. In addition, Table 3 lists the standard deviation (σ) and average percent relative error (E) values. Figure 2 indicates that the predictions fluctuate randomly about the mean (green line) without any clear bias, which implies the statistical

analysis in Table 3 is sound. In Table 3, the largest σ and E values are for the He/N₂ gas pair, presumably due to the smallest number of polymers considered, whereas the smallest σ and E values are for the CO₂/CH₄ gas pair, which is notably of great industrial interest in the gas separation field. The agreement of the selectivity values between experiments and predictions is likely because of (i) the use of large subunits representative of diamine and dianhydride for the repeat unit of a polyimide, as per the method of Alentiev et al. [16], and (ii) the accurate calculation of the molar volume of the subunits that accounted for effects such as intra-molecular interactions defined by the used force field type. This underscores that the chemical structure of the constituent repeat unit as well as configurations of subunits are dominant factors in the gas permeation properties of glassy polymers, since they dictate key parameters such as connectivity (meta, para, or ortho), symmetry, etc. that affect the resulting membrane separation properties significantly.

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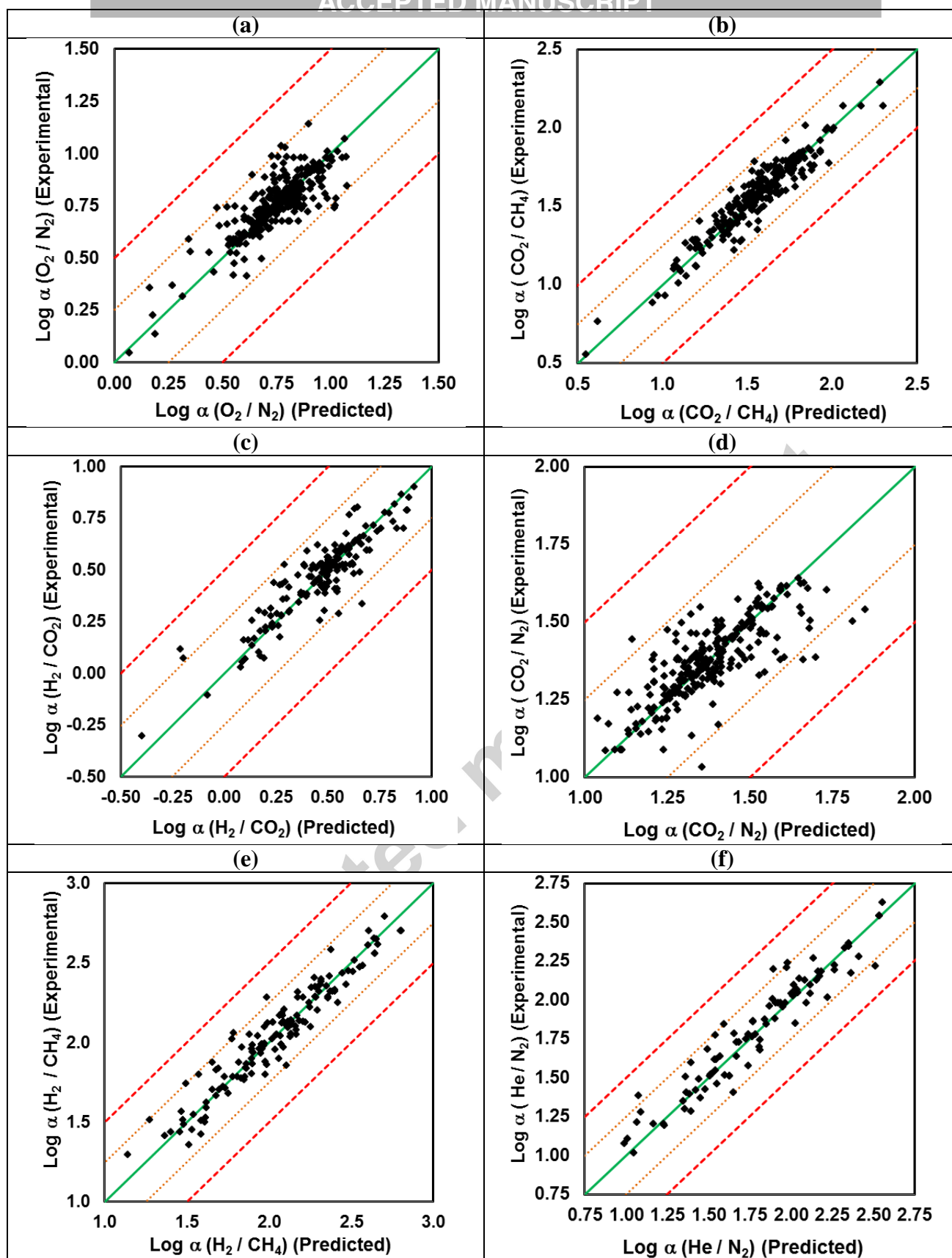


Figure 2. Comparison of experimental and predicted ideal selectivity coefficients calculated from the ratio of the permeability coefficients for (a) O_2/N_2 , (b) CO_2/CH_4 , (c) H_2/CO_2 , (d) CO_2/N_2 , (e) H_2/CH_4 , and (f) He/N_2 .

Table 3. Error analysis of the selectivity coefficients for different gas pairs calculated by the proposed method in this study. (The same formulas listed as footnotes in Table 2 are used.)

σ	0.19	0.17	0.22	0.21	0.22	0.27
E	12.9	12.7	16.2	13.9	17.6	20.8
Number of polymers	311	255	177	271	144	93

3.2 Analysis of proposed copolyimide structures

The possible combinations from the 32 dianhydrides and 75 diamines are enormous, therefore, we first identify the high-performing subunits, then specify that two out of the three subunits making up the copolyimide are the high-performing ones, and finally evaluate the performance of the resulting polymers. Specifically, in this part of the study, the better-performing subunits for each gas separation application (namely, O₂/N₂, CO₂/CH₄, H₂/CO₂, CO₂/N₂, H₂/CH₄, and He/N₂) are identified then analyzed in more depth. Firstly, for each gas pair, all the subunits considered are first plotted in terms of selectivity versus permeability to distinguish the dianhydride or diamine subunits with superior performance in terms of both selectivity and permeability. Secondly, these dianhydride subunits displaying superior performance are then paired with different subunits to make up different copolyimide structures for further assessment of the resulting performance. It should be noted that each copolyimide contains repeating units of dianhydride(1)/dianhydride(2)-diamine or dianhydride-diamine(1)/diamine(2). Specifically, (i) the diamine/diamine or dianhydride/dianhydride ratios are set at a constant of 50/50, (ii) when the copolyimide is of the form dianhydride(1)/dianhydride(2)-diamine, the superior dianhydride is set as dianhydride(1) in the repeating unit, while dianhydride(2) is any of the other dianhydrides and diamine is one of five diamines chosen based on either higher permeability or higher selectivity, and (iii) when the copolyimide is of the form dianhydride-diamine(1)/diamine(2), the superior dianhydride is kept constant, diamine(1) is any of the 75 considered here, while diamine(2) is one of five diamines chosen based on either higher permeability or higher selectivity. Regarding (ii) and (iii), Table 4 explicitly lists the combinations used for the O₂/N₂ gas pair predictions. Notably, 6FDA is set as the first dianhydride for all gas pairs because of the general agreement that it is a remarkable monomer with unique transport properties. Thirdly, the evaluation of the performance of the proposed copolyimide structures is carried out to ascertain whether the upper permeability-selectivity bounds established in years 1991 and 2008 based on the trade-off between permeability and selectivity [27, 28] are exceeded, which is similar to the analysis reported earlier [17].

Therefore, all the figures in this section contains four sub-figures of selectivity versus permeability: (a) all subunits considered, (b) 6FDA-based copolyimides, and (c) and (d) for the copolyimides composed of a high-performing dianhydride each identified in (a). All the sub-figures (b) – (d) have the same ranges for the x - and y -axes for easier comparison. The analysis is valuable for providing insights into the fabrication of novel materials with better performance with respect to both selectivity and permeability for the separation of specific gas pairs.

Analysis of the performance of copolyimides in O_2/N_2 separation

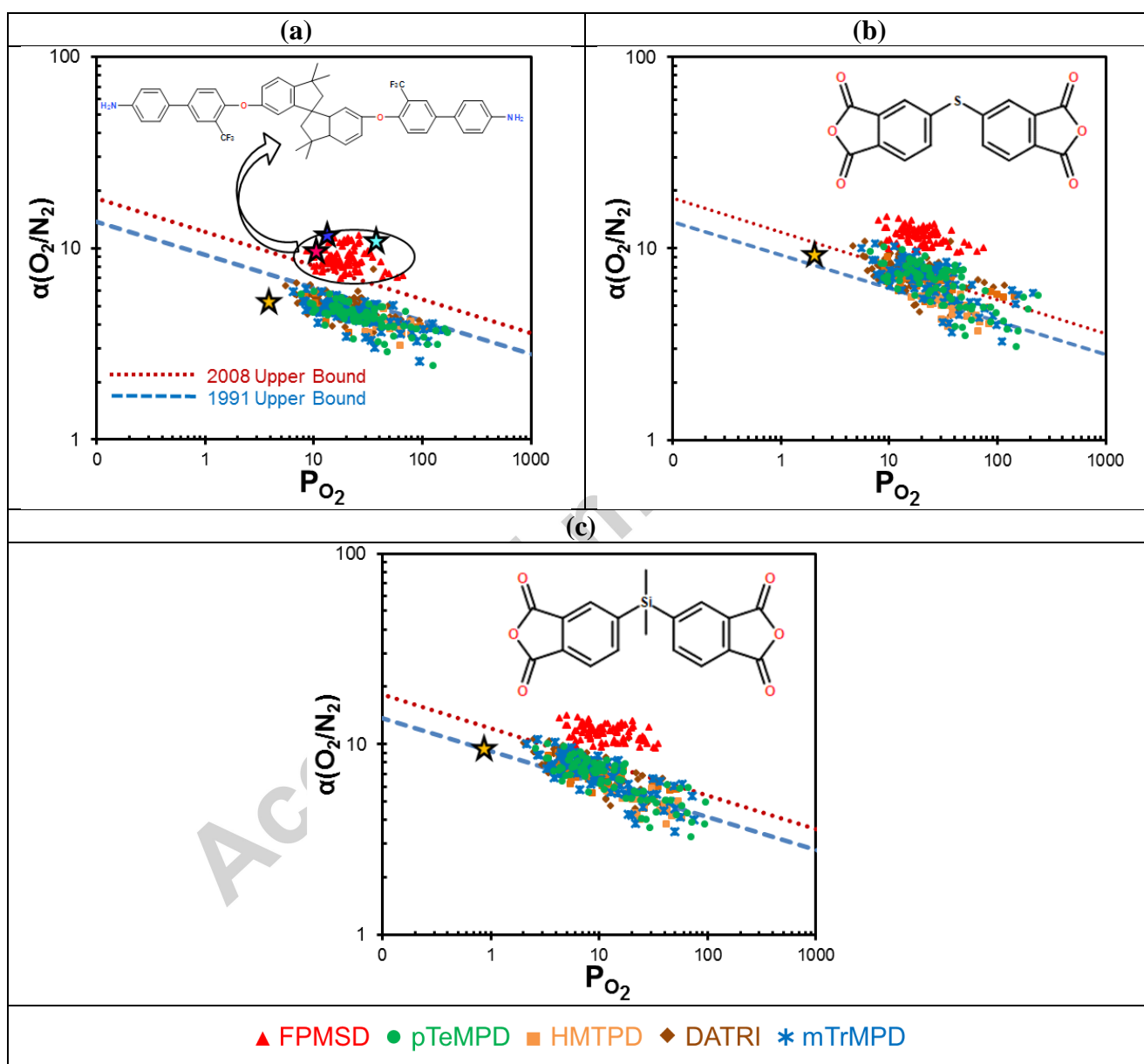


Figure 3. Predicted selectivity versus permeability diagrams of O_2/N_2 separation for (a) 6FDA-based copolyimides (star symbols with pink, blue, aqua and yellow color represent experimental transport properties of BPADA-FPMSD, 6FDA-FPMSD, ODPA-FPMSD, and 6FDA-ODA, respectively [38-

40]), (b) pTDPA-based copolyimides (star symbol with yellow color represents experimental transport property of pTDPA-ODA [41]), and (c) SiDA-based copolyimides (star symbol with yellow color represents experimental transport property of SiDA-ODA [42]). The chemical structures of FPMSD, pTDPA, and SiDA are given in the inset of Figures (a), (b) and (c), respectively. The blue dashed and red dotted lines represent respectively the 1991 and 2008 upper bounds based on the selectivity-permeability tradeoff [27, 28].

