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2 **Green recycling methods to treat lithium-ion batteries e-waste: A**  
3 **circular approach to sustainability**  
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34 **Abstract:**

35 E-waste generated from end-of-life spent lithium-ion batteries (LIBs) is increasing at a  
36 rapid rate owing to the increasing consumption of these batteries in portable electronics,  
37 electric vehicles, and renewable energy storage worldwide. On the one hand, landfilling and  
38 incinerating LIBs e-waste poses environmental and safety concerns owing to their constituent  
39 materials. On the other hand, scarcity of metal resources used in manufacturing LIBs and  
40 potential value creation through the recovery of these metal resources from spent LIBs has  
41 triggered increased interest in recycling spent LIBs from e-waste. State of the art recycling of  
42 spent LIBs involving pyrometallurgy and hydrometallurgy processes generates considerable  
43 unwanted environmental concerns. Hence, alternative innovative approaches towards the  
44 green recycling process of spent LIBs are essential to tackle large volumes of spent LIBs in an  
45 environmentally friendly way. This review focuses on such evolving techniques for spent  
46 LIBs recycling based on green approaches, including bioleaching, waste for waste approach,  
47 and electrodeposition. Furthermore, we discuss ways to regenerate strategic metals post-  
48 leaching, efficiently re-process extracted high-value materials, and reuse them in applications  
49 including electrode materials for new LIBs. This review highlights the concept of "circular  
50 economy" through closed-loop recycling of spent LIBs achieved through green-sustainable  
51 approaches.

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54 **Keywords:** Battery e-waste, recycling, electrodeposition, bioleaching, Circular economy,  
55 Metal-organic framework (MOF)

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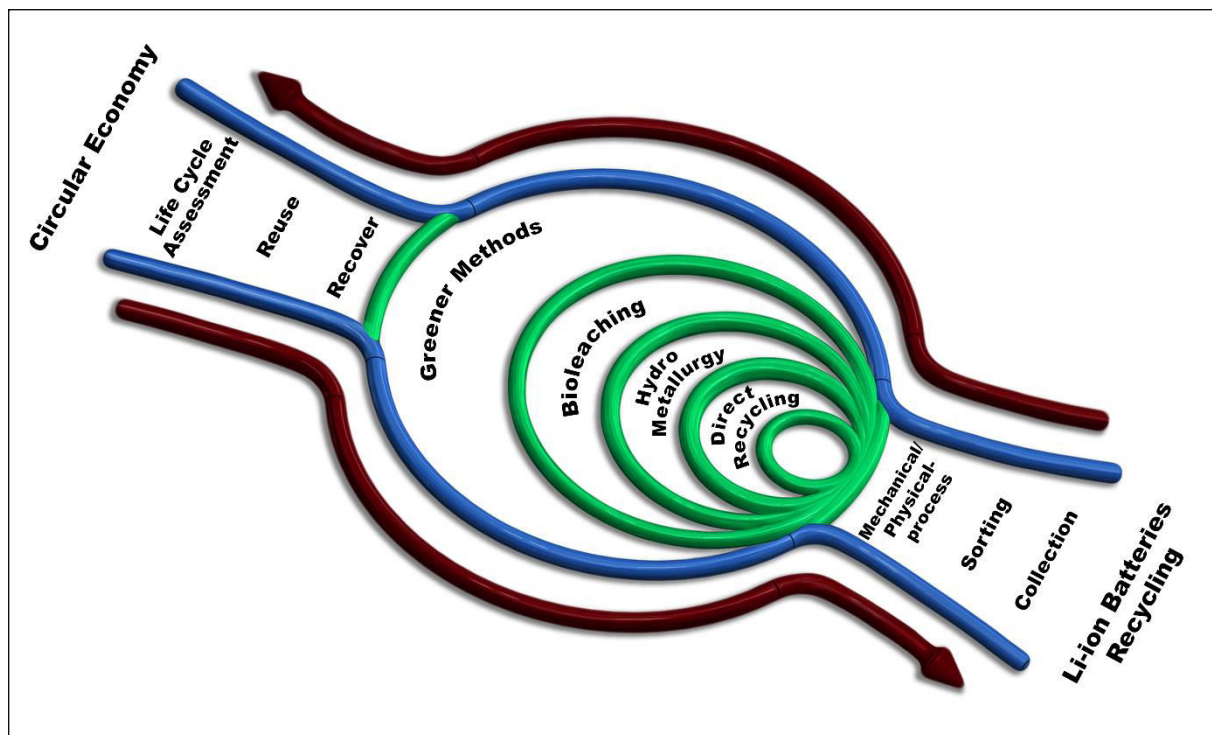
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## 68 Abbreviations:

SS	Stainless steel
Pb-8 Sb	Impure Sb, containing up to 8% Pb
SCE	Saturated calomel electrode
RT	Room temperature
RE	Reference electrode
CE	Counter electrode
WE	Working electrode
SOFC	Solid oxide fuel cells
CAM	Cathode active material
ILs	Ionic liquids

W4W	Waste for Waste
EVs	Electric vehicles
LIBs	Lithium-ion batteries
FVW	Fruit and Vegetable Waste
LCO	Lithium cobalt oxide
LMO	Lithium Manganese oxide
NMC	Lithium Nickel manganese cobalt oxide
OP	Orange peel
E-waste	Electronic waste
ORP	Oxidation-reduction potential

## 69 **1. Introduction**

70 Advances in electric vehicles (EVs), portable electronic devices, and renewable grid  
71 energy storage systems have increased the demand for lithium-ion batteries (LIBs) with  
72 higher energy storage capacities, faster charging capabilities, and increased cycle life. [1-4]  
73 Global lithium-ion battery market is estimated to reach \$95 billion by 2025, with an expected  
74 compound annual growth rate (CAGR) of around 16% that is forecasted to lead to around 11  
75 million metric tons of spent LIBs waste generated by 2030. [5] The volume of discarded/spent  
76 LIBs is predicted to rise by 59 % from 10,700 tons in 2012 to 464,000 tons in 2025. [6]  
77 Presently, less than 6% of spent LIBs waste are recycled worldwide, while most of them end  
78 up in landfills posing environmental concerns as these spent LIBs consist of toxic metals (Co,  
79 Mn, Ni) and flammable electrolytes that may react with water releasing harmful gases. [7-9]  
80 These piles of spent LIBs also represent valuable secondary resources of critical elements  
81 (such as lithium, manganese, cobalt, nickel, etc) that are of geopolitical supply risk fuelled by  
82 their growing demand in new LIBs production. Interestingly, the constituents elements

83 employed in LIB manufacturing are only abundant and mined in selected geographical  
84 locations worldwide. For instance, the Republic of Congo produces about 60% of the world's  
85 cobalt, Australia and Chile produce 80% of lithium, and China produces 70% of graphite.[10]  
86 However, these critical elements can potentially be recovered from spent LIBs, thus avoiding  
87 the depletion of finite resources and reducing over-reliance on classical mining to maintain the  
88 supply chain.[6-9] Recycling of spent LIBs waste, on the one hand, would reduce and/or  
89 eliminate potential environmental impacts and, on the other hand, would recover and reuse  
90 valuable metal recycling of resources, thus promoting a circular economy approach based on  
91 sustainable LIBs development industries.

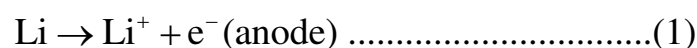
92 State-of art industrial processes for spent LIBs recycling are mainly based on (i) pyro-  
93 metallurgy and/or (ii) hydrometallurgy approaches. Pyrometallurgy involves melting spent  
94 LIBs at very high temperatures (>1000 degC) and recovering metal resources from the  
95 remaining slag.[11] Pyrometallurgy is (i) energy/cost-intensive, (ii) leads to loss of metals in  
96 slag, and (iii) involves hazardous gaseous emissions, thus not environmentally friendly.  
97 Hydrometallurgy involves treating spent LIBs in concentrated corrosive acids to dissolve and  
98 extracts metals. Hydrometallurgy operates at lower temperatures and offers higher metal  
99 recovery efficiency than pyrometallurgy (Table 1). However, multiple complex treatment  
100 steps and selectivity of strong acid reagents that lead to gaseous emissions and wastewater  
101 production poses environmental concerns of hydrometallurgy. [12-17] In an effort to lower  
102 the energy and environmental footprints, novel green recycling approaches towards spent  
103 LIBs have been investigated to achieve higher recycling efficiency and reuse of critical  
104 elements. This review presents a summary of greener and environmentally friendly recycling  
105 approaches of spent LIB. We address the detailed assessment of battery recycling process  
106 starting from pre-treatment, such as sorting, dismantling, and shredding of LIBs followed by  
107 metal extraction processes from black mass and their regeneration and reusability.

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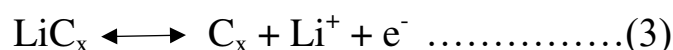
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110 **2. Lithium-ion batteries types and pre-treatment**

111 Primary non-rechargeable lithium batteries consist of lithium metal anode and metal  
 112 oxide cathode in which the following chemical reactions occur at the anode (Equation 1) and  
 113 MnO<sub>2</sub> cathode (Equation 2)



115 Secondary rechargeable lithium-ion batteries consist of lithium containing oxide as a  
 116 cathode, graphite anode, and lithium salt in an organic solvent as electrolyte. During charging  
 117 of these batteries, lithium is removed (deintercalated) from the cathode (LiCoO<sub>2</sub>) and inserted  
 118 (intercalated) into graphite anode. While discharging, the reverse reaction process takes place  
 119 reversibly, as shown in Equation 3, 4. [18-19] The lithium-ion moves in the electrolyte within  
 120 the cell, and the electron moves in the external circuit, providing current.