Figure 3 presents the selectivity-permeability plots for the O_2/N_2 gas pair. The performance of the subunits shown in Figure A1 (a) shows that, other than 6FDA, pTDPA and SiDA exhibit higher permeability compared to other dianhydrides and comparable selectivity. Therefore, Figures 3 (a), (b) and (c) represent respectively the 6FDA-, pTDPA- and SiDA-based copolyimides. Additionally, while DATRI, HMTPD, mTrMPD and pTeMPD are selected as the diamines due to high permeability, FPMSD is chosen owing to high O_2/N_2 selectivity. It is desired in the membrane-based gas separation industry that the ideal membrane should have both high permeability and selectivity properties, however, a tradeoff inevitably exists in reality. For this reason, subunit combinations for the copolyimide construction are performed based on some subunits with high permeability and some with high selectivity. On the other hand, when the permeability contribution of each monomer or subunit is investigated, it is shown in Figure A1 (a) that, generally, high permeability stems from the diamine, while high selectivity arises from the dianhydride. All combinations to form a copolyimide from either dianhydride(1)/dianhydride(2)-diamine or dianhydride-diamine(1)/diamine(2) are explicitly listed in Table 4 for clarification. Such details will not be given for subsequent gas pairs.

It should be noted that O_2/N_2 selectivity values of less than one are unrealistic, which is linked to the different permeabilities of the same polyimide reported in the literature due to solvent effects, annealing, imidization methods, etc. For instance, the 6FDA-mTrMPD polyimide is associated with nine different O_2 permeability coefficients (inset in Figure A1 (a)) varying between 40 to 200 Barrer [29-37]. Because each O_2 and N_2 permeability value for the 6FDA-mTrMPD polyimide is included as an independent equation in the matrix of the system using Eq. 2, the large deviation in experimental values leads to the unrealistic O_2/N_2 selectivity values of lower than one, as is also the case for other polyimides. Notably, this compromises the accuracy of group contribution methods if the second type of polyimide is directly related to the polyimide with such scattered experimental data. As explained later in the section of “Analysis of the performance of copolyimides in CO_2/N_2 separation”, such error can be mitigated in the current method by (i) increasing the number of

different polyimides derived from the same dianhydride or diamine, and/or (ii) taking into consideration the factors (solvent type, synthesis route, residual solvent, etc.) that influence the membrane performance during synthesis. The experimental permeability coefficients of polyimides presented along with predicted permeabilities of copolyimides in Figure 3 clearly demonstrates the agreement between predicted and experimental values. For instance, Figure 3 (a) shows that the predicted data of the copolyimide constituted from 6FDA dianhydride and FPMSD diamine (red triangles) fall into the same region as the experimental data for 6FDA-FPMSD polyimide (blue star).

Table 4. Copolyimide combinations used in the predictive analysis of O₂/N₂ separation in Figure 3

	Symbol	Dianhydride (1)	Dianhydride (2)	Diamine (1)	Diamine (2)	
1	◆	6FDA	all others*	DATRI	-	Figure 3 (b)
		6FDA	-	DATRI	all others*	
2	■	6FDA	all others*	HMTPD	-	
		6FDA	-	HMTPD	all others*	
3	*	6FDA	all others*	mTrMPD	-	
		6FDA	-	mTrMPD	all others*	
4	●	6FDA	all others*	pTeMPD	-	
		6FDA	-	pTeMPD	all others*	
5	▲	6FDA	all others*	FPMSD	-	
		6FDA	-	FPMSD	all others*	
6	◆	pTDPA	all others*	DATRI	-	Figure 3 (c)
		pTDPA	-	DATRI	all others*	
7	■	pTDPA	all others*	HMTPD	-	
		pTDPA	-	HMTPD	all others*	
8	*	pTDPA	all others*	mTrMPD	-	
		pTDPA	-	mTrMPD	all others*	
9	●	pTDPA	all others*	pTeMPD	-	
		pTDPA	-	pTeMPD	all others*	
10	▲	pTDPA	all others*	FPMSD	-	
		pTDPA	-	FPMSD	all others*	
11	◆	SiDA	all others*	DATRI	-	Figure 3 (d)
		SiDA	-	DATRI	all others*	
12	■	SiDA	all others*	HMTPD	-	
		SiDA	-	HMTPD	all others*	
13	*	SiDA	all others*	mTrMPD	-	
		SiDA	-	mTrMPD	all others*	
14	●	SiDA	all others*	pTeMPD	-	
		SiDA	-	pTeMPD	all others*	
15	▲	SiDA	all others*	FPMSD	-	
		SiDA	-	FPMSD	all others*	

* Other dianhydrides or diamines considered in this study

It is evident from Figure 3 that both the upper bounds based on the selectivity-permeability tradeoff can be exceeded by the judicious selection of dianhydrides and diamines as subunits to make up the copolyimides, which thereby provides recommendations for the synthesis of such polyimides to enhance O_2/N_2 separation. Figure 3 (a) shows that, although the 6FDA-based copolyimides largely fall below even the 1991 bound, those with the FPMSD diamine surpass the 2008 bound by having better selectivity comparatively. Although the copolyimides represented by the same symbol are composed of the same two high-performing subunits, the third subunit is different (refer to Table 4), which leads to the scatter of data. This indicates the non-negligible influence of the third constituent subunit on the performance of the resulting copolyimide. As for the pTDPA-based and SiDA-based copolyimides respectively in Figures 3 (b) and (c), (i) the performance is generally superior to that of the 6FDA-based copolyimides (Figure 3 (a)) in terms of largely exceeding the 1991 bound particularly with higher selectivity, and (ii) FPMSD persists in conferring the best performance, surpassing the 2008 bounds by greater extents than that of other subunits (Figure A1 (a)). Regarding FPMSD, the only report available in the literature combining it with 6FDA, BPADA and ODPA dianhydrides (star symbols with blue, pink and aqua colors in Figure 3 (a) respectively), also indicated high O_2/N_2 performance for these three polyimides with selectivity of about 10 [38], the value of which agrees with Figure A1 (a). However, one can get even higher selectivity of about 50% more (i.e., 15) by coupling FPMSD with other dianhydrides like either pTDPA (Figure 3 (b)) or SiDA (Figure 3 (c)). In addition, the O_2/N_2 selectivity enhancement can be revealed by the comparison of experimental transport properties of polyimides derived from commonly-used diamine type in the literature like ODA (star symbols with yellow color represent 6FDA-ODA, pTDPA-ODA, and SiDA-ODA respectively in Figures 3 (a), (b) and (c)). The percent relative error of O_2 and N_2 permeabilities for 6FDA-ODA, pTDPA-ODA, and SiDA-ODA polyimides differ from 0.3 to 5.9 %. For the membrane-based gas separation industry, increase in either permeability or selectivity represents lower operating cost. Collectively, the results demonstrate that the application of the group contribution method is straightforward and insightful in providing guidance on the tailoring of polymers for specific applications.

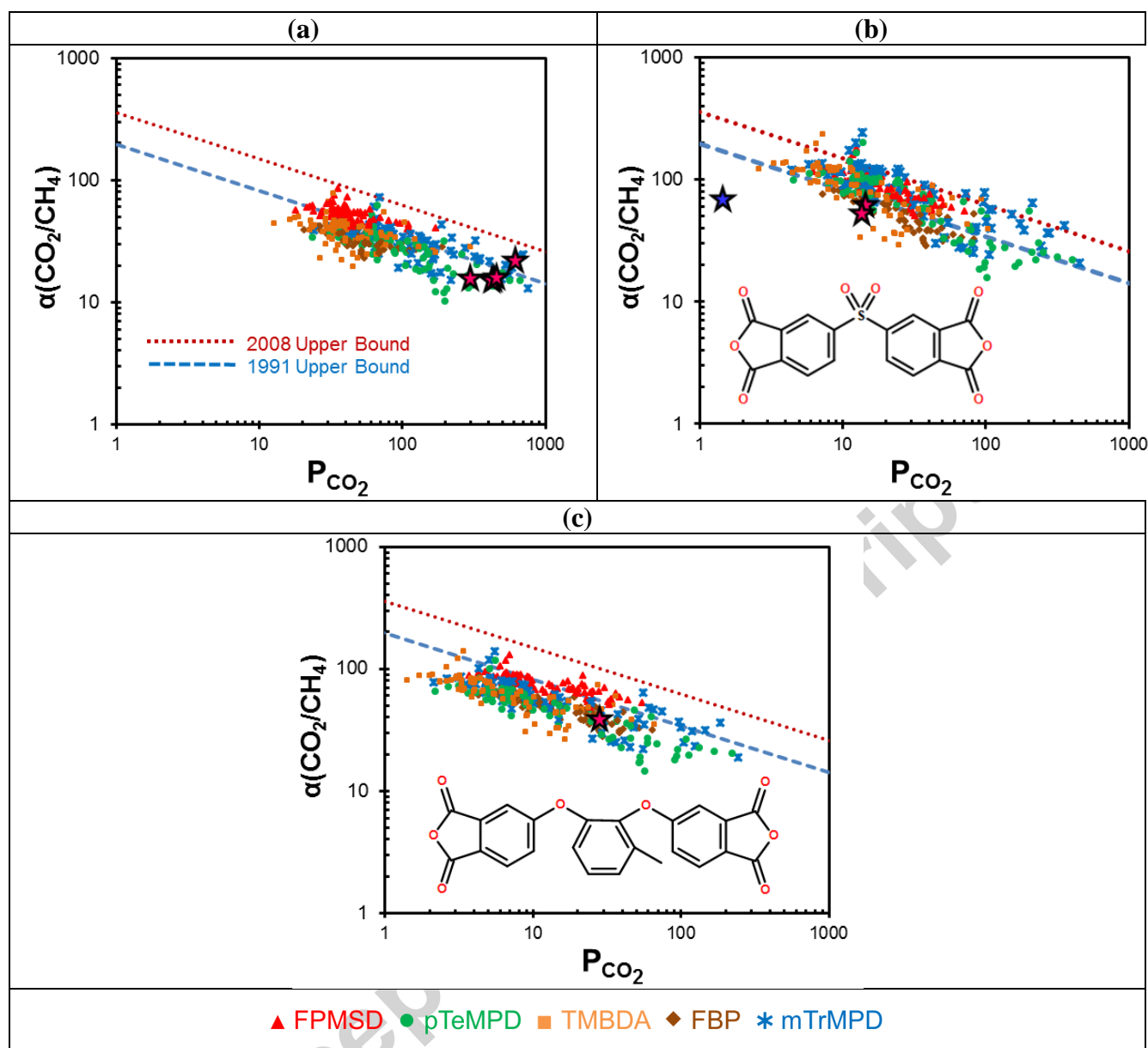


Figure 4. Predicted selectivity versus permeability diagrams of CO₂/CH₄ separation for (a) 6FDA-based copolyimides (star symbols with pink color represent available experimental transport properties of 6FDA-pTeMPD [29, 33, 43-45]), (b) DSDA-based copolyimides, with the inset showing the chemical structure of DSDA (star symbols with blue and pink color represent experimental transport property of respectively DSDA-BAPS and DSDA-DDBT [46-48]), and (c) 3MCADPA-based copolyimides, with the inset showing the chemical structure of 3MCADPA (star symbol with pink color represents experimental transport property of 3MCADPA-pTeMPD [49]). The blue dashed and red dotted lines represent respectively the 1991 and 2008 upper bounds based on the selectivity-permeability tradeoff [27, 28].