123 There are different types of lithium-ion batteries based on the constituent cathode,  
 124 anode, and electrolyte materials. The most commercially used anode is graphite and lithium  
 125 titanate. The electrolyte typically is a mixture of lithium containing salts (such as lithium  
 126 hexafluoro phosphate, LiPF<sub>6</sub>) dissolved in organic carbonates (such as ethylene carbonate or  
 127 diethyl carbonate) as solvent. The cathode is generally made up of three classes of materials: a  
 128 layered oxide (e.g., LiCoO<sub>2</sub>, LiNi<sub>0.3</sub>Mn<sub>0.3</sub>Co<sub>0.3</sub>O<sub>2</sub>), a polyanion (e.g., LiFePO<sub>4</sub>), or a spinel  
 129 (e.g., LiMn<sub>2</sub>O<sub>4</sub>). The physio-electro properties of different LIB types are described in Table 2.  
 130 [22-25] Depending on the applications, there are different form factors of LIBs such as  
 131 cylindrical, prismatic, and pouch configurations that employ various packaging materials.

132 Efficient recycling processes should address the recovery, recycling, and reuse of these  
133 packaging materials. Some parameters that should be considered when employing LIBs for  
134 various applications include capacity, power, voltage, charging and discharging rates, cost,  
135 life span, safety, and environmental impact. Currently, LIBs have capacities ranging from 550  
136 mAh to 2.5 Ah for portable and stationary applications and up to 45 Ah or higher for high  
137 power and energy applications. [18-22] With the advancements in LIBs, numerous innovative  
138 approaches have been developed for newer positive (cathode) and negative (anode) electrode  
139 and electrolyte materials. Hence, recycling processes that are being developed should be able  
140 to accommodate these variations in the LIBs constituent chemistry to be able to recover  
141 materials efficiently.

142         Recycling of LIBs consists of several pre-treatment steps such as sorting, discharging,  
143 dismantling, shredding, mechanical-physical process of separation followed by metal  
144 extraction, metal recovery, metal reuse. The waste LIBs collected are manually sorted, and  
145 fully discharged to <0.5V using a salt solution in the preliminary pre- treatment step to  
146 prevent any fire or explosion risk during the shredding process. Mechanical shredding of  
147 spent LIBs consists of crushing and shredding LIBs using duo-directional shredder blades in  
148 an inert atmosphere purged with argon or nitrogen to break apart and shred the batteries with  
149 the casing/packaging materials. The mechanical shredding process occurs in an inert  
150 atmosphere to prevent the presence of oxygen during shredding, which might lead to lithium  
151 reacting violently with oxygen leading to fire risk. The detailed pre-treatment process used in  
152 our facility is shown in **Figure 1**. The shredded materials should be stored in a fume cupboard  
153 or under exhaust suction to remove any toxic electrolyte and volatile organic compounds  
154 (VOCs) after being collected from the drum at the bottom of the mechanical shredder. After  
155 the drying process under exhaust, subsequent pre-treatment processes would include milling,  
156 sieving, magnetic separation, froth flotation, or a combination of these processes would lead

157 to black mass powder. It is necessary to do fine grinding to reduce shredded battery materials  
158 to near micron-sized particles to form black mass powder. Various green recycling approaches  
159 are described in the following sections that are employed on extracted black mass powder  
160 after pre-treatment steps to extract and leach out elements. Pre-treatment steps affect the  
161 quality and constituent of the black mass powder and can affect the metal recovery  
162 efficiencies in the following green recycling approaches.

163

### 164 **3. Greener Recycling Approaches**

#### 165 **3.1. Bioleaching**

166 Bio-hydrometallurgy, as a green technology, is a promising method for metal  
167 extraction from spent LIBs, printed circuit boards (PCBs), and other e-wastes. [26-28] The  
168 bio-hydrometallurgical process has attracted great attention recently because it is a cost-  
169 efficient and eco-friendly alternative to conventional processes such as pyrometallurgy and  
170 hydrometallurgy.[29, 30] The extraction of metals from secondary sources such as ores,  
171 concentrates and recycled or waste materials using microbes, such as bacteria, fungi, and  
172 archaea, is called “bioleaching or bio-hydrometallurgy.” Chemistry, biology, and  
173 metallurgical phenomenon are all involved in this interdisciplinary extraction process.[31- 33]  
174 Bioleaching is used to extract and treat metals from ores and wastes, as well as for reducing  
175 pollution and greenhouse gas emissions.[31-35] In the bioleaching process, microbes act as a  
176 biocatalyst by producing lixivants (leaching agents) such as  $H_2SO_4$  or organic acids through  
177 their metabolism, which can dissolve the metals from their ores and secondary resources such  
178 as LIBs, PCBs, and other e-wastes.[30] The bioleaching process comprises of various groups  
179 of microbes, such as chemolithotrophic prokaryotes, heterotrophic bacteria, and fungi. For  
180 many years, these microbes have been widely used to extract valuable metals (e.g., cobalt,  
181 nickel, manganese, and copper) from ores and other secondary sources.[34, 36-40] In the

182 bioleaching process (explained in **Figure 2**), valuable metals are extracted from waste LIBs  
183 by naturally existing biological microorganisms using their metabolic products.  
184 Microorganism assisted dissolution and recovery of elements from spent LIBs has immense  
185 potential as a green recycling technology because it is safe for the environment, has no  
186 harmful gases emitted, has low operational costs and energy requirements. The aim of spent  
187 LIB recycling employing a green bioleaching process is to extract the metal constituents from  
188 them and reuse them in new LIBs, thus reducing battery waste and in that process reducing  
189 exposure of LIB toxic constituents in the environment.

### 190 **3.1.1 Microbes used in Bioleaching Process**

191 Earlier, bioleaching systems were developed towards the recovery of metals from ores.  
192 In the 1980s, the first commercial bioleaching facility was created to recover copper utilizing  
193 acid-producing acidophilic bacteria such as *A. ferrooxidans* and *A. Thiooxidans*. [41] Later,  
194 when the metal was covered with an intractable covering of metal sulfides, making cyanide  
195 extraction difficult, bioleaching technology was used for gold mining. [42] Metal extraction  
196 from spent batteries has been done using a bioleaching process since the late 1990s. Many  
197 research publications on metal extraction from LIBs using a bioleaching technique have been  
198 published since 2000 and reviewed in detail. [33,34,37,43] The microbes used in the  
199 bioleaching process have evolved over the years and have been categorized into mesophiles  
200 (below 40 °C), moderate thermophiles (45 °C – 70 °C), and thermophiles (70 °C or above)  
201 and fungi (below 35 °C). [37] Bioleaching of spent LIBs can be performed either using single  
202 or multiple microorganisms in combination (consortia) to experiment with the synergistic  
203 effects.

#### 204 *3.1.1.1 Bacteria for LIBs bioleaching*

205 The most extensively studied mesophilic bacteria in LIBs bioleaching are  
206 *Acidithiobacillus ferrooxidans*, *Acidithiobacillus thiooxidans*, and *Leptospirillum*

207 *ferrooxidans*; moderate thermophilic microbes are sulfur-oxidizing *Acidithiobacillus caldus*,  
208 and iron-oxidizing *Leptospirillum ferriphilum*. [30, 34, 44- 46] The bioleaching studies of  
209 LIBs reported using single and mixed bacteria are shown in **Table 3**. The bioleaching process,  
210 aided by the bacteria, converts the metal complex from an insoluble form into water-soluble  
211 metals by bio-oxidation. During this process, the microbes gain energy by rupturing and  
212 breaking LIBs wastes into their constituent metallic complexes. [47] Bioleaching of LIBs  
213 using mesophilic bacteria is usually performed in acidic pH between 1 and 3, at almost room  
214 temperatures of around 30-32 °C, where most of the metal ions are soluble in solution. One of  
215 the critical parameters and challenges in the bioleaching process is the pulp density (w/v) or  
216 referred as solid to liquid ratio (S/L ratio), which controls the viability of microbes in liquid  
217 solution vs the amount of solid black mass from spent LIB. The bioleaching efficiency  
218 decreases considerably with increasing solid content (S/L ratio) because of the alkaline nature  
219 of the spent LIBs and toxic compounds, including electrolytes and binders. [31,32] As seen in  
220 **Table 3**, varying the bacterial pulp density, 0.25-10%, results in different leaching efficiencies  
221 of individual elements such as Li, Co, Ni, Mn.

#### 222 3.1.1.2. Fungi for LIBs bioleaching

223 *Aspergillus niger*, *Penicillium simplicissimum*, and *Penicillium chrysogenum* are the  
224 most studied fungi for bioleaching of LIBs (**Table 3**). [44, 48-59] Fungi-mediated bioleaching  
225 of LIBs usually takes place at a near-neutral pH or alkaline, and the dissolution of the LIB  
226 components increases the pH of the solution.[56] The fungi-mediated bioleaching is  
227 performed by acidolysis, complexolysis (generation of organic acids), redoxolysis, and metal  
228 dissolution occurs at near-neutral or alkaline conditions. The metabolites of organic acid form  
229 a complex with metallic components, and the resulting complex has low toxicity.[49,50]  
230 Fungi-based bioleaching requires carbon-based primary nutrients such as glucose and sucrose  
231 into the leaching solution. Alternatives carbon-based sources such as food-processing wastes,

232 potato processing waste, and sugarcane bagasse have been supplemented as primary nutrients  
233 and studied. [51,54] Bacteria-based bioleaching has been successfully demonstrated at higher  
234 pulp density (10%) as compared to fungi-based (2%) bioleaching Table 3.

235

### 236 **3.1.2 Factors affecting the bioleaching process**

237 The potential of microorganisms and chemical composition of spent LIBs waste  
238 determines the bioleaching process' leaching efficiency. The kinetics of the bioleaching  
239 process can be improved by optimizing the microbe's growth conditions, including  
240 temperature, pH, redox potential, O<sub>2</sub>, and CO<sub>2</sub> supply, growth nutrients, metal toxicity, and  
241 pulp density. [34]

242 The microbial growth depends on the specific nutrient and their dosages.  
243 Concentration and dose of nutrients and microbes are essential to produce metabolites, which  
244 are associated with the metal solubilization of LIBs. *A. ferrooxidans* utilize ferrous salts as  
245 their major nutrition for the production of biogenic sulphuric acid and Fe<sup>3+</sup> ions, and *A.*  
246 *thiooxidan* needs elemental sulfur. Fungi, on the other hand, require sucrose or glucose as a  
247 carbon source, which can be replaced with cost-effective alternatives such as food processing  
248 wastes, potato processing waste, and sugarcane bagasse.[48, 55, 56] An adequate amount of  
249 oxygen supply (1%-10%) is also required for the optimal growth and function of the  
250 microorganism, which can be attained by various methods, including aeration, stirring, or  
251 shaking.[57,58] However, at high pulp densities, the aeration may be less due to limited air  
252 penetration caused by the high viscosity of the solution, thus decreasing the leaching  
253 efficiency. Microbes are well grown in an optimum pH condition to produce their metabolites.  
254 The *Acidiophilic* bacteria's optimal pH is in the range of 1.5 – 2.5.[34, 45-46, 55] The ideal  
255 pH for *A. niger* mediated bioleaching is around 5.0 [49,54]. The oxidation/reduction potential  
256 (ORP) is also an important and crucial factor in ferric sulfate-mediated bioleaching, mainly

257 determined by the  $\text{Fe}^{3+}/\text{Fe}^{2+}$  redox couple. Here, high concentrations of  $\text{Fe}^{3+}$  indicate high  
258 potentials.[59,60] The ORP during the bioleaching process can be controlled by using  
259 chemical reductants or controlling the oxygen supply. When ferrous ions oxidize into ferric  
260 ions during bacterial growth, the redox potential rises; however, it drops dramatically in the  
261 first few days of LIB bioleaching and decreases even more at high pulp densities (S/L). [60-  
262 64] So far, there is no study on the optimal ORP range for increasing metal leaching  
263 efficiency in LIB bioleaching. The bioleaching efficiency can also be enhanced by carrying  
264 out the process at the microorganism's optimal temperature. The optimal temperature range  
265 for the acidophilic bacteria is between 28 and 30 °C. The majority of the fungi-mediated  
266 bioleaching has been carried out at 30 °C. Although higher temperatures help to improve the  
267 kinetics of the bioleaching process, they can also decrease microbial viability. To enhance  
268 the leaching efficiency, moderately thermophilic and thermophilic bacteria can be utilized at  
269 their optimal temperature.[50, 57,58, 65,66] Different microbes have different sensitivity to  
270 metal tolerance; however, at high pulp densities (S/L ratio), the metal toxicity is high; thus,  
271 the metal dissolution is slower due to reduced microbial activity. When LIB bioleaching is  
272 performed at high pulp densities, the viscosity of the leaching media increases,  
273 thus, decreasing dissolved oxygen and air supply to the microbe. The diffusion of oxygen into  
274 the bottom of the leaching medium is reduced when the viscosity is high; this influences the  
275 metabolism of the microorganisms, thus, reducing metal leaching efficiency. [34, 57,58]

276         The recovery of metals from LIB by the bioleaching process happens only through the  
277 metabolites produced by the microorganism. The ability of acidophilic bacteria to produce  
278 sulphuric acid and sustain the cyclic regeneration of Fe(III) ions, which can leach out various  
279 metals from complex battery matrices and promote acidophile growth by stabilizing the pH of  
280 the leaching medium, demonstrates the efficacy of bacterial bioleaching. On the other hand,  
281 fungal bioleaching efficiency is entirely dependent on excreted organic acids, which utilize

282 the O<sub>2</sub>/ H<sub>2</sub>O redox pair to oxidize LIB metals by complexing with protonated metals. The  
283 efficacy of various bioleaching systems by single bacteria, mixed bacteria, and fungi was  
284 evaluated using the leaching percentage of different metals. Generally, the metals leaching  
285 efficiency (amount of extracted metals) after the bioleaching process would be determined by  
286 comparing the amount of metal leached from the black mass using aqua regia [62-64] solution  
287 that is assumed to leach out and dissolve all the elements from spent LIB. The detailed  
288 leaching efficiency of bacteria and fungi for various metals using the bioleaching process is  
289 given in Table 3.

### 290 **3.1.3 Enhancing leaching efficiency in bioleaching process**

291 There are different ways to enhance the kinetics of the bioleaching process. The  
292 addition of metal ions such as Ag<sup>+</sup> (0.02 g/L) and Cu<sup>2+</sup> (0.75 g/L) can enhance the leaching  
293 efficiency by accelerating the electron transfer through the oxidation process and increasing  
294 metal solubility by forming intermediate metal complexes that can be very soluble in  
295 water.[67,68] The inhibitory as well as toxic effects of these metal ions on microorganisms  
296 are challenging when using them in the bioleaching process. Thus, engineering the  
297 microorganism to tolerate higher concentrations of metallic ions like Ag<sup>+</sup> and Cu<sup>2+</sup> is  
298 necessary. Another approach is to employ ultrasound bioleaching or sono-bioleaching, which  
299 improves the metal solubility by increasing the stirring at both macroscopic and microscopic  
300 stages, therefore increasing the metabolic activities of microbes.[69] The microbial tolerance  
301 against the metal toxicity at high pulp densities can be increased through the serial adaptation  
302 of bacteria or fungi over a long period by increasing the pulp densities gradually. [49,70] The  
303 adaptive microorganism is resistant to the toxic LIB components and can continue its growth  
304 and activity during the bioleaching process. The microorganism can be used as a combination  
305 of two or more species in the bioleaching process to increase the tolerance against high metal  
306 toxicity to improve the leaching efficiency.[71-73] In the bioleaching of LIBs, a mixed culture

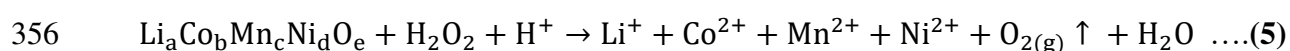
307 of iron-oxidizing-bacteria *A. ferrooxidans* and *L.ferriphilum* and sulfur-oxidizing bacteria  
308 such as *A. thiooxidans*, *Alicyclobacillus* sp, and *Sulfobacillus* sp. have been employed.[64,70]  
309 In our studies, increasing the production of bacterial metabolites such as biogenic sulphuric  
310 acid and ferric ions in the culture medium could increase the leaching efficiency at high pulp  
311 densities.[62-64] By genetically engineering microbe's, heavy metal resistance, acid  
312 endurance, and Rubisco-free carbon fixation pathways, the tolerance against metal toxicity,  
313 the fluctuating and challenging process conditions, and reduction in the time for metal  
314 extraction can be improved.[74-76]

### 315 **3.2 Food waste-enabled waste for waste (W4W) leaching approaches**

316 Traditional hydrometallurgical methods heavily involve strong acids such as HCl,  
317 HNO<sub>3</sub>, and H<sub>2</sub>SO<sub>4</sub>, producing gaseous products that are ecologically detrimental. [77-79]  
318 Therefore, the primary research focus over the past decade has been finding suitable  
319 alternatives to replace the strong acids in the metal leaching process. Bioleaching described in  
320 the previous section is one such alternative. Several other studies have employed weak  
321 organic acids such as citric acid, malic acid, succinic acid, and tartaric acids to replace strong  
322 acids in the metal leaching process. Such weak organic acids have been proven successful  
323 with a competitive leaching performance (**Table 4**). Notably, with the assistance of 0.5-15  
324 vol% H<sub>2</sub>O<sub>2</sub>, which serves as a reductant, the resulting H<sub>2</sub>O<sub>2</sub>-weak organic acid combination  
325 can extract up to >95% of metals from spent LIBs waste. One of the drawbacks of weak acids  
326 is the need to add H<sub>2</sub>O<sub>2</sub> that has a concern owing to its explosive chemical status and  
327 chemically unstable nature that has set the quest for greener alternatives to replace H<sub>2</sub>O<sub>2</sub> in  
328 this hydrometallurgy-based process. Trials on applying sodium thiosulfate (Na<sub>2</sub>S<sub>2</sub>O<sub>3</sub>) and  
329 sodium bisulfite (NaHSO<sub>3</sub>) as a reducing agent in the LIB waste recycling process instead of  
330 H<sub>2</sub>O<sub>2</sub> have shown promises, in which ~ 50-90% of the Li, Co, Mn, Ni were retrieved from the  
331 LIBs waste. [80,81] Nevertheless, the introduction of Na<sup>+</sup> into the metals-containing leaching

332 lixiviant produces undesirable adverse effects on the final recovered metals and incur  
333 additional operating steps and costs for the final product purification. Thus, searching for a  
334 green reductant such as from food waste will have a far-reaching impact on the development  
335 of sustainable close-looped recycling of spent LIBs.