Analogous to Figure 3, Figure 4 displays the selectivity versus permeability plots for CO₂/CH₄ separation. Figure A1 (b) indicates that the most promising subunits are the 6FDA (Figure 4 (a)), DSDA (Figure 4 (b)) and 3MCADPA (Figure 4 (c)) dianhydrides; additionally, the diamines TMBDA, mTrMPD and pTeMPD are selected due to their high permeability performance, and FBP and FPMSD are chosen owing to high selectivity performance compared to other diamine subunits. In contrast to Figure A1 (a), much fewer subunits exceed the upper bound in Figure A1 (b), which suggests that more improvements for CO₂/CH₄ separation is needed. Despite the rapid progress in membrane fabrication, CO₂/CH₄ separation application so far is limited to novel monomers.

The same deduction in the analysis of O₂/N₂ selectivity can be made regarding the CO₂/CH₄ selectivity values of less than one in Figure A1 (b), whereby the inset shows that the 6FDA-mTrMPD polyimide has eight different CO₂ permeability coefficients in the wide range of 150 and 850 Barrer. This is also the case for the 6FDA-pTeMPD polyimide, whereby the experimental CO₂ permeability coefficients range from 300 to 615 Barrer (pink stars in Figure 4 (a)). The corresponding predicted CO₂ permeability coefficient is 380 Barrer with minimum, average and maximum percent relative errors of 10.2, 20.7 and 40.7, respectively, which underlies the similar error values obtained in the study of Robeson et al. [1, 18] that only included a smaller number of polyimides. Nevertheless, coherence between experimental and predicted values is apparent in Figure 4 (a). It is well-known that the 6FDA-mTrMPD and 6FDA-pTeMPD polyimides exhibit the highest CO₂ permeability values among the polyimides reported in the literature, so it is expected that the experimental CO₂ permeability of the 6FDA-pTeMPD polyimide should have higher x-axis values, as explicit in Figure 4 (a).

It is evident in Figure 4 that the copolyimides largely fall below the 2008 bound, which implies that even the combinations of better performing subunits fall short of improving such separations. While the 6FDA-based copolyimides congregate around the 1991 upper bound without exceeding the 2008 upper bound (Figure 4 (a)), the 3MCADPA-based copolyimides perform even worse with a larger proportion being below the 1991 bound (Figure 4 (c)). Among the three high performing dianhydride subunits (Figure 4 (a) – (c)), the DSDA-based copolyimides performs the best with most falling in between the two bounds and particularly those with the mTrMPD diamine surpassing the 2008 upper bound. The performance of the mTrMPD diamine in polyimide membranes for CO₂/CH₄ separation has been widely reported, and has been attributed to the large d-spacing value due to three –CH₃ groups connected to the phenyl ring in the mTrMPD moiety, which increases the free volume of the polymer and thereby increases permeability [7, 8, 10, 50]. The mTrMPD diamine is generally seen to give superior performance for CO₂/CH₄ throughout Figures 4 (a) – (c) in some combinations of

copolyimides. Comparing the predicted sub-unit contributions of 6FDA and 3MCADPA in Figure A1 (b), 6FDA has high permeability but low selectivity compared to 3MCADPA. When we combine these two dianhydrides with the same diamine like pTeMPD, the experimental values exhibit the same trends, specifically. 6FDA-pTeMPD has high CO₂ permeability and low CO₂/CH₄ selectivity compared to 3MCADPA-pTeMPD. This indicates the consistency of our predictions with experiments. CO₂/CH₄ selectivity enhancement can be easily obtained by coupling existing diamines with the DSDA dianhydride (which confers superior CO₂/CH₄ selectivity). Experimental performance of some DSDA-based polyimides is given in Figure 4 (b) as an example (star symbols with blue and pink color represent experimental transport property of DSDA-BAPS and DSDA-DDBT, respectively).

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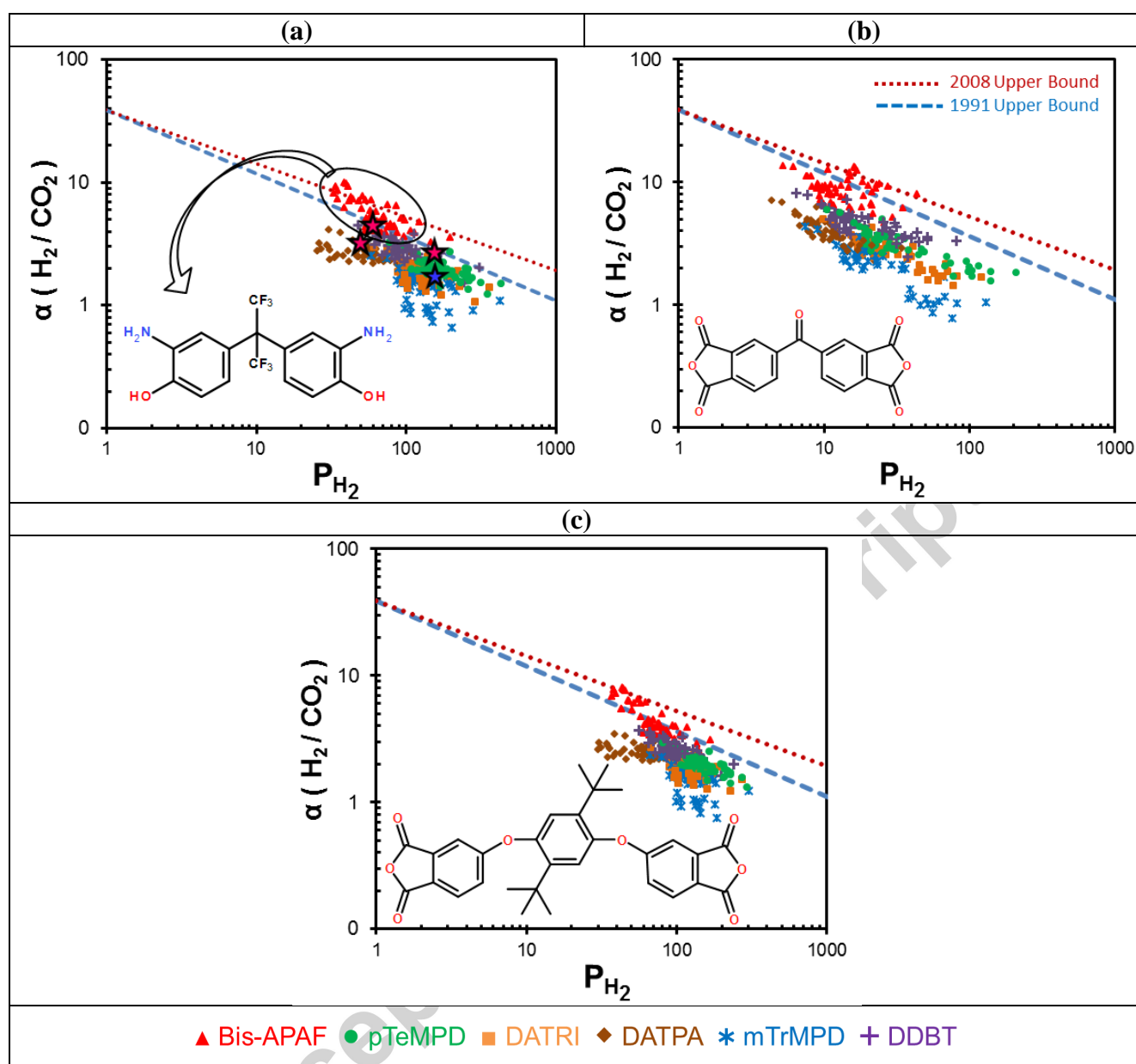


Figure 5. Predicted selectivity versus permeability diagrams of H_2/CO_2 separation for (a) 6FDA-based copolyimides (star symbols with pink and blue color represent experimental transport properties of 6FDA-bis-APAF polyimides and 6FDA-bis-APAF/mTrMPD copolyimide, respectively [51-53]), (b) BTDA-based copolyimides, and (c) DTBHQDPA-based copolyimides. The chemical structures of Bis-APAF, BTDA and DTBHQDPA are given in the insets of Figures (a), (b) and (c), respectively. The blue dashed and red dotted lines represent respectively the 1991 and 2008 upper bounds based on the selectivity-permeability tradeoff [27, 28].

Figure 5 presents the selectivity versus permeability plots for H₂/CO₂ separation. Three observations are highlighted here. Firstly, Figure A1 (c) shows that all dianhydride subunits are above the upper bound, with most exhibiting low permeability behavior. The dianhydride with the highest selectivity (namely, BTDA) and two with the highest permeability (namely, 6FDA and DTBHQDPA) are selected for further assessment in Figures 5 (a) – (c). In contrast, all diamines are below the upper bound; nonetheless, those with higher selectivity (namely, bis-APAF and DATPA) and higher permeability (namely, DATRI, DDBT, mTrMPD and pTeMPD) are selected for analysis. Secondly, similar to that for CO₂/CH₄ separation (Figure 4), the copolyimides fall below but close to the 2008 upper bound with the monomers available in the literature in Figure 5, despite the consideration of the best-performing dianhydrides and diamines. Compared to the 6FDA dianhydride (Figure 5 (a)), the BTDA dianhydride (Figure 5 (b)) confers lower permeability, while the DTBHQDPA dianhydride (Figure 5 (c)) leads to similar but smaller ranges of both selectivity and permeability. This indicates that the 6FDA-based copolyimides seem most promising in the H₂/CO₂ separation application. Thirdly, the bis-APAF diamine stands out in terms of giving copolyimides that are closest to and with some exceeding the 2008 bound. Recently, a new class of thermally-modified aromatic polyimides, in which the diamine is either bis-APAF or mHAB, has emerged as a prominent membrane material in gas separation [54, 55]. With respect to the effect of bis-APAF, it is hypothesized that the attendant changes in molecular connectivity and conformation that alter chain packing leads to a unique free volume distribution and rigid structure, which is crucial to enabling thermal modification and obtaining insoluble polybenzoxazoles (PBOs) membranes that exhibit exceptional thermal and chemical resistance. The results here affirm that bis-APAF is a beneficial amine in copolyimides for H₂/CO₂ separation application. On the other hand, Figure 5 (a) shows that the experimental H₂ permeability coefficient of 6FDA-bis-APAF polyimide (pink stars) fall into the region of the group of copolyimide constituted from 6FDA dianhydride and bis-APAF diamine (red triangles). In addition, Figure 5 (a) indicates that the experimental H₂ permeability of 6FDA-bis-APAF/mTrMPD copolyimide (blue star) is 156 Barrer which is exactly the same as that predicted, and the experimental and predicted H₂/CO₂ selectivity is respectively 1.8 and 2.7. These observations affirm the predictive capability of group contribution models.