336 Like LIBs waste, food waste has also increased exponentially on a global scale over  
337 the last two decades. The EU's annual food waste production is estimated to be 123 kg per  
338 person, and fruit and vegetable waste (FVW) accounts for ~ 60% of the total food waste. [82]  
339 Unfortunately, the majority of the FVW ends up in landfills or incinerated. FVW contains a  
340 wide range of reactive molecules, including dietary fibers, catechins, phenolic acids, and  
341 flavonoids, and the current handling of FVW results in a significant waste of valuable  
342 resources. [79] Recently, researchers have started investigating the possibility of using these  
343 “unnoticed and under-utilized” food waste materials as a low-cost and sustainable green way  
344 to recycle LIBs e-waste. Recent successes in using tea and plant wastes [79], grape seeds [83],  
345 discarded orange peel [84], food waste-derived products like glucose [85] and ethanol [86] as  
346 green reductants to effectively recover precious metals from LIBs waste have validated the  
347 concept of waste for waste (W4W). **Figure 3** shows various types of food waste employed in  
348 the recent progress on the food-waste enabled W4W approaches for recycling spent LIBs. The  
349 lignocellulosic content, including cellulose and hemicellulose content, have been reported to  
350 be critical for the efficient removal of metals using these various food waste types. [87,88 ]  
351 The traditional H<sub>2</sub>O<sub>2</sub>-based reductive leaching process (**Equation 5**) of extracting metals from  
352 spent LIBs is likely to cause occupational hazards and increase operational costs. In contrast,  
353 the incorporation of food waste-based natural reductants into the metal leaching process  
354 provides a safer and more cost-effective solution for recovering valuable metals sustainably  
355 from the spent LIBs.



357 Where a, b, c, d, e, refer to the number of respective atoms present in the molecular formula of  
358 the cathode in the spent LIBs. Note that the reaction is not balanced, and the value of a-d is  
359 subject to change due to different types of cathode materials.

### 360 *3.2.1. Pre-treatment of food waste*

361 Pre-treatment of food waste is shown to be necessary to enable the breakdown of the  
362 lignocellulosic structure and the release of reductants, including reducing sugars to use food  
363 waste as a reductant in the LIBs recycling. There are three types of existing technologies for  
364 pre-treating food waste: physical, chemical, and biological. [89] Physical pre-treatments are  
365 commonly employed to reduce the size of food waste to enhance its reaction surface area and  
366 reactivity. Ultrasonication, grinding, extrusion, and ball-milling are commonly employed  
367 physical pre-treatments methods. In terms of industrial scale-up and applicability, grinding  
368 and extrusion are highly recommended due to their ease of scale-up operation and efficiency.  
369 Food waste is also reported to have been treated chemically or biologically after physical pre-  
370 treatments for depolymerization, crystallinity reduction, and the production of reducing agents.

371 Chemicals such as acids (e.g., sulfuric acid, citric acid, etc.) and alkalis (e.g.,  
372 potassium permanganate) have been used for cleaning, pre-treatment, and activation of food  
373 waste. These involve higher temperature and pressure pre-treatment. Alternatively, ionic  
374 liquids have also been employed that produce reducing molecules from food waste under  
375 milder conditions as compared to acids and alkalis, albeit at a higher chemical cost. Biological  
376 pre-treatments involve enzymatic reactions of food waste to convert them to reducing  
377 molecules. Even though this approach is attractive in terms of low operation temperature, the  
378 efficiency of this process is the least among the other above pre-treatment processes and  
379 hence not widely used.

380

### 381 **3.2.2 Different food wastes employed for spent LIBs recycling**

## 382 3.2.2.1 Tea and plant waste

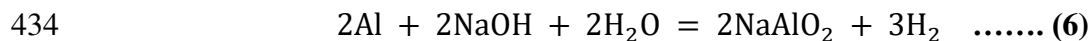
383 A sustainable hydrometallurgical process for effective metal leaching from spent  
384 lithium cobalt oxide (LCO) batteries employed tea and plant waste as reductants by Chen et al.  
385 [79] In this work, the collected LCO battery waste was subjected to multiple pre-treatment  
386 steps to separate the cathodes from anodes, separators, metallic current collectors (i.e., Cu and  
387 Al), preceding to the subsequent metal leaching experiments (**Figure 4**). After drying the tea  
388 and plant (*Phytolacca Americana* branch) waste that was mineralized and used for the  
389 leaching without any prior chemical modifications. [79] When the leaching efficiency of  
390 metals (such as Li and Co) in the presence of tea/plant waste or H<sub>2</sub>O<sub>2</sub> as a reducing agent was  
391 compared, the leaching performance of tea/plant waste was found to be comparable to that of  
392 H<sub>2</sub>O<sub>2</sub>. This is because the mass of reducing molecules was comparable, indicating that these  
393 two waste materials could be used as a replacement for H<sub>2</sub>O<sub>2</sub>. After careful analysis of the  
394 impact of multiple parameters such as time, temperature, reductant amount, acidity, pulp  
395 density on the leaching performance of tea/ plant waste; 80%-99% of the metals could be  
396 leached out at the optimal working conditions: 80 min, 70 °C, 2.0 M citric acid, reductant  
397 dosage 0.6 g/g, and pulp density 50 g/L). Around 93% of Li and 98% of Co were precipitated  
398 by adding phosphoric acid and oxalic acid after the leaching process. The recovered Li<sub>3</sub>PO<sub>4</sub>  
399 and CoC<sub>2</sub>O<sub>4</sub> after precipitation had a purity of > 98%. Another study confirmed the concept of  
400 using tea waste as a green reductant to extract valuable metals from spent LIBs, where 2 M  
401 H<sub>2</sub>SO<sub>4</sub> aided with tea waste powder was effectively leached out 100% of Li, Ni, Mn, and 90%  
402 of Co from the mixed spent LIBs.[90] The optimal condition for the above leaching process  
403 was found to be: 120 min, 90 °C, tea waste dosage 0.3 g/g, at a pulp density of 50 g/L. Further  
404 analysis by XRD, SEM, and FTIR confirmed and demonstrated the successful dissolution of  
405 the cathode materials.

406 A possible working mechanism for tea/ plant waste was proposed. Tea/plant waste is  
407 considered a rich source of lignocellulose and polyphenols (e.g., catechins), and these  
408 saccharides and polyphenols can be used as potential reducing agents to accelerate metal  
409 dissolution. It is known that cellulose and hemicellulose can be degraded into glucose and  
410 other mono/oligosaccharides under acidified conditions [91,92]. The obtained glucose and  
411 other sugars are effective reductants because of the presence of aldehyde groups. As a result,  
412 the conceived idea was that the lignocellulose component of tea/ plant waste would be  
413 decomposed into reducing sugars such as d-glucose, fructose, arabinose, etc., which would  
414 then serve as a reductant in the redox-based metal dissolution process. On the other hand, the  
415 reducing potential of polyphenols has been well documented and used in many other  
416 applications such as nanomaterials synthesis and medical use. [93-95] Chen *et al.* have  
417 tentatively demonstrated the oxidation of polyphenols including epigallocatechin gallate  
418 (EGCG), epigallocatechin (EGC), and theaflavin-3,3digallate during the leaching process.  
419 [79] FTIR analysis of the molecular structure of tea waste before and after the leaching  
420 indicated a decrease in the intensity of the -OH peak. At the same time, an increase in the  
421 intensity of the C=C peak confirms the conversion of polyhydric groups to the oxidized  
422 product, i.e., aldehyde/carboxylic group.

#### 423 3.2.2.2 Grapeseed waste

424 Aside from tea waste and plant waste, the discarded grape seeds, which contain  
425 various polyphenols such as catechins, EGCG, and EGC, can be used as a green reductant for  
426 metal extraction from spent LIBs. Zhang *et al.* recently investigated and validated the use of  
427 grape seeds for reductive metal leaching. Around 92% of Co and 99 % Li could be leached  
428 out at the optimal conditions, i.e., 0.5 g spent cathode materials, 1.5 M malic acid, 0.3 g grape  
429 seeds at 80 °C for 180 min [83]. However, pre-treatment steps such as manual dismantling  
430 were performed before the leaching experiments to separate the cathode materials from other

431 parts. Cathode current collector (Al foil) was removed by pre-leaching the spent cathode  
 432 materials using 6 % NaOH solution. **Equation 6 and 7** describes how NaOH removes Al  
 433 from the cathode materials.



436 Interestingly, the authors revealed that the grape seed-enabled reductive leaching consists of  
 437 two steps, i.e. surface chemical reaction and reactive ions diffusion, as evidenced by SEM,  
 438 TEM, XPS, and UV-Vis spectroscopy, as well as analysis of the physicochemical properties  
 439 of cathode materials such as surface morphology, metal valency, etc. at different time  
 440 intervals of leaching.[83] Notably, only  $\text{Co}^{3+}$  was formed during the first 40 minutes of the  
 441 leaching experiment, whereas  $\text{Co}^{2+}$  predominated after 180 minutes. As a result, the authors  
 442 proposed that the reduction of Co by grape seeds lags for 40 minutes to allow the  $\text{H}^+$  provided  
 443 by the malic acid to attack the surface of cathode materials, forming  $\text{Co}(\text{OH})_3$ ; which flocs on  
 444 the surface and etches the surface to improve the diffusion of the reactive reducing molecules  
 445 into the materials, as well as the subsequent redox reaction initiated by grape seeds.

#### 446 *3.2.2.3 Orange peel waste*

447 Waste from fruits and vegetables is known to be rich in numerous kinds of reducing  
 448 molecules, such as dietary fibers, phenolic acids, and flavonoids; yet these vital naturally  
 449 derived reducing substances are mostly turned into waste and dumped into landfills. Because  
 450 of this, our group conceptualized that it is possible to utilize fruit waste as a reductant in  
 451 leaching valuable metals from LIBs waste. Specifically, we investigated the possibility of  
 452 using orange fruit peel waste as a green reductant to recover valuable metals from spent LIBs.  
 453 Orange peel has an acidic nature and an abundance of dietary fibers such as cellulose and  
 454 hemicellulose, as well as antioxidants such as phenolic acids and flavonoids. Recently, we  
 455 have reported a green reductive leaching process using discarded orange peel (OP) to  
 456 effectively solubilize Li and Co from the spent LCO battery powder in a citric acid-based

457 leaching solution. [84] The detailed workflow of our study is shown in **Figure 5**. [84]. Our  
458 study gave an in-depth understanding of how individual factors (i.e., size of OP, amount of  
459 OP, leaching temperature, acidity, slurry density) modulate the metal leaching efficiency in  
460 the OP leaching system of LCO batteries. Optimal leaching conditions of 100°C for leaching  
461 temperature, 200mg OP, 1.5M citric acid, 4 hours for leaching time, and 25g/L for slurry  
462 density provided the highest leaching efficiency of >80% of metals such as Li, Co, Mn, and  
463 Ni from black mass obtained from spent LCO batteries. We investigated the underlying  
464 mechanism of operation and found that according to the reducing sugars and antioxidants  
465 theory, our ABTS and DNS analysis revealed a significant increase and abundance of  
466 reducing sugars (0 to 2.8 g/L) as well as antioxidants (0 to 0.1 mM) in the OP containing  
467 leaching liquor compared to the control, which contained only citric acids. More importantly,  
468 OP has comparable reducing power to H<sub>2</sub>O<sub>2</sub> at equal mass, implying that it has the potential to  
469 replace H<sub>2</sub>O<sub>2</sub> as a future green reductant for the rapid extraction of valuable metals from spent  
470 LIBs. In addition to that, the environmental impact of the post-leaching solid waste was  
471 carefully evaluated for its cytotoxicity to several human cell lines. Finally, to develop a  
472 closed-loop process, the recovered metals were used to synthesize an LCO cathode and then  
473 produce a brand-new recycled LCO battery [84].

### 474 **3.2.3 Food waste-derived reducing agents**

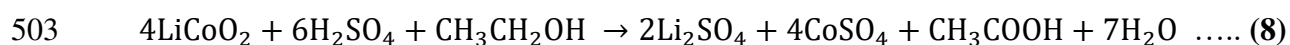
#### 475 *3.2.3.1 Glucose*

476 As previously stated, one of the proposed working principles for food waste is to use it  
477 as a reductant due to its abundance in cellulose and hemicellulose, which can be converted  
478 into reducing sugars such as glucose, xylose, arabinose, and others in an acidified solution at  
479 elevated temperatures.[91,92] Thus, it is conceivable for the direct application of food waste-  
480 derived reducing sugars for hydrometallurgical green recycling of spent LIBs. Indeed, Meng  
481 *et al.* reported using glucose as a reductant to facilitate metal extraction from mix-type spent

482 LIBs containing phosphoric acids.[85] They successfully recovered > 98% Co and ~ 100% Li  
483 using 1.5 M phosphoric acid, 0.02 M glucose at 80 °C for 2 h. Chen *et al.* [90] has also  
484 reported the optimal conditions for recovering 98% Co and 96% Li at glucose 0.4 g/g, 3 M  
485 sulfuric acids at 95 °C for 2 h, with a slurry density of 25 g/L. The presence of hydroxyl and  
486 aldehyde groups in the glucose molecule exerts the reducing power and partakes in the redox  
487 reaction with the Co<sup>3+</sup> in the spent cathode materials. As a result, Co<sup>3+</sup> is reduced to Co<sup>2+</sup> and  
488 readily soluble in the leaching solution, while glucose is oxidized into various carboxylic  
489 acids. **Figure 6** shows a diagram of the possible oxidized products of metal leaching by  
490 glucose and phosphoric acid.[86]

#### 491 3.2.3.2 Ethanol

492 Ethanol has been well researched over the years as an alternative transportation fuel  
493 for various vehicles. However, its ability to act as a reducing agent to facilitate metal  
494 extraction from spent LIBs has only been revealed recently. [96,97] Food waste, such as corn  
495 cobs, corn stalks, sugar cane waste, and rice straw, can be easily converted into ethanol via  
496 yeast-assisted fermentation and enzymatic reaction. [98] Various approaches for converting  
497 food waste into ethanol have been extensively reviewed elsewhere. [99] Recently, Zhao *et al.*  
498 reported a green hydrometallurgical process using ethanol as a reductant to extract nearly  
499 100% of the Co and Li from spent LIBs employing 6 M H<sub>2</sub>SO<sub>4</sub>, 5 vol% ethanol, 90 °C, 80  
500 min. [86] The author attributed the reducing power of ethanol to its hydroxyl groups, which  
501 were oxidized to carboxylic acid groups during the dissolution process of the spent LIBs. The  
502 redox reaction involved in this work can be expressed as follows (**Equation 8**)



504 In addition to the mechanistic understanding of the oxidation of ethanol, the authors further  
505 reported the best-fit kinetic model to explain the ethanol-enabled metal dissolution process.

506 The kinetic model, known as the residual layer diffusion control model, is expressed in  
507 **(Equation 9)**.

$$508 \quad 1 - 3(1 - x)^{\frac{2}{3}} + 2(1 - x) = kt \quad \dots\dots (9)$$

509 Where x is the leaching efficiency, k is the slope of the fitted trendline, and t is the reaction  
510 time (min).

511 Using **Equation 9**, along with the Arrhenius law and the optimal leaching condition, the  
512 activation energy of Co and Li in the ethanol-containing leaching liquor was obtained and  
513 compared with the control where only H<sub>2</sub>SO<sub>4</sub> was used. The author noted a significant  
514 decrease in activation energy for Co (54.22 to 37.60 kJ/mol) and Li (52.04 to 37.03 kJ/mol)  
515 by using ethanol as the reductant. The lower activation energy metal readily undergoes a  
516 redox reaction, where the marked decline in the activation energy for both metals further  
517 emphasizes the strong reducibility of ethanol. Although the complete extraction of Co and Li  
518 via the ethanol-based leaching method is remarkable, the potential environmental impacts  
519 incurred by the acetic acid waste (equation 8) generated during the leaching reaction have  
520 also been discussed. Thus, proper handling of the leaching-derived acid waste is entailed  
521 without causing environmental pollution.

### 522 **3.3 Electrochemical approaches**

523 Electrochemical methods are well-developed, cost-efficient, environment-friendly, and  
524 easy to scale-up, and have widespread applications in sensing, energy, mining, etc., including  
525 metal extraction/recovery from different sources by electrochemical means.[110-113]  
526 Electrochemical methods for metal recovery were first applied in the mining industry to  
527 selectively electrodeposit pure metals from their natural ores. [114] This technology soon  
528 attracted researchers who were developing sustainable methods to recycle spent waste to  
529 adopt this method for recycling spent LIB. [113] Specifically, electrochemical approaches  
530 have been employed in different hydrometallurgical recycling stages, such as leaching [115]

531 and recovery [116] of valuable metals from spent LIB waste (**Figure 7**). In an  
532 electrochemically-assisted leaching process, the applied electric current acts as a “reducing  
533 agent” to improve the metal extraction (dissolution) from their insoluble form in spent LIB  
534 waste into a soluble ionic form in the acidic leaching solution. [115] Therefore, it replaces  
535 explosive and expensive chemical reducing agents such as hydrogen peroxide ( $H_2O_2$ ),  
536 enabling the leaching process to be safer and more cost-efficient.

537 Moreover, applying an electrolysis process, mildly acidic solutions are prepared in a  
538 sustainable approach from broadly available sources, e.g., seawater. [117,118] A wide range  
539 of electrochemical methods have been exploited for metal recovery from leaching solutions or  
540 directly from a cathode active material (CAM). [119, 120] Metal electrodeposition offers  
541 quick, simple, selective, and efficient recovery of metals (or their compounds in their pure  
542 state) in a highly controllable approach. Moreover, by adjusting the electrodeposition  
543 parameters, electrodeposited metal properties such as thickness, morphology, and crystal  
544 structure can be easily controlled. [120] Therefore, due to their varying physical and chemical  
545 properties, electrochemically extracted metals/metal compounds or their mixtures may not  
546 only be used as precursors to regenerate LIBs [121] but to generate materials that have a  
547 variety of other applications such as electrochemical supercapacitors [122,123],  
548 superhydrophobic coatings [124], electrochromic compounds [125], magnetic alloys [120],  
549 etc. (**Figure 7**). Hence the materials from spent LIB e-waste can potentially be applied in  
550 various applications enhancing the sustainability of the LIB industry.

### 551 **3.3.1 Electrochemically-assisted hydrometallurgical processes**

552 In a typical LIB, the negative electrode (anode) and positive electrode (cathode)  
553 constitute more than half of the LIB composition (**Figure 8A**). [128] The majority of  
554 recyclable metals are present in the CAM. Depending on the LIB type, the constitution and  
555 variety of metals present in LIBs may vary among the following ones: Li, Co, Ni, Mn, Al, and

556 Fe (**Figure 8B**). Additional amounts of Al (from the cathode collector), Cu (from the anode  
557 collector), and Fe (from the casing material) could be found in spent LIB residue if the case  
558 material and current collectors were not separated during a pre-treatment stage (**Figure 8C**).  
559 After the pretreatment process of spent LIBs described in Section 2, the metal-containing  
560 black mass is subjected to an acidic solution to dissolve the metals in their ionic form in a  
561 standard hydrometallurgical process. The dissolved ions are then recovered either by  
562 precipitation in alkaline media [129] or separated by solvent extraction. [130] As the most  
563 efficient acids cannot fully leach metals, chemical reducing agents such as  $H_2O_2$  are usually  
564 added into an acidic leaching solution to improve the metal leaching efficiency. [131] During  
565 a recovery stage, metal ions present in the leaching solution are separated by adding chemicals,  
566 namely either strong bases to raise the pH of the leaching solution for metal precipitation  
567 [129] or organic extractants in a solvent extraction method. [130] Even though chemical-  
568 based hydrometallurgy approaches can enable selective and effective metal recovery, they  
569 suffer from drawbacks such as large chemical consumption, tedious and complicated handling  
570 protocols, secondary pollution generation, and the high cost of recycling. The low-recycling  
571 profit accordingly impedes the development and scaling-up of a chemical-based  
572 hydrometallurgical method in the recycling industry. Electrochemical methods have recently  
573 attracted considerable attention for recycling metals from spent LIBs because of their  
574 environmental compatibility, high efficiency and adoptability, operation viability, and cost-  
575 effectiveness when electrons are employed as “green redox reagents“ instead of hazardous  
576 chemicals. The standard reduction potentials of metals (**Figure 8D**) [127] are critical for  
577 selective metal electrodeposition, as explained in Section 3.3.1.2.1.