In particular for H₂/CO₂ separation, the membrane should be equipped with the ability to discriminate the small difference in the kinetic diameters of H₂ and CO₂, and/or preferentially adsorb H₂ compared to CO₂. While molecular dynamics simulation is informative on the choice of dianhydrides and diamines to enhance the performance of copolyimides in H₂/CO₂ separation, further advances in molecular design will improve membranes for such gas separation applications.

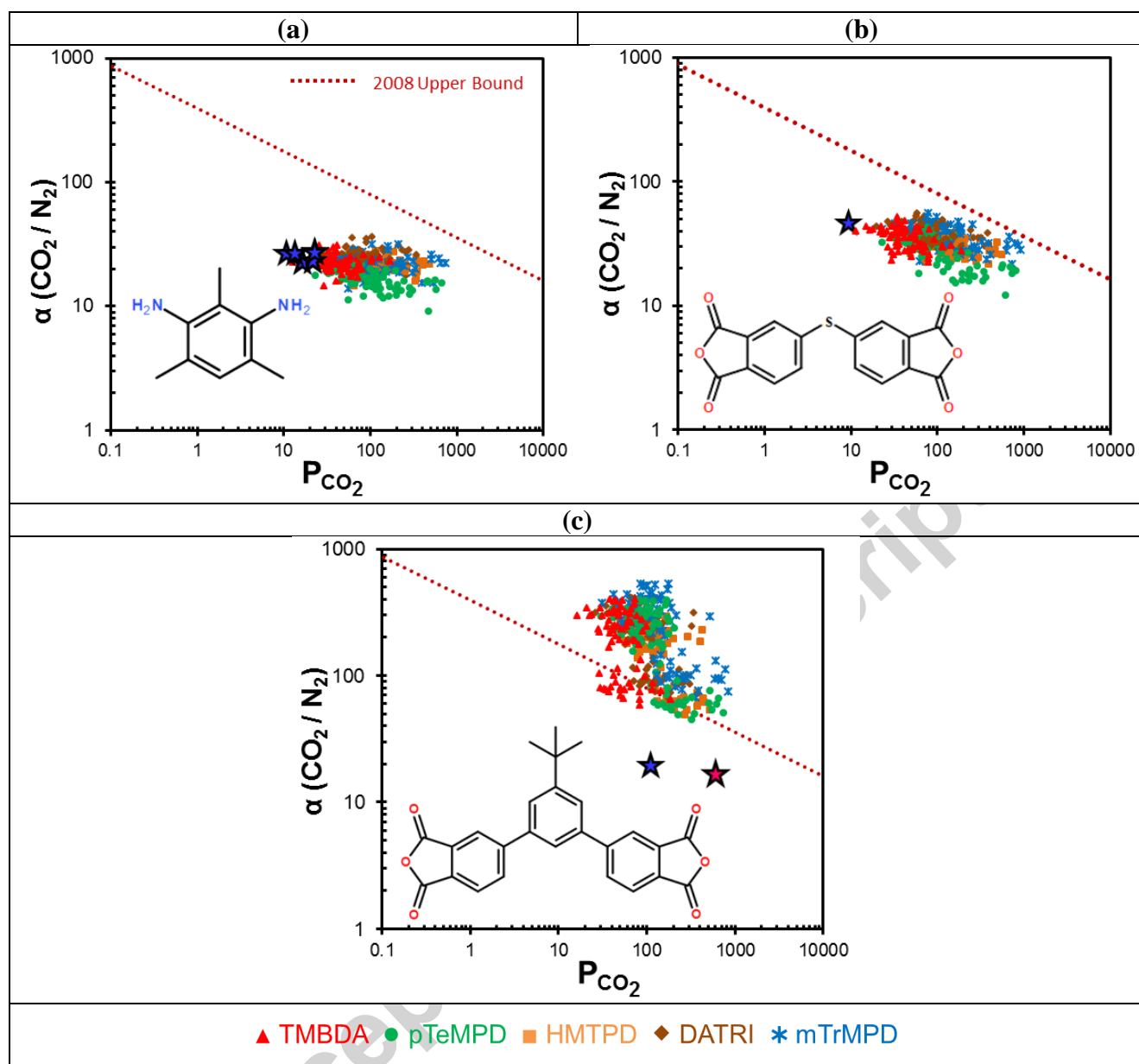


Figure 6. Predicted selectivity versus permeability diagrams of CO_2/N_2 separation for (a) 6FDA-based copolyimides, with the inset showing the chemical structure of mTrMPD (star symbols with blue color represent experimental transport properties of various 6FDA-ODA polyimides [39, 40, 56-60]), (b) pTDPA-based copolyimides, with the inset showing the chemical structure of pTDPA (star symbol with blue color represents experimental transport property of pTDPA-ODA [41]), and (c) BTPDA-based copolyimides, with the inset showing the chemical structure of BTPDA (star symbols with pink and blue colors represent experimental transport property of BTPDA-mTrMPD and BTPDA-6FpDA, respectively [61]). The red dotted line represents the 2008 upper bound based on the selectivity-permeability tradeoff; the 1991 study did not investigate CO_2/N_2 separation [27, 28].

Figure 6 depicts the selectivity-permeability information for CO₂/N₂ separation. It should be noted that the 1991 upper bound is not shown in Figures 6 (a) – (c) because the CO₂/N₂ separation was not included in the study [27]. Figure A1 (d) shows clearly that only a few subunits are above the upper bound, which indicates the limited performance of the available subunits for the CO₂/N₂ gas pair and suggests the need for further improvements. Accordingly, in this study, higher performing subunits are chosen to customize the copolyimides to enhance the CO₂/N₂ separation. The 6FDA, BTPDA and pTDPA dianhydrides are identified for the high permeability, while the DATRI, HMPD, TMBDA, mTrMPD and pTeMPD diamines are identified for the high CO₂/N₂ selectivity. Among the three dianhydrides assessed (Figures 6 (a) – (c)), pTDPA (Figure 6(b)) gave better performance than 6FDA (Figure 6(a)), both of which are below the 2008 bound. Experimental CO₂/N₂ selectivity is enhanced with the incorporation of the pTDPA-ODA polyimide (blue star in Figure 6 (b)) instead of 6FDA-ODA (blue stars in Figure 6 (a)), which is evident in Figure A1 (d). As for diamines, the mTrMPD noticeably gives better performance with all three dianhydrides considered (Figures 6 (a) – (c)).

In the literature, seven different polyimides constituted by the BTPDA dianhydride have been synthesized, and shown to give reasonable performance for O₂/N₂ and CO₂/CH₄ separations, but CO₂/N₂ separation was not investigated [61-63]. Two polyimides, namely, BTPDA-mTrMPD and BTPDA-6FpDA (pink and blue stars in Figure 6 (c), respectively), have reported O₂, N₂, CO₂ and CH₄ permeability coefficients from which CO₂/N₂ selectivity can be calculated. Although BTPDA dianhydride displays high performance in Figure A1 (d), two experimental CO₂/N₂ selectivities associated with these polyimides fall well below the performance of the copolyimide group (Figure 6 (c)) derived from BTPDA dianhydride. It is evident in Figure 3 for O₂/N₂ separation that group contribution methods may mislead if the second type of polyimide is directly related to the polyimide that has scattered experimental data that leads to unrealistic selectivity values, and has very few experimental data derived from the novel monomer. For example, the 6FDA-mTrMPD (or any polyimide including mTrMPD diamine) polyimide has scattered data which leads to increased error associated with the mTrMPD diamine, as is also the case for the 6FpDA diamine. Correspondingly, the permeability contribution of BTPDA for BTPDA-mTrMPD and BTPDA-6FpDA polyimides should benefit from the permeability contribution of mTrMPD and 6FpDA diamines, respectively. The results will lead to a higher contribution for BTPDA due to the lower contribution of mTrMPD in order to yield comparable predicted permeability of BTPDA-mTrMPD with experimental results. The error can be mitigated by increasing the number of different polyimides derived from the BTPDA dianhydride and/or taking into consideration the factors that influence the membrane performance in synthesis.

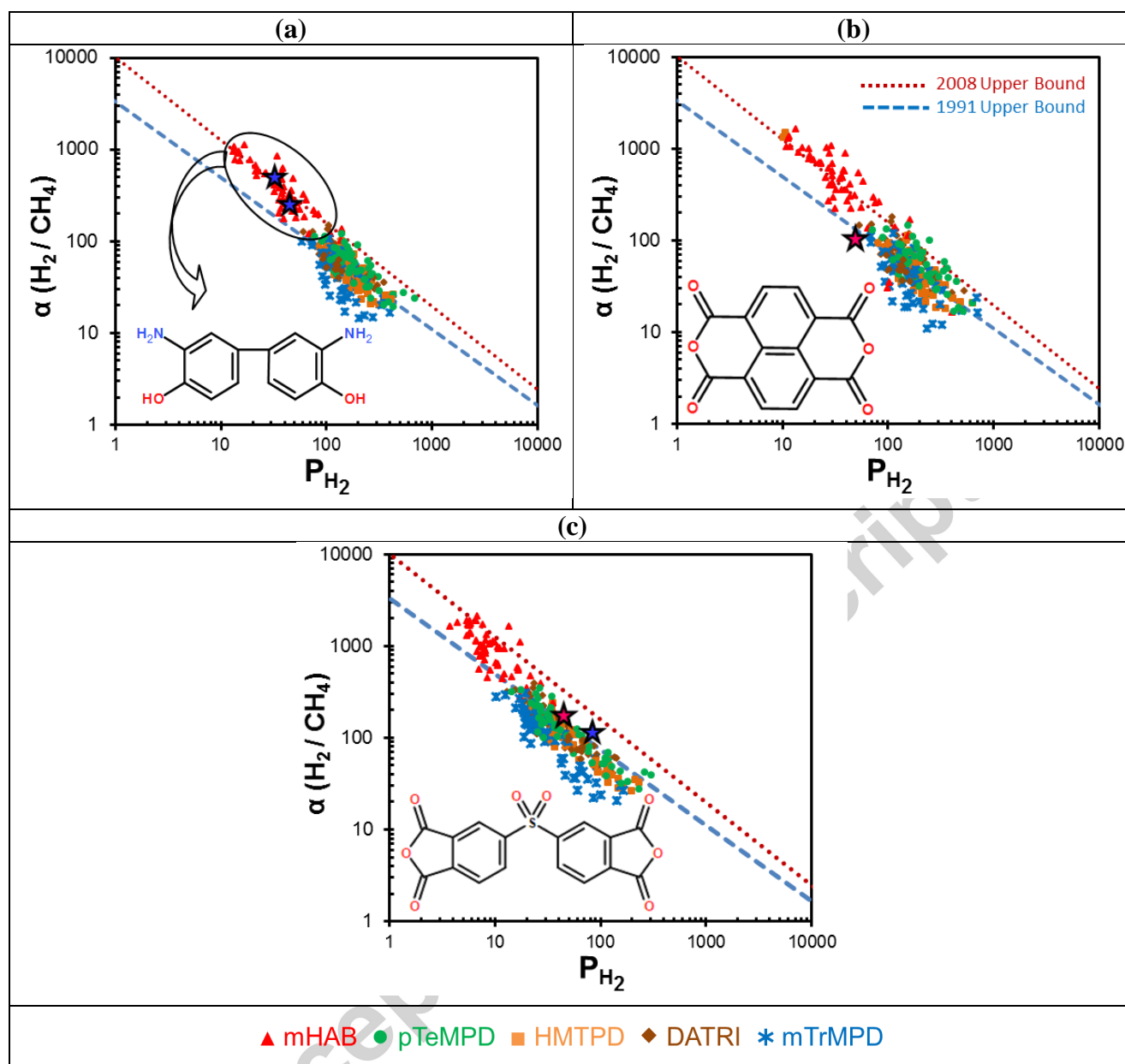


Figure 7. Predicted selectivity versus permeability diagrams of H_2/CH_4 separation for (a) 6FDA-based copolyimides (star symbols with blue color represent experimental transport properties of 6FDA-mHAB polyimides [64, 65]), (b) NTDA-based copolyimides (star symbol with pink color represents experimental transport property of NTDA-BAPHF [66]), and (c) DSDA-based copolyimides (star symbols with pink and blue color represent experimental transport properties of DSDA-DDBT polyimide and DSDA/TADATO-DDBT copolyimide, respectively [48, 67]). The chemical structures of mHAB, NTDA and DSDA are given in the insets of Figures (a), (b) and (c), respectively. The blue dashed and red dotted lines represent respectively the 1991 and 2008 upper bounds based on the selectivity-permeability tradeoff [27, 28].