### 578 **3.3.1.1 Electrochemically-assisted leaching/leaching solution generation**

579 Electrochemically-assisted redox reactions have been exploited to facilitate the metal  
580 leaching process without the addition of chemical reductants (**Table 5**). [115, 132]  
581 Specifically, during sulfuric acid ( $H_2SO_4$ ) leaching, Prabakaran *et al.* applied a direct current

582 of 400 A/m<sup>2</sup> between the Pb anode and the stainless-steel (SS) cathode and achieved 99 %  
583 leaching rates for Co and Mn from the mixed spent LIBs, as compared to the H<sub>2</sub>SO<sub>4</sub> leaching  
584 without a reducing agent (between 50 % and 80 %). [115] The electrochemically-assisted  
585 leaching showed no improvement when compared to a chemical reducing agent such as H<sub>2</sub>O<sub>2</sub>  
586 (close to 99 %) [133]. However, this approach allowed for the re-use of the leaching solution,  
587 significantly reducing the amount of chemicals used and secondary waste generated. [126] A  
588 few years later, Li *et al.* successfully employed slurry electrolysis to both leach and  
589 electrochemically recover Li and Mn from LMO batteries (**Table 5**). [115,132,] Furthermore,  
590 the electrolysis process has been employed as an alternative sustainable approach to generate  
591 acidic leaching solutions from low-cost resources such as NaCl, seawater, or weak brine  
592 solutions for leaching complex spent LIBs waste (**Table 5**). [117] Even though  
593 electrochemically-generated leaching solutions were used, metal leaching efficiency was  
594 significantly lower than using strong inorganic acids with chemical reductants, and the  
595 preliminary studies indicated the process to be economically feasible. It was primarily based  
596 on the value of recoverable Co and Li if the existing challenges are addressed accordingly.  
597 For instance, different spent LIBs pretreatment protocols could be applied to separate highly  
598 acid-consuming elements such as Al, thus sustaining stable acidic pH during the leaching  
599 procedure.

### 600 3.3.1.2 Metal recovery by electrochemical approaches

601 Selective metal recovery in their pure state is achieved by electrochemical methods,  
602 such as classical electrodeposition, electrolysis, electrodialysis, when potential or current  
603 (electrons) is applied to initiate non-spontaneous electrochemical reactions. [113] The most  
604 common electrochemical recovery method is metal electrodeposition (electrowinning) from  
605 their leaching solution *via* a reduction reaction where the dissolved metal ions are precipitated  
606 into their solid metallic form on a cathodic electrode. The electron supply through the circuit

607 from the anode to a cathode is driven by an external electric source, and its magnitude is  
608 selected based on the standard reduction potentials of metals recovered (**Figure 8D**).

609

### 610 3.3.1.2.1 Metal compatibility in electrochemical recovery

611 It is important to emphasize that electrodeposition is not a straightforward recovery  
612 method for each metal. In particular, easier electrodeposition is achieved with metals of higher  
613 standard reduction potentials. From all the metals found in spent LIB waste (**Figure 8D**), only  
614 Li ( $E^0 = -3.05$  V vs NHS) cannot simply be electrochemically deposited from aqueous  
615 solutions due to its strong negative potential. Therefore, Li is often either discarded as a waste  
616 [125, 134-136] or recovered last as  $\text{Li}_2\text{CO}_3$  by chemical precipitation after other metals have  
617 been recovered electrochemically. [132, 121, 137] To recycle LIBs without any wastage of Li,  
618 Ra *et al.*[138] developed an electrochemical relithiation process *via* the combined  
619 electrochemical and hydrothermal reactions where LCO is regenerated in one step. Using this  
620 methodology, CAM can be regenerated either directly from the LCO slurry without leaching  
621 [138] or from a leaching solution (**Figure 7**). [139] It can also be used to regenerate  
622 precursors for other types of LIBs, such as LFP [140] or LMO. [141] However, the above  
623 research shows that the regenerated CAM demonstrates significantly lower energy capacity  
624 than the initial cathode capacity.

625 Another important consideration in the electrochemical recovery of metal is the metal  
626 co-precipitation due to their similar standard reduction potentials, which results in impurities  
627 of the deposited metal layer. By considering the adequate difference among the standard  
628 reduction potentials of Cu ( $E^0 = +0.34$  V vs NHS), Co ( $E^0 = -0.28$  V vs NHS), Fe ( $E^0 = -0.44$   
629 V vs NHS), Mn ( $E^0 = -1.18$  V vs NHS) and Li ( $E^0 = -3.05$  V vs NHS) (**Figure 8D**) [127], i.e.  
630 the metals found in LCO, LMO, LFP batteries or their mixtures, separation of the individual  
631 metals by electrodeposition is feasible without additional chemicals for removal/recovery for

632 these types of LIBs. [115] However, a great challenge in the recovery of pure metals is  
633 encountered when NMC, NCA or mixed spent LIBs from various sources are being recycled.  
634 A CAM obtained from NMC, NCA, or their mixture contains Co ( $E^0 = -0.28$  V *vs* NHS) and  
635 Ni ( $E^0 = -0.26$  V *vs* NHS), which are not compatible with electrochemical recycling because  
636 of their similar standard reduction potentials. Different approaches have been utilized to  
637 recycle NMC and NCA batteries or LIBs mixtures. For instance, before electrodeposition,  
638 Lupi *et al.* [134, 135] recovered pure Co and Ni from mixed LIBs when the two metals were  
639 first separated by solvent extraction. Dutta *et al.* [133] carried out a much more delicate  
640 recycling approach where the leachate containing Co, Li, Mn, Cu, and Fe ions was subjected  
641 to chemical precipitation/solvent extraction to obtain a pure solution of Co for its  
642 electrodeposition. The combined separation methodology is pretty complicated as well as  
643 results in high consumption of chemicals and disposal of incompletely recycled (metal-  
644 containing) waste. Therefore, instead of recycling each metal separately, Mesbah *et al.* [122]  
645 exploited an alternative, a one-step electrodeposition approach of Li-Ni-Mn-Co hydroxide  
646 film for supercapacitor device applications.

#### 647 3.3.1.2.2 Critical factors for metal electrodeposition

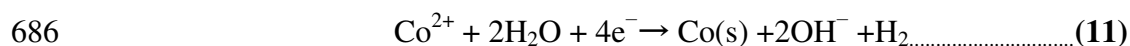
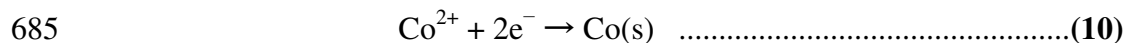
648 The most extensive fundamental and practical research in electrochemical recycling  
649 has been done using LCO type of LIBs (**Table 6**) [116, 119-122, 139-145] because it is the  
650 most common type of LIBs. It has the highest content of Co, which is the most valuable metal  
651 found in LIBs due to its global scarcity. [146] Among several research groups working on  
652 LIB recycling, the most considerable work on metal electrochemical recycling from spent  
653 LIBs has been done by Garcia's group. [116, 119-122, 139-145] Through fundamental studies  
654 on metal electrodeposition from different leaching solutions (**Table 6**), different research  
655 groups have proven that the metal electrodeposition efficiency and deposited metal/metal  
656 product physicochemical properties highly depend on different parameters, e.g. electrode

657 materials [134,135,142], electrochemical method [116,119,134,135,143], electrolyte  
658 conditions (pH)/composition [115, 119, 120, 143,144], current density [119, 120], mass  
659 transfer. Therefore, it is essential to select suitable technical components and parameters as  
660 well as electrolyte properties to improve the deposition yield and properties of the deposited  
661 metal(s). Specifically, the key factors for selecting electrodes for metal recovery are electrode  
662 stability, current efficiency, and inertness towards side reactions on a cathodic electrode, such  
663 as a hydrogen evolution reaction. Prabaharan *et al.* [115] and Lupi *et al.* [135] have used SS  
664 and Al, respectively, as cathode materials, which provide a relatively high hydrogen  
665 overpotential, are made of low-cost material, and enable easy recovery of metallic Co deposit.

666 On the other hand, since an anode is electrochemically inert, electrodes such as Pb  
667 alloys and Ti/IrO<sub>2</sub> are widely used. [115, 135] Moreover, electrodeposition behavior is highly  
668 affected by technical parameters of the process, such as current density. For instance, higher  
669 microporosity of the Co layer was observed with an increase in current density. [120] The  
670 higher current density also results in slightly lower current efficiency since the current is  
671 partly involved in hydrogen evolution reaction instead of direct deposition reaction of a metal.  
672 Mass transfer is also known to have a significant impact on metal electrodeposition behavior,  
673 as proven previously. [147]

674 Besides the impact of technical components and parameters, electrolyte properties  
675 such as pH are critical for metal recovery. The electrodeposition studies of Co from different  
676 sources, e.g. LCO [120, 142] or mixed LIBs [115], clearly demonstrated that the Co  
677 deposition yield, deposition morphology, and crystalline structure are pH-dependent. The  
678 highest yield of the deposited Co, most intense 3D crystal growth, and largest grain size  
679 within the layer were observed at pH 5.4 in the investigated pH range of 2.7-5.4. Freitas *et al.*  
680 performed simultaneous electrochemical-quartz crystal microbalance (E-QCM) studies to  
681 elucidate the Co electrodeposition mechanism as a function of pH. [142-143] It was revealed

682 that electrodeposition of Co at pH 5.4 occurred *via* a direct reduction mechanism (**Equation**  
 683 **10**). Whereas at pH 2.7, electrodeposition occurred *via* a mechanism of  $\text{Co}^{2+}$  reduction with  
 684 the formation of adsorbed hydrogen (**Equation 11**):



687 The combined approach of E-QCM measurements was later employed to investigate Cu  
 688 deposition mechanism from spent LIB anodes. [116]

### 689 **3.3.2 Alternative applications of electrochemically recovered metal compounds**

690 The ultimate purpose of a closed-loop recycling approach of spent LIBs is to recycle  
 691 and directly reuse valuable metals for LIB regeneration (Section 5.1). [137-139] However,  
 692 electrochemically-recovered metal compounds also have a great prospect to be exploited for  
 693 different alternative applications. In 2012, Garcia's group pioneered the research on the  
 694 possibility of using recycled metallic Co as a supercapacitor [144]. The specific capacitance  
 695 determined from cyclic voltammetry and electrochemical impedance spectroscopy  
 696 measurements showed a good agreement, yielding the value of 625 F/g. This shows that Co  
 697 recycling from spent LIBs is economically and environmentally viable for application in  
 698 supercapacitor devices. As mentioned in Section 3.3.1.2.1, a mixed hydroxide supercapacitor  
 699 was electrochemically deposited from NMC batteries, in which the recycling procedure is,  
 700 otherwise, complicated if the goal is to recover each metal individually. [122] Later, Garcia *et*  
 701 *al.* proposed the application of recycled Co in interconnects for solid oxide fuel cells (SOFC).  
 702 [145] Rafsanjani-Abbasi *et al.* [124] developed a new electrochemical Co recycling process  
 703 fabricating low resistivity superhydrophobic Co coating on a carbon steel surface when using  
 704 ascorbic acid-assisted  $\text{H}_2\text{SO}_4$  leaching system.

705 Moreover, it was demonstrated that a Cu layer could be formed electrochemically on  
 706 an electrodeposited Co layer, thus forming the Co-Cu bilayer. [119] Thin Co-Cu multilayers

707 are of great interest due to their giant magnetoresistance that can be exploited in magnetic  
708 field sensors. [148] Mei *et al.* electrochemically recycled the spent LPO and LCO batteries to  
709 obtain high-performance hematite/CoPi photoanodes for water splitting application. [149] The  
710 possibility to recover a variety of metal products with well-controlled physicochemical  
711 properties for different applications is a crucial advantage of electrodeposition.

712

### 713 **3.4 Ionic Liquids and Deep Eutectic Solvents**

714 Ionic Liquids (ILs) are organic salts that consist of organic or inorganic cations and  
715 anions, usually in a liquid state below 100°C. They have been seen as replacement options for  
716 sustainable and environmentally friendly solvents because of their low volatility, vapor  
717 pressure, and flammability. [150] Moreover, ILs allow structural metal coordination like a  
718 potential template or a structure-directing agent in the formation of materials, thus enabling  
719 metal removal from spent LIBs. [151] For example, high-quality Cu-BTC (HKUST-1)  
720 synthesis was reported, using cholinium ionic liquids (ILs) in water at room temperature.  
721 [152] Guillaume *et al.* reported that lithium, cobalt, and nickel could be extracted from  
722 leaching solutions using imidazolium-based ionic liquids [C<sub>4</sub>mim][NTf<sub>2</sub>] as diluents and tri-*n*-  
723 butyl phosphate TBP as a specific ligand with a low pH (pH < 3). [153] Selective extraction  
724 of Mn, Co, Ni, and Li have been explored using ionic liquids by the same group. In the first  
725 step, more than 90% of Mn was selectively extracted from the leaching solution using  
726 N,N,N',N'-Tetra-*n*-octyldiglycolamide (TODGA) extractant diluted in an ionic liquid,  
727 followed by 90% cobalt extracted using an ionic liquid tri-hexyltetradecylphosphonium  
728 chloride in the second step. Nickel was removed by deep eutectic solvents (DESs) based on  
729 lidocaine and carboxylic acids, leaving Li in the solution to be recovered by precipitation.  
730 [154] Another study investigated the extraction of metals from spent LIBs using deep eutectic  
731 solvents and achieved a leaching efficiency of more than 90% of Co and Li from LCO and

732 NMC-based LIBs. [155] Another type of Ionic liquids, such as  
733 trihexyl(tetradecyl)phosphonium chloride (Cyphos IL 101) or tricaprylmethylammonium  
734 chloride (Aliquat 336), has been investigated to extract Ni specifically from nickel-metal  
735 hydride batteries. [156]

#### 736 **4. Regeneration of materials from spent LIBs**

737 Spent LIBs consist of several components from packaging materials, current collectors  
738 (Al, Cu), electrolyte containing lithium salt and organic solvent, cathode containing various  
739 metals, anode (primarily carbon/graphite based), polymeric fluorinated and non-fluorinated  
740 binders, conductive carbon additives, polymeric separator sheets, external tabs (Ni/Fe), etc. It  
741 is generally accepted that among these various components, cathode material possesses a  
742 higher economic recovery value as compared to others. Hence presently, less attention is paid  
743 to the regeneration of other components of the spent LIBs except for cathode. However, the  
744 electrolytes' toxicity, fluorinated binders, limited Lithium metal reserves, and the extensive  
745 use of carbon-based materials would stimulate proactive, innovative thoughts on the proper  
746 recycling of other components of spent LIBs, including anodes and electrolytes from spent  
747 LIBs. [13] Other challenges are posed in extracting these components from spent LIBs; for  
748 example, recycling of LIB electrolytes reports are rare because the majority of the electrolyte  
749 is bound on the separator and active materials, making extraction and collection difficult.  
750 Moreover, the electrolyte components are volatile, flammable, and toxic that would require  
751 recycling and recovery to be performed in a confined, safe environment. Finally, the  
752 electrolyte components exist as complex, which include lithium salts, organic solvents, and  
753 additives, making their separation and purification challenging. Hence, current regeneration  
754 approaches are focused mainly on cathode materials from spent LIBs.

755 There have been strategies reported on selective metal recovery from green leaching  
756 processes, which we highlight in section 4.1. However, in current industrial recycling

757 processes, selective separation of the associated individual components from the leach liquor  
758 is still a significant problem for cost-saving, technology innovation, and process enhancement.  
759 Regeneration technologies of battery materials could be one way to potentially address this  
760 problem wherein it regenerates battery materials by utilizing the co-existence and  
761 collaborative extraction characteristics of valuable metal ions in a complex system, resulting  
762 in a closed-loop therapy with significant development potential. Researchers have developed  
763 several high-value regeneration ways of valuable components, including technologies such as  
764 coprecipitation-calcination regeneration, sol-gel-calcination regeneration, hydrothermal-  
765 calcination regeneration, electrodeposition regeneration, solvent extraction regeneration, etc.  
766 [157-159] Among which the coprecipitation approach is widely employed in regenerating  
767 valuable components synergistically into a precipitate from the leachate liquor. However,  
768 there are challenges associated with regeneration technologies that still need to be researched  
769 and addressed, including the addition of an excess of complexing/precipitating agent and their  
770 further removal, unwanted ion adsorption, agglomeration, side reactions leading to loss of  
771 extracted elements.

772

#### 773 **4.1 Metal recovery from green leaching process**

774 After the green leaching processes, the leach liquor consists of elements mainly from  
775 the cathode and current collector, including Li, Mn, Ni, Co, Al, Fe, Cu etc. Solvent extraction  
776 and chemical precipitation are commonly reported to recover specific metal ions or to  
777 eliminate other impurities from the aqueous leaching solution. Cyanex 272 (Bis-(2,4,4-  
778 trimethylpentyl) phosphinic acid) and PC-88A (2-ethylhexyl phosphoric acid mono-2-  
779 ethylhexyl ester) are widely used solvents to separate cobalt from the leach liquor solution,  
780 and D2EHPA (di-(2-ethylhexyl) phosphoric acid) can selectively extract Mn from the  
781 leaching liquor. Lithium (Li), on the other hand, is difficult to efficiently remove using

782 solvents from a mixed-metal leaching solution [13]. Transition metal ions such as Ni, Co, Mn  
783 are also precipitated using the solubilities of metal compounds at different pH levels. The  
784 most common precipitating agents used are sodium hydroxide (NaOH), oxalic acid ( $\text{H}_2\text{C}_2\text{O}_4$ ),  
785 ammonium oxalate  $[(\text{NH}_4)_2\text{C}_2\text{O}_4]$ , sodium carbonate ( $\text{Na}_2\text{CO}_3$ ), and sodium phosphate  
786 ( $\text{Na}_3\text{PO}_4$ ). In most cases, they form insoluble transition metal precipitates such as hydroxides,  
787 carbonates, or oxalates, as well as lithium carbonate or phosphate. [13,157]

788         Generally, solvent extraction is employed in separating both nickel and cobalt ions  
789 because of their similar properties [160]. Other approaches such as electrodeposition have  
790 been reported to recover pure nickel from spent LIBs [161]. In this study, CYANEX 272 was  
791 used to separate nickel and cobalt via solvent extraction, while nickel was later recovered by  
792 electrodeposition. Nan *et al.* (2005) have reported the precipitation of cobalt as oxalate and  
793 lithium as carbonate, respectively, finally regenerating  $\text{LiCoO}_2$  cathode material from the  
794 recovered cobalt and lithium [162]. Chen *et al.* (2011), has recovered cobalt using an oxalate  
795 precipitation agent [158]. Iron, manganese, and copper from the leached solution were  
796 separated by selective precipitation as follows : (i) iron removal by precipitation with sodium  
797 hydroxide (NaOH), (ii) manganese removal by ammonium persulfate  $(\text{NH}_4)_2\text{S}_2\text{O}_8$ , and iii)  
798 copper removal by NaOH. Using solvent extractant P507, cobalt, nickel, and lithium were  
799 separated from the leached solution, and cobalt was finally precipitated using ammonium  
800 oxalate. The interesting aspect of recycling LIBs is the regeneration of electrode materials for  
801 new LIBs. Sol-gel or coprecipitation technologies can be used in the leaching-resynthesis  
802 process for synthesizing the regenerated cathode materials in short steps. [162,163]. Lee &  
803 Rhee (2002) regenerated the  $\text{LiCoO}_2$  cathode material through the sol-gel method using citric  
804 acid and lithium nitrate from spent LIBs. [163]

#### 805 **4.2 Regeneration of battery cathode materials**

806 In the final loop of the regeneration and recovery process, cathode materials are re-  
807 synthesized from individual salts recovered from leachates or leaching solutions through  
808 green recycling and assembled into new LIBs. Various synthesis methods [164] of  
809 regeneration have been applied depending on the type of battery materials, as described in the  
810 section below.