Figure 7 presents the analysis for the H₂/CH₄ separation application. Figure A1 (e) shows that all dianhydride subunits lie above the upper bound, exhibiting low permeability but high selectivity; the dianhydride with the highest selectivity (namely, DSDA) and two with highest permeability (namely, 6FDA and NTDA) are selected for further analysis in Figures 7 (a) – (c). As for the diamines, all fall below the upper bound; nonetheless, DATRI, HMTPD, mTrMPD and pTeMPD are selected for high permeability, and mHAB is selected for high selectivity. It is worth noting that the sulphone-containing dianhydrides have been identified as giving superior performance, such as DSDA in H₂/CH₄ (Figure 7), CO₂/N₂ (Figure 6) and CO₂/CH₄ (Figure 4) separations, and pTDPA in CO₂/N₂ (Figure 6) and O₂/N₂ (Figure 3) separations. A previous study also concluded that copolyimides derived from the sulphone containing diamines such as BAPS and pDDS exhibit outstanding properties [17].

Based on Figure 7, with combinations of high performing dianhydrides and diamines, the resulting copolyimides lie close to but below the 2008 upper bound like the case of H₂/CO₂ (Figure 5). Among the three dianhydrides, the DSDA-based copolyimides (Figure 7 (c)) performed the worst, with many falling even below the 1991 upper bound, while both 6FDA-based (Figure 7 (a)) and NTDA-based copolyimides (Figure 7 (b)) perform similarly. Among the diamines, the mHAB, which, as with bis-APAF (with high performance in H₂/CO₂ separation (Figure 5)), is mainly used in the literature as a precursor for thermally rearranged polymers, enhances the performance of the copolyimide for H₂/CO₂ separation. In addition, Figure 5 (a) shows that the experimental coefficients of 6FDA-mHAB polyimides (blue stars) fall into the region of the predicted coefficients belonging to the group of copolyimide derived from 6FDA dianhydride and mHAB diamine (red triangles), revealing consistency between predicted and experimental values.

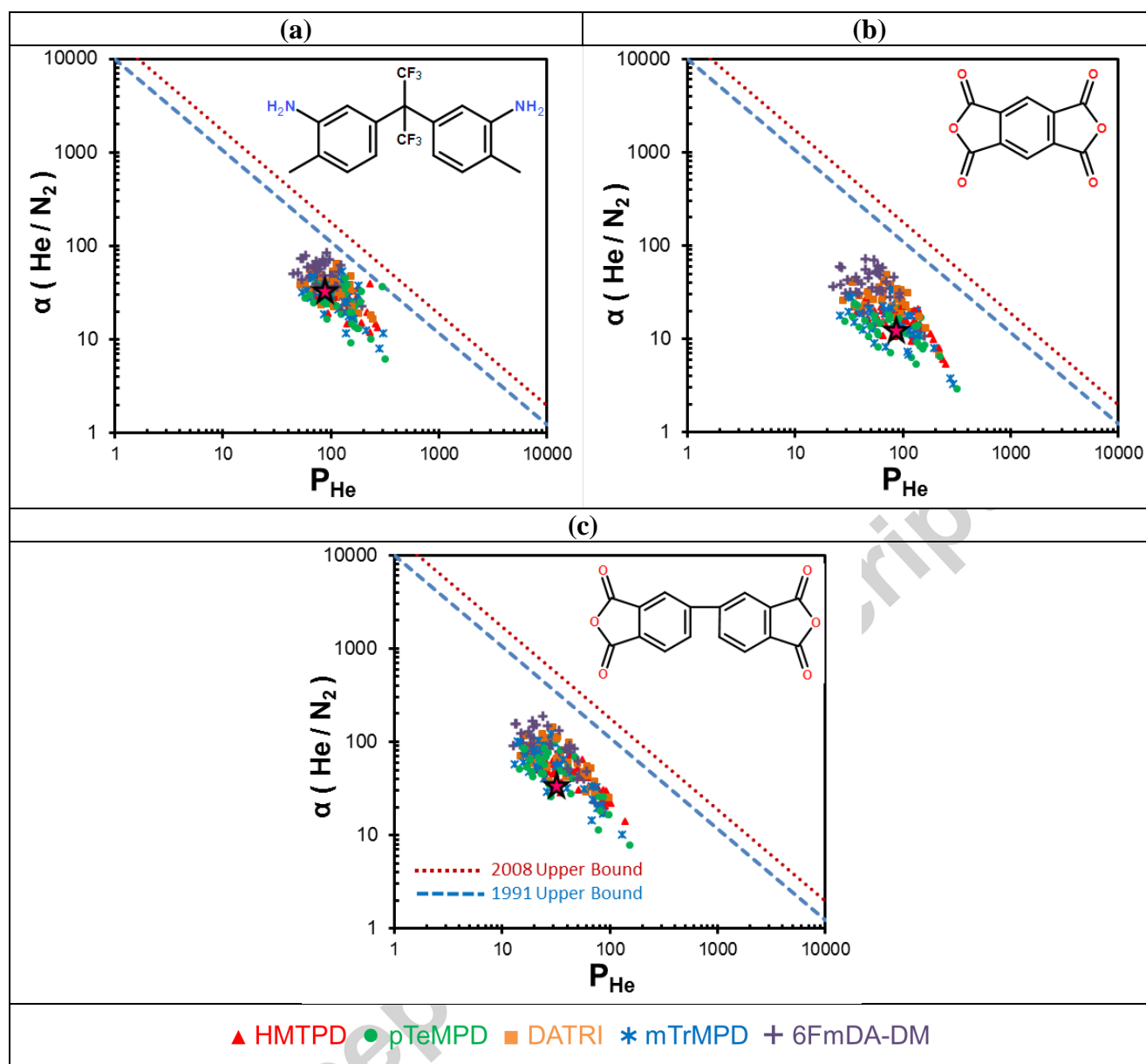


Figure 8. Predicted selectivity versus permeability diagrams of He/N₂ separation for (a) 6FDA-based copolyimides (star symbol with pink color represents experimental transport property of PTPDA-6FmDA-DM [61]), (b) PMDA-based copolyimides (star symbol with pink color represents experimental transport property of PMDA-TMMDA [40]), and (c) BPDA-based copolyimides (star symbol with pink color represents experimental transport property of BPDA-TMMDA [40]). The chemical structures of 6FmDA-DM, PMDA and BPDA are given in the insets of Figures (a), (b) and (c), respectively. The blue dashed and red dotted lines represent the upper bounds based on the selectivity-permeability tradeoff [27, 28].

Figure 8 presents the analysis for He/N₂ separation. In Figure A1 (f), the 6FDA, PMDA and BPDA dianhydrides and the DATRI, HMTDP, 6FmDA-DM, mTrMPD and pTeMPD diamines are selected for further analysis due to the comparatively higher permeability. According to Figure 8, the all copolyimides fall below even the 1991 bound for He/N₂ separation. Although the 6FDA, PMDA and BPDA dianhydrides are above the upper bound in Figure A1 (f), they perform poorly when combined with other monomers to yield copolyimides. With respect to diamines, copolyimides constituted from 6FmDA-DM, which have been reported by two studies in literature [61, 68], offer higher selectivity consistently in Figures 8 (a) – (c). It is worth noting that the predicted and experimental He permeability and He/N₂ selectivity values of PTPDA-6FmDA-DM (pink star in Figure 8 (a)) are exactly same.

4. Conclusions and Recommendations

The volume-based group contribution approach proposed by Robeson et al. [1] is reutilized for the extended dataset of polyimide and copolyimide structures to predict gas transport characteristics like permeability and selectivity of He, H₂, O₂, N₂, CO₂ and CH₄. Comparisons between the predicted and experimental data show that the average percent relative error is between 9.2% and 21.2% for permeability, and 12.7% and 20.8% for selectivity, which are similar to those by Robeson et al. [1, 18] despite a much larger number of polymers considered. The improvement is due to the (i) use of larger subunits which not only account for specifications of the whole chemical structure but also the spatial organization of the molecules, (ii) means of accounting for the contribution of the subunits based on molar volume rather than empirical factors, (iii) the expanded database, and (iv) the focus on a particular polymer class like polyimide and copolyimide rather than a wide range of polymers.

High-performing subunits are identified after screening through those available in literature, then used to combine into new copolyimides, whose performance are evaluated based on comparing with the selectivity-permeability trade-off bound [27, 28]. The separation of the commercially relevant gas pairs, namely, O₂/N₂, CO₂/CH₄, H₂/CO₂, H₂/CH₄, CO₂/N₂ and He/N₂, are used for the assessment. The results show that a judicious selection and combination of existing high-performing monomers is beneficial for exceeding the selectivity-permeability trade-off bound for O₂/N₂, CO₂/CH₄, H₂/CO₂ and H₂/CH₄ separation applications, whereas novel monomers and molecular design approaches are needed for CO₂/N₂ and He/N₂ separation applications. It should be noted that all three monomers constituting the copolyimide influence the resulting performance, as evident in the scatter of data when only two high-performing monomers were chosen while the third was

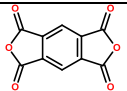
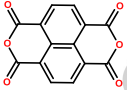
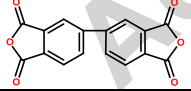
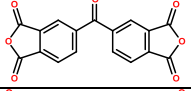
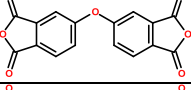
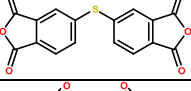
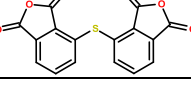
random. The predicted data points above the trade-off bounds are recommended for synthesis and validation of predictions. Summarized below are some monomer structures that can be easily designed to enhance the performance of copolyimide membranes:

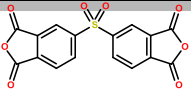
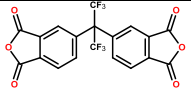
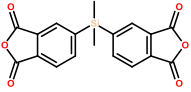
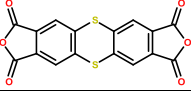
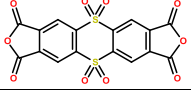
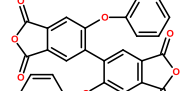
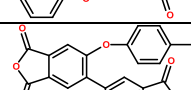
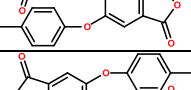
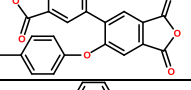
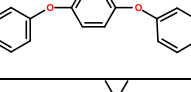
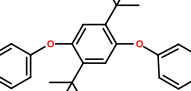
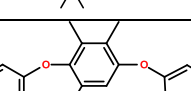
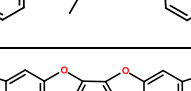
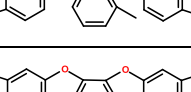
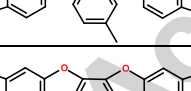
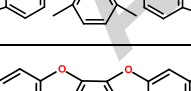
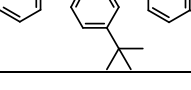
- Sulphone-containing monomers, which have been highlighted in the literature due to their high sorption capacity, are also seen to perform well here in gas separation applications. While the DSDA monomer is advantageous in H_2/CH_4 , CO_2/N_2 , and CO_2/CH_4 separations, pTDPA is beneficial in CO_2/N_2 and O_2/N_2 separations, and mTDPA and DDBT in O_2/N_2 and H_2/CO_2 separations. By using sulphone groups in targeted molecular designs, it is possible to further improve performances.
- The widely known and used mTrMPD and pTeMPD monomers in the literature also exhibit their high permeability capacity here as well, due to the steric hindrance of the methyl side groups which lead to the increase in free volume and hence in permeability. The other monomers with methyl side groups are HMTPD and TMBDA, which have three and two phenyl rings respectively with two methyl groups in each phenyl. While the HMTPD outperforms in many separation applications like O_2/N_2 , H_2/CH_4 , CO_2/N_2 , and He/N_2 , TMBDA is successful in CO_2/CH_4 and CO_2/N_2 separations.
- The other well-known group of monomers is the ones used in thermally rearranged polymers which are promising in many gas separation applications due to their interconnected micro volumes and distinctive free volume morphologies. The monomers used in the precursor of thermally rearranged polymers demonstrate their importance here as well in H_2/CO_2 (namely, bis-APAF) and H_2/CH_4 (namely, mHAB) separations.
- The use of contorted monomers like spiro-centered (polymers of intrinsic microporosity (PIMs)) or bridged bicyclics (tritycene, ethanoanthracene and Tröger's base) are recently gaining much attention in membrane-based gas separation area due to the resulting highly ultramicroporous, solution-processable polymers [69]. In this study, the spiro-centered FPMSD performs well in O_2/N_2 and CO_2/CH_4 separations, and FBP in CO_2/CH_4 separation application, probably due to the spiro-center feature enabling ultramicroporosity. Owing to bridged bicyclics, DATRI shows up as a promising monomer in all separation applications studied except CO_2/CH_4 .

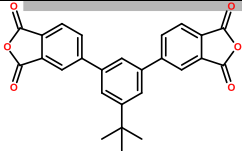
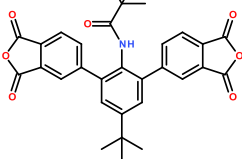
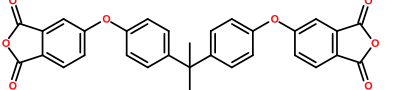
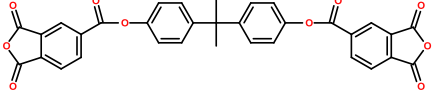
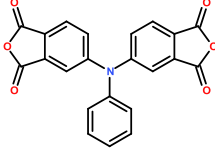
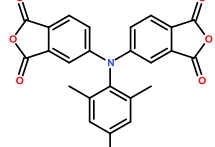
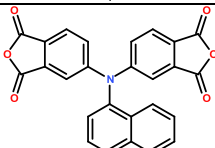
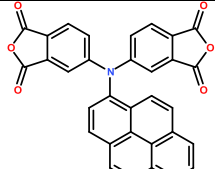
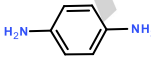
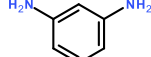
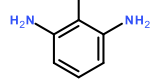
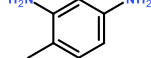
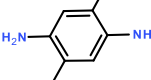
This study presents a method for enhanced predictions of the perm-selectivity behavior of the current dataset and also other novel monomers used in the constitution of polyimides or copolyimides. For a new polyimide synthesized with a novel monomer, if gas permeability coefficients are measured for a gas pair studied here, it is straightforward to predict the performance when the monomer is combined with a range of different monomer structures at different ratios. This will be valuable in

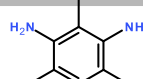
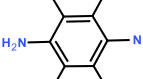
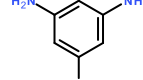
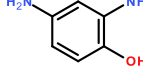
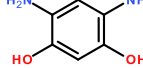
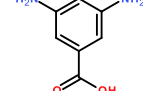
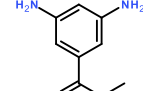
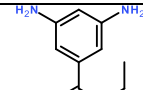
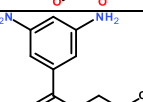
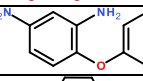
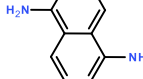
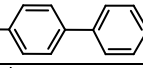
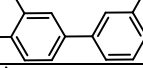
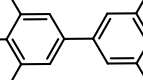
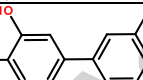
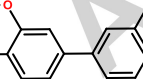
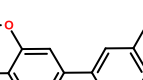
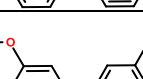

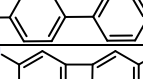
leading more systematic experimental studies. Besides being beneficial for novel polymeric monomers, this fast screening method is also important in selecting the continuous phase for mixed-matrix membranes. Finally, the use of group contribution methods is a more advantageous polymer screening approach than the molecular simulation techniques for membrane based gas separation, since the latter necessitate much more time to even characterize one structure. Moreover, in spite of the recent progress in molecular simulation techniques to calculate the sorption properties of polymers, diffusion coefficients calculated by using simulation tools are not in good agreement with experimental properties in the literature, possibly due to the limited time span and/or ensemble size of the simulations, hence the statistical reliability of their results are poor [70].

Table 1. Predicted permeability data for structural units along with their molar volume comprising the group contribution approach

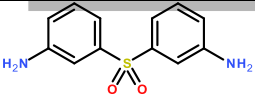
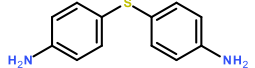
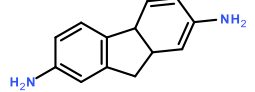
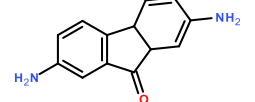
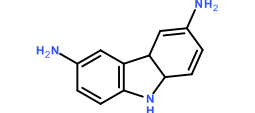
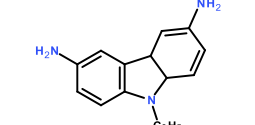
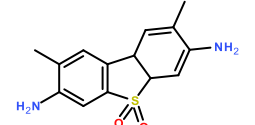
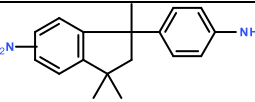
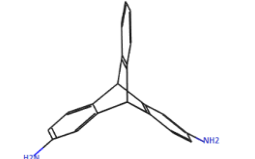
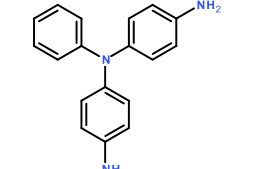
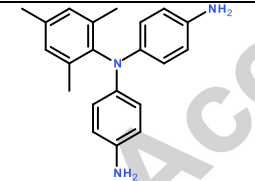
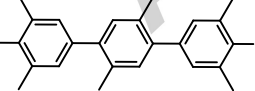
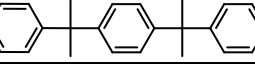
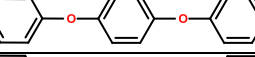
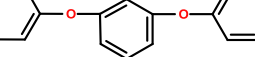
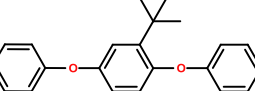
Chemical structures of subunits	Abbreviation	Molecular Volume (\AA^3) of subunits	Permeability (Barrer*) contribution of subunits					
			He	H ₂	O ₂	N ₂	CO ₂	CH ₄
	PMDA	157.47	—	—	0.1879	0.0385	3.7030	0.0120
	NTDA	200.39	—	769.8881	0.6744	1.0672	13.0929	0.0349
	BPDA	229.38	26.7410	22.6364	0.0655	0.0030	0.3772	0.0025
	BTDA	250.19	21.0919	19.1526	0.0466	0.0026	0.2810	0.0013
	ODPA	241.43	24.0946	20.5754	0.0600	0.0031	0.3028	0.0011
	pTDPA	249.60	—	—	2.4182	0.0758	20.2970	—
	mTDPA	248.69	—	—	4.7588	0.2771	44.9820	—

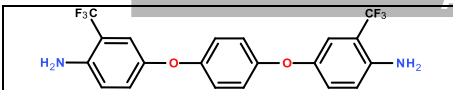
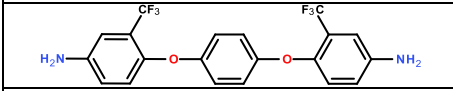
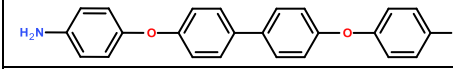
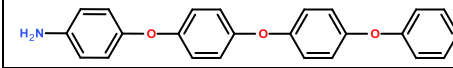
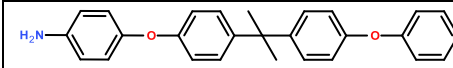
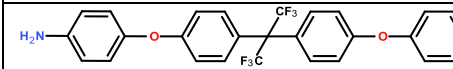
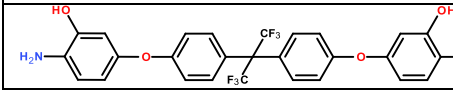
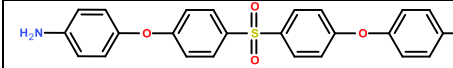
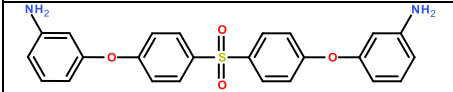
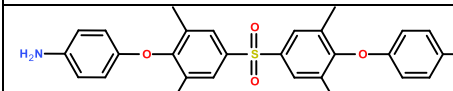
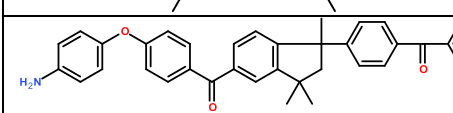
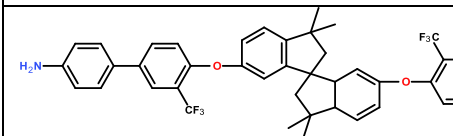
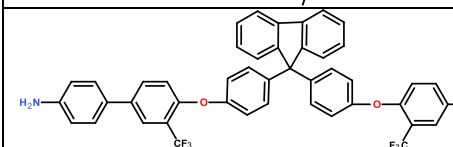
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	6FDA	313.7 7	251.3 617	366.4 412	3.636 4	0.318 9	21.93 40	0.134 5
	SiDA	292.8 1	—	—	0.630 0	0.023 5	2.628 8	0.046 8
	TADA	256.2 2	—	75.96 26	0.458 6	0.025 8	4.334 2	0.027 1
	TADAT O	290.1 5	—	122.1 497	—	—	6.273 2	0.063 4
	A-BPDA	389.7 2	—	—	5.283 5	0.673 4	62.74 97	0.906 6
	B-BPDA	423.9 4	—	—	8.107 9	1.385 3	120.4 646	2.316 4
	C-BPDA	526.0 4	—	—	21.58 02	4.196 5	237.7 246	5.884 1
	HQDPA	319.2 9	—	15.30 26	0.075 8	0.005 1	0.562 1	0.003 1
	DTBHQ DPA	454.5 6	—	241.8 022	5.677 5	0.645 3	27.90 19	0.812 3
	TMHQD PA	370.9 6	57.30 61	91.23 60	0.843 3	0.075 0	6.827 2	0.058 8
	3MCAD PA	336.1 5	13.97 88	13.13 09	0.050 0	0.002 5	0.622 5	0.001 6
	4MCAD PA	336.3 9	11.77 21	14.20 89	0.044 4	0.002 2	0.427 2	0.001 3
	DMCAD PA	353.2 5	32.82 76	36.55 65	0.202 7	0.011 9	2.493 7	0.008 8
	TBCAD PA	388.8 2	32.51 09	58.41 32	0.527 9	0.040 4	3.739 2	0.034 5
	TBMCA DPA	404.7 8	45.02 23	47.58 21	0.425 7	0.030 2	4.113 3	0.021 4
	TPDA	300.3 3	—	—	0.608 5	0.041 4	4.028 8	0.032 1

	BTPDA	317.3 3	212.1 371	10.90 51	0.681 1	0.006 8	32.79 53	0.556 9	
	PTPDA	416.3 1	122.9 389	—	3.429 7	0.476 8	26.90 59	0.630 2	
	BPADA	443.3 8	—	26.13 79	0.448 7	0.040 7	3.275 4	0.040 8	
	BTAPDA	482.2 1	—	—	0.169 7	0.012 7	—	—	
	DCPAN	317.6 4	—	—	0.245 5	0.034 2	3.289 5	0.079 6	
	DCPAN-M	368.8 7	—	—	0.827 1	0.099 0	11.03 55	0.290 9	
	DCPAN-N	361.1 1	—	—	0.523 4	0.101 0	5.666 6	0.249 1	
	DCPAN-P	420.1 1	—	—	0.619 7	0.096 2	6.390 1	0.202 3	
Chemical structures of subunits					Permeability (barrer*) contribution of subunits				
Diamines	Abbreviation	Molecular Volume (Å³) of subunits	He	H₂	O₂	N₂	CO₂	CH₄	
	pPDA	78.85	—	0.008 2	3.055 5	14.42 93	5.334 3	1.000 0	
	mPDA	78.61	0.071 0	0.007 1	0.834 9	1.711 8	0.587 9	0.980 3	
	2,6-DAT	96.04	6.273 3	1.665 5	240.1 804	263.0 960	170.9 362	155.9 783	
	2,4-DAT	96.81	—	0.455 3	75.39 17	131.4 566	222.9 482	284.9 436	
	pDiMPD	113.7	—	5.340 5	490.0 59	940.6 82	268.4 19	327.5 35	

	mTrMPD	132.3 6	417.5 698	275.8 99	17702 8.5	59475 6.4	50236 2.3	16977 24
	pTeMPD	148.4	536.6 203	1260. 998	17004 5.0	51058 2.2	15784 9.4	78465 4.3
	3,5-DBTF	111.7 3	—	0.340 6	31.86 92	45.05 51	20.83 51	13.38 20
	DAP	86.87	0.207 5	0.010 6	—	—	1.000 0	0.071 6
	DAR	95.04	0.138 1	0.013 3	0.301 9	0.217 9	0.330 0	0.017 9
	DABA	106.2 3	0.441 7	0.372 5	2.130 5	0.830 6	1.890 1	0.507 8
	MDABA	125.0 2	—	0.432 6	5.105 9	4.699 0	9.411 4	—
	EDABA	142.7 1	—	2.066 7	49.94 99	36.81 24	59.54 04	—
	PFDABA	306.2	—	—	—	—	281.3 289	43.90 68
	PDAB	150.4 8	1.630 7	1.006 7	7.820 1	38.70 34	12.53 52	2.714 9
	DANT	122.1 5	—	—	44.40 56	41.20 67	—	—
	BDA	151.1 6	—	0.011 9	0.012 6	0.007 0	—	—
	DMBDA	184.7 9	—	1.715 1	0.641 6	1.410 7	—	—
	TMBDA	220.5 1	22.79 40	44.30 03	163.8 387	147.7 653	494.7 822	132.3 280
	pHAB	166.6 2	2.115 3	0.525 3	0.336 0	—	2.578 0	0.026 1
	pHAB-M	202.1 9	8.861 3	1.265 2	—	1.240 8	17.10 73	1.235 5
	pHAB-Ac	241.9	—	1.603 6	1.948 6	0.822 0	3.857 3	0.587 3
	pHAB-PrAc	276.0 5	—	3.400 8	6.008 9	3.212 4	12.72 50	4.291 6
	pHAB-PAc	343.7 7	—	35.41 16	59.66 12	27.85 29	136.2 813	54.35 17
	mHAB	166.6 3	3.925 7	0.607 4	0.406 1	0.306 5	4.339 7	0.016 5

	mHAB-Ac	229.6 3	—	2.301 3	4.556 3	2.050 0	8.924 7	1.671 1
	MDA	168.6 8	0.724 6	0.596 8	1.363 5	—	9.048 9	1.429 0
	DMMD A	203.1 4	2.158 9	3.132 6	4.439 4	1.195 6	11.08 24	0.832 9
	DCMDA	197.0 4	1.262 8	0.749 7	1.096 6	0.395 1	3.043 5	0.169 8
	DMoMD A	220.8 7	—	—	2.048 0	0.471 0	7.422 2	0.441 5
	DCMDA 2	197.0 4	0.363 6	—	0.148 8	0.047 3	0.291 8	0.014 1
	DBrMD A	204.1 3	0.367 1	—	0.135 7	0.041 5	0.257 2	0.013 1
	DFMDA	178.8 1	0.421 2	—	0.389 3	0.237 6	0.862 8	0.108 6
	APAP	203.6 9	—	1.173 4	2.028 6	0.868 4	3.541 4	0.453 6
	IPDA	203.2 9	10.20 22	2.841 0	16.11 77	11.22 91	45.88 40	10.73 26
	6FpDA	233.6 5	68.90 62	66.64 78	417.4 904	156.6 830	621.5 505	111.9 928
	6FmDA	233.4 9	8.872 0	—	1.808 8	0.510 3	1.964 5	0.093 9
	6FmDA-DM	267.5 7	59.98 10	—	143.8 780	45.30 39	—	—
	Bis-APAF	249.6 2	—	13.47 22	11.73 24	5.238 6	5.162 2	0.274 3
	Bis-APAF-Ac	324.4 8	—	7.086 0	6.566 1	2.429 9	11.54 70	1.061 1
	mODA	160.4	—	0.051 0	0.061 2	0.009 1	0.048 4	0.003 9
	mpODA	160.1 8	—	0.162 2	0.432 2	0.076 8	0.416 2	0.067 5
	pODA	159.4 8	0.327 2	0.493 3	1.596 2	1.133 0	3.516 2	0.485 2
	ODA-CF3	192.1 7	11.83 12	7.657 4	25.75 91	17.55 76	—	—
	ODA-OMe	214.2 9	1.885 7	1.209 6	0.699 3	0.703 5	—	—
	pDDS	187.1 3	1.366 9	1.693 9	3.827 7	2.517 5	11.82 83	1.411 1

	mDDS	186.9 2	—	0.045 1	0.032 2	0.005 8	0.027 3	0.002 7
	SDA	169.6 4	—	—	—	—	2.045 4	0.214 4
	DAF	158.0 3	25.07 34	—	—	—	69.01 03	13.52 49
	DAFO	159.9 1	—	—	0.985 2	0.382 3	—	—
	CDA	151.5 7	—	1.283 6	6.947 3	3.953 9	10.21 33	1.628 9
	ECDA	188.0 7	—	6.593 6	42.28 75	29.97 20	69.53 97	30.76 79
	DDBT	176.4 6	99.43 00	55.87 58	—	—	505.1 413	799.8 884
	DAPI	243.9 1	27.68 47	38.86 31	76.95 82	28.68 66	254.6 201	40.57 93
	DATRI	238.7 5	144.6 996	161.2 314	881.5 087	568.6 312	3204. 116	952.7 985
	DATPA	237.1 5	—	7.092 3	14.62 45	8.029 1	37.00 03	7.843 5
	DATPA-M	288.6 8	—	—	112.1 892	35.25 62	220.7 685	59.88 67
	HMTPD	325.2 6	228.8 882	363.0 281	994.6 773	665.0 760	3800. 855	1263. 891
	BIS-P	326.8 2	4.670 6	—	6.604 1	1.425 5	19.61 71	—
	TPE-Q	240.1 8	2.925 2	1.476 0	4.213 6	2.201 7	7.481 8	2.151 7
	TPE-R	240.6 2	—	—	—	—	0.727 1	0.055 0
	TPE-M	309.2 7	—	—	5.428 3	1.278 8	—	—

	TPE-mF	299.9	—	20.98 80	32.85 78	20.25 78	84.32 27	14.97 60
	TPE-oF	304.6 1	—	10.82 12	20.48 47	11.56 17	42.69 34	7.847 3
	BAPB	311.8 7	—	—	—	—	7.533 0	0.639 3
	BAPE	321.5 7	1.197 6	—	0.741 9	0.270 8	2.913 1	0.239 6
	BAPP	364.7 8	3.372 0	5.076 9	2.493 8	0.912 4	11.08 54	0.764 7
	BAPHF	394.2 8	16.26 27	12.45 81	11.41 35	2.620 6	26.69 95	1.820 3
	BAPHF- OH	410.8 7	10.75 62	4.205 0	16.59 51	7.425 5	0.024 0	0.126 7
	BAPS	348.2 6	2.248 4	—	1.147 0	0.368 2	4.010 4	0.265 6
	BADS	348.2	—	—	13.41 57	4.516 6	0.682 5	0.032 5
	TMBAP S	416.2 1	—	—	7.813 0	1.535 3	—	—
	TMPI	587.6 8	—	—	2.658 2	0.710 6	—	—
	FPMSD	651.3 5	—	—	96.07 90	9.889 7	95.35 33	2.862 1
	FBP	671.9 3	—	—	37.02 52	8.326 9	121.5 607	8.370 4

*barrer= 10^{-10} cm³(STP).cm/(cm².s.cmHg)

Abbreviations:**Dianhydrides**

PMDA	: pyromellitic dianhydride
NTDA	: 1,4,5,8-naphthalene tetracarboxylic dianhydride
BPDA	: 3,3',4,4'-biphenyltetracarboxylic dianhydride
BTDA	: 3,3',4,4'-benzophenonetetracarboxylic dianhydride
ODPA	: 4,4'-oxydiphthalic anhydride
pTDPA	: 3,3',4,4'-thiaphthalic dianhydride
mTDPA	: 2,2',3,3'-thiaphthalic dianhydride
DSDA	: 3,3',4,4'-diphenylsulfone tetracarboxylic dianhydride
6FDA	: 4,4'-(hexafluoroisopropylidene)diphthalic anhydride
SiDA	: bis (phthalic anhydride) dimethylsilane
TADA	: thianthrene-2,3,7,8-tetracarboxylic dianhydride
TADATO	: thianthrene-2,3,7,8-tetracarboxylic dianhydride-5,5,10,10-tetraoxide
A-BPDA	: 2,2'-diphenoxy-4,4',5,5'-biphenyltetracarboxylic dianhydride
B-BPDA	: 2,2'-di(p-methylphenoxy)-4,4',5,5'-biphenyltetracarboxylic dianhydride
C-BPDA	: 2,2'-di (p-tert-butylphenoxy)-4,4',5,5'-biphenyltetracarboxylic dianhydride
HQDPA	: 1,4-bis(3,4-dicarboxyphenoxy)benzene dianhydride
DTBHQDPA	: Dianhydride J in [71]
TMHQDPA	: Dianhydride H in [71]
3MCADPA	: Dianhydride A in [71]
4MCADPA	: Dianhydride B in [71]
DMCADPA	: Dianhydride C in [71]
TBCADPA	: Dianhydride D in [71]
TBMCADPA	: Dianhydride E in [71]
TPDA	: 3,4,3'',4''-m-terphenyltetracarboxylic dianhydride
BTPDA	: 5'-t-butyl-m-terphenyl-3,4,3'',4''-tetracarboxylic acid dianhydride
PTPDA	: 5'-t-butyl-2'-pivaloylimino-3,4,3'',4''-m-terphenyltetracarboxylic dianhydride
BPADA	: 4,4'-(4,4'-isopropylidenediphenoxy)bis(phthalic anhydride)
BTAPDA	: 2,2'-bis(p-trimellitoxylphenyl) propane dianhydride
DCPAN	: n,n-bis(3,4-dicarboxyphenyl)aniline dianhydride
DCPAN-M	: n,n-bis(3,4-dicarboxyphenyl)-2,4,6-trimethylaniline dianhydride
DCPAN-N	: n,n-bis(3,4-dicarboxyphenyl)-1-aminonaphthalene dianhydride
DCPAN P	: n,n-bis(3,4-dicarboxyphenyl)-1-aminopyrene dianhydride

Diamines:

pPDA	: 1,4-phenylenediamine
mPDA	: 1,3-phenylenediamine
2,6-DAT	: 2-methyl-1,3-phenylenediamine
2,4-DAT	: 2,4-diaminotoluene
pDiMPD	: 2,5-dimethyl-1,4-phenylenediamine
mTrMPD	: 2,4,6-trimethyl-1,3-phenylene-diamine
pTeMPD	: 2,3,5,6-tetramethyl-1,4-phenylenediamine
3,5-DBTF	: 3,5-diaminobenzotrifluoride
DAP	: 2,4-diaminophenol di hydroxyl
DAR	: 4,6-diaminoresorcinol di hydroxyl
DABA	: 3,5-diaminobenzoic acid
MDABA	: methyl 3,5-diaminobenzoate
EDABA	: ethyl 3,5-diaminobenzoate
PFDABA	: 2-(perfluorohexyl)ethyl-3, 5-diamino benzoate
PDAB	: 1-phenoxy-2,4-diaminobenzene
DANT	: 1,5-naphthalene
BDA	: benzidine
DMBDA	: 3,3'-dimethylbenzidine
TMBDA	: 3,3',4,4'-tetramethyl- benzidine
pHAB	: 3,3'-dihydroxybenzidine
pHAB-M	: 3,3'-dimethoxybenzidine
pHAB-Ac	: 3,3'-dihydroxy-4,4'-diamino-biphenyl-acetate
pHAB-PrAc	: 3,3'-dihydroxy-4,4'-diamino-biphenyl- propanoate

pHAB-PAc	: 3,3'-dihydroxy-4,4'-diamino-biphenyl-pivalate
mHAB	: 3,3'-diamino-4,4'-dihydroxybiphenyl
mHAB-Ac	: 3,3'-diamino-4,4'-dihydroxybiphenyl-acetate
MDA	: methylenedianiline
DMMDA	: 4,4'-methylene-bis(2-methylaniline)
TMMDA	: tetramethylmethylene dianiline
DCMDA	: 4,4'-methylene bis(2-chloroaniline)
DMoMDA	: 3,3'- dimethoxy-4,4'- methylenedianiline
DCMDA2	: 4,4'-methylene bis(3-chloroaniline)
DBrMDA	: di brominated 4,4'-methylenedianiline
DFMDA	: 4,4'-methylene bis(3-flouroaniline)
APAP	: 2-(3-amino-(4-phenyl)-2-aminophenyl)propane
IPDA	: isopropylidenedianiline
6FpDA	: 4,4'-(hexaflouroisopropylidene)-dianiline
6FmDA	: 2,2'-(hexaflouroisopropylidene)-dianiline
6FmDA-DM	: 2,2-bis-(3-amino-4-methylphenyl)hexafluoro-propane
Bis-APAF	: 2,2'-bis(3-amino-4-hydroxyphenyl)-hexafluoropropane
Bis-APAF-Ac	: 2,2'-bis(3-amino-4-hydroxyphenyl)-hexafluoropropane-acetate
mODA	: 3,3'-oxydianiline
mpODA	: 3,4'-oxydianiline
pODA	: 4,4'-oxydianiline
ODA-CF3	: 2-trifluoromethyl-4,4'-diaminodiphenyl ether
ODA-OMe	: 2-methoxy-5,4'-diaminodiphenyl ether
pDDS	: 4,4'-Diaminodiphenyl sulfone
mDDS	: 3,3'-Diaminodiphenyl sulfone
SDA	: 4,4'-diaminodiphenylsulfide
DAF	: 2,7-fluorenediamine
DAFO	: 2,7-diaminofluorenone
CDA	: 3,6-diaminocarbazole
ECDA	: n-ethyl-3,6-diaminocarbazole
DDBT	: 3,7-diamino-2,8-dimethyldibenzothiophene sulfone
DAPI	: 5(6)-amino-1-(4' aminophenyl)-1,3,-trimethylindane
DATRI	: 2,6-diaminotriptycene
DATPA	: 4,4'-diaminotriphenylamine
DATPA-M	: 4,4'-diamino-2'',4'',6''-trimethyltriphenylamine
HMTPD	: 1,3,3',3'',5,5',6''-hexamethyl-(1,1',1''-triphenyl)-4,4'-diamine
BIS-P	: 4,4'-[(1,4-phenylene)dipropene-2,2-diyl]dianiline
TPE-Q	: 1,4-bis(4-amino-phenoxy)benzene
TPE-R	: 1,4-bis(3-amino-phenoxy)benzene
TPE-M	: 1,4-bis(4-aminophenoxy)2-tert-butylbenzene
TPE-mF	: 1,4-bis(4-amino-3-trifluoromethylphenoxy)benzene
TPE-oF	: 2,3-bis(4-amino-3-trifluoromethylphenoxy)benzene
BAPB	: 4,4'-bis (4-aminophenoxy) biphenyl
BAPE	: bis[4-(4-aminophenoxy)phenyl]ether
BAPP	: 2,2-bis [4-(4-aminophenoxy)phenyl] propane
BAPHF	: 2,2-bis(4-(4-aminophenoxy) phenyl) hexafluoropropane
BAPHF-OH	: 2,2-bis(4-(4-amino-3-hydroxyphenoxy)phenyl)- hexafluoropropane)
BAPS	: 2,2-bis [4-(4-aminophenoxy) phenyl] sulfone
BADS	: 4,4'- bis(3-aminophenoxy)diphenyl sulfone
TMBAPS	: 3,3',5,5'-tetramethyl-bis[4-(4-aminophenoxy)phenyl]sulfone
TMPI	: in ref. [72]
FPMSD	: 6,6-bis-[2-trifluoromethyl 4-(4-aminophenyl)phenoxy]-3,3,3,3-tetramethyl-1,1-spirobiindane
FBP	: 4,4'-bis-((2'-trifluoromethyl-4'-(4''-aminophenyl) phenoxy)-9-fluorenylidene

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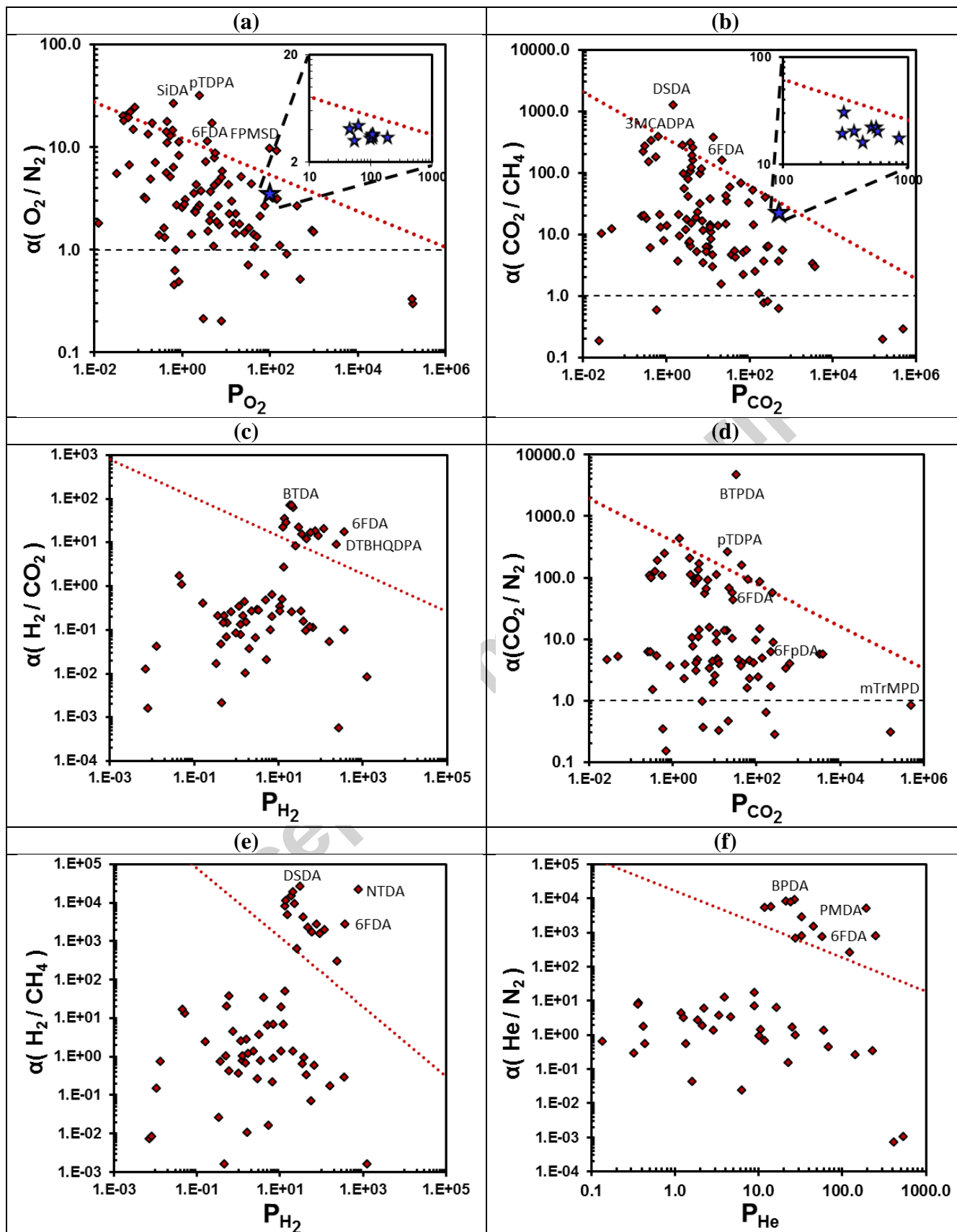


Figure A1. Predicted selectivity versus permeability diagrams for the various subunits used for the separation applications of (a) O₂/N₂, with the inset displaying the scatter of the transport properties of 6FDA-mTrMPD from nine experimental studies [29-37]; (b) CO₂/CH₄, with the inset displaying the scatter of the transport properties of 6FDA-mTrMPD from eight experimental studies [29-36]; (c) H₂/CO₂; (d) CO₂/N₂; (e) H₂/CH₄; and (f) He/N₂. The red dotted line represents the 2008 upper bound based on the selectivity-permeability tradeoff [28]. Note that the data points represent subunits instead of polymers.

highlights

Advances group contribution study based on molar volume contributions of subunits
Database screened to identify the high-performing subunits to make up copolyimides
Enhanced agreement between experimental and predicted transport properties
Some gas separation properties cannot be further improved while others can
Predictions indicate that polymers that exceed the trade-off bound are possible

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