#### 811 4.2.1. Regeneration of NMC

812 Solid-state synthesis is the primary reported method for cathode material synthesis,  
813 with many optimization procedures in terms of stoichiometry, synthesis temperature to  
814 improve the performance of the cathode materials formed. As  $\text{LiNi}_x\text{Mn}_y\text{Co}_z\text{O}_2$  (NMC) has  
815 multiple formulas depending on the composition intended, there is no single optimized  
816 synthesis procedure capable of producing all NMC materials. In the NMC111  
817 ( $\text{LiNi}_{0.3}\text{Mn}_{0.3}\text{Co}_{0.3}\text{O}_2$ ) context, a stoichiometric ratio of metals (Ni:Mn:Co: Li = 1:1:1:3) was  
818 added/topped up in the leaching solution using their acetate salts of the three transition metals  
819 (Ni, Co, Mn) and  $\text{Li}_2\text{CO}_3$ . [165]. This process includes a pre-heating step at  $350^\circ\text{C}$  for 4  
820 hours in air, followed by further heating at  $500^\circ\text{C}$  to  $900^\circ\text{C}$  for 12 hours in an ambient  
821 atmosphere to obtain phase pure NMC111 cathode material. Li-rich NMC materials have also  
822 been experimented and optimized, with synthesis methods ranging from solid-state to solution  
823 synthesis [166]. In a hydrothermal synthesis, the leaching solution from the green recycling  
824 process is mixed with 4 M LiOH solution and heated at ( $120^\circ\text{C}$ -  $200^\circ\text{C}$ ) in a reactor followed  
825 by sintered with 5%  $\text{Li}_2\text{CO}_3$  in an oxygen environment at  $850^\circ\text{C}$  for 4 hours. [166] The sol-  
826 gel method can also be employed to synthesis Li-NMC cathode material by using citric acid  
827 as a chelating agent. However, when compared to solid-state and hydrothermal procedures,  
828 the operating process of this approach is more complex, and the preparation time is  
829 longer.[167] Different compositions of NMC have been synthesized when a different

830 synthesis method is explored. Thus, for NMC materials, the selection and control of the  
831 composition of NMC ratio are critical for choosing the synthesis methods.

#### 832 *4.2.2. Regeneration of LiCoO<sub>2</sub>*

833 In the bid to re-synthesize LCO cathode materials from leached elements, the most  
834 common methods are via solid-state synthesis or hydrothermal synthesis. Solid-state synthesis  
835 of LCO cathode involves mixing the leach solution, which contains Li<sub>2</sub>CO<sub>3</sub> and CoCO<sub>3</sub>, and  
836 heating in a furnace in ambient atmosphere at 600°C for 3 hours, followed by calcination at  
837 900°C for 1 hour [168,169]. This process is suitable for recovering Li<sub>2</sub>CO<sub>3</sub> and CoCO<sub>3</sub> from  
838 the leachates without the addition of the respective salts. Alternatively, hydrothermal  
839 synthesis has also been shown to be feasible for synthesizing pure LiCoO<sub>2</sub> material with a  
840 high success rate. Pure LiCoO<sub>2</sub> material can be synthesized by adding Co(OH)<sub>2</sub> and LiOH in  
841 the stoichiometric amount in deionized water and heating at 220°C in a hydrothermal  
842 autoclave [170]. Some of the less-explored synthesis methods reported for LCO include (1)  
843 the addition of Co (NO<sub>3</sub>)<sub>2</sub>, LiNO<sub>3</sub> in polyacrylic acid (PAA) and spin coating in a sol-gel  
844 synthesis process, (2) microwave synthesis of Co- and Li-methyl carboxylate salts and (3)  
845 molten salt synthesis of Co(NO<sub>3</sub>)<sub>2</sub> and LiNO<sub>3</sub> with KOH and calcination in 650°C for 8 hours  
846 in air were also explored in the synthesis of LCO cathode [171, 172,173].

#### 847 *4.2.3. Regeneration of LiFePO<sub>4</sub>*

848 Synthesizing LiFePO<sub>4</sub> using solid-state reaction is feasible, with a strict requirement of  
849 an inert synthesis atmosphere. The rationale is to prevent the oxidation and formation of  
850 Fe<sub>2</sub>O<sub>3</sub>, which is inevitable if calcination is conducted in the presence of O<sub>2</sub> gas in the air. By  
851 introducing an inert gas such as Ar, the calcination of FePO<sub>4</sub>, Li<sub>2</sub>CO<sub>3</sub> with a reducing agent  
852 (sugar) is feasible for the formation of LiFePO<sub>4</sub> materials [174]. In this same atmosphere,  
853 FeC<sub>2</sub>O<sub>4</sub> as the iron source could also be utilized for the solid-state synthesis of LiFePO<sub>4</sub>, with  
854 a prior step involving ball-milling of FeC<sub>2</sub>O<sub>4</sub> and Li<sub>2</sub>CO<sub>3</sub>, calcination at 350°C for 10 hours,

855 and then at 600°C for 10 hours [175]. The alternative method for synthesizing LiFePO<sub>4</sub>  
856 includes hydrothermal process using FeSO<sub>4</sub>, LiOH, and H<sub>3</sub>PO<sub>4</sub> in deionized water, where the  
857 solution needs to be heated in an autoclave at T=150°C = ~ 220°C (optimum temperature at  
858 180°C) for 5 hours [176]. Carbon-thermal reduction process can also be used to regenerate  
859 LiFePO<sub>4</sub>. In this method, a FePO<sub>4</sub>·2H<sub>2</sub>O precursor was produced from the leaching solution  
860 by heat treatment, which was then calcined with Li<sub>2</sub>CO<sub>3</sub> and glucose in N<sub>2</sub> environment to  
861 produce LiFePO<sub>4</sub>/C. Overall, LiFePO<sub>4</sub> regenerated via carbon-thermal reduction has superior  
862 electrochemical performances than regenerated via solid-state reaction. [164,177]

863

## 864 **5. Reusability**

865 The construction of new batteries from the regenerated electrode materials is the final  
866 step in the LIB recycling process. Commonly, coin cells or cylindrical cells are made from  
867 regenerated electrode material, and electrochemical performance such as charging,  
868 discharging capacity, and cycling stability tests are used to be performed. This section has  
869 discussed the reusability of leached and regenerated using various green recycling processes  
870 as potential cathode and anode materials in new LIBs constructed.

871

### 872 **5.1 Reusability of cathode materials from green recycling process**

873 Jai Kumar et al. recovered lithium as LiCO<sub>3</sub>, and FePO<sub>4</sub> from LiFePO<sub>4</sub>-based spent  
874 LIBs using citrus juices from lemon, orange, and apple, that contained organic acid. The  
875 recovered materials were then used to regenerate LiFePO<sub>4</sub> cathode, yielding a discharged  
876 capacity of 155.3 mAh/g and a capacity retention of 98.30 % over 100 cycles at 1C. [178] In  
877 another study, NMC cathode material was resynthesized from ascorbic acid leaching solution  
878 using oxalic acid co-precipitation method, followed by a hydrothermal and calcination process.  
879 The resynthesized sample had a charge capacity of 345.8 mAh/g and a discharge capacity of

880 258.8 mAh/g at 0.1C, and the capacity retention was 87% after 50 cycles. [179] Oxalic acid  
881 was used as leaching as well as a co-precipitation agent in another research to regenerate  
882 NCM cathode material through the calcination process. At 0.2C, the highest discharge  
883 capacity was 168 mAh/g, with a 91.5% capacity retention after 150 cycles. [180] Wu et al.  
884 extracted  $\text{LiCoO}_2$  from LIB scraps using citric acid as a lixiviant and orange peel as a  
885 reductant to regenerate new cathode material. The regenerated cathode material's initial  
886 charge and discharge capacities were 120 and 103 mAh/g, respectively. [84] Ra et al.  
887 developed an electrochemical relithiation process in which LCO was produced in one step  
888 directly from slurry using a combination of electrochemical and hydrothermal reactions,  
889 allowing them to recycle and regenerate LCO without losing Lithium. The regenerated  
890 cathode active material (CAM) LCO battery had an initial discharge capacity of 134.8 mAh/g,  
891 with 95.9% retention after 50 cycles. [138] A CAM of LCO battery was regenerated from a  
892 leaching solution following the above methodology, and the regenerated LIB had a discharge  
893 capacity of 127 mAh/g and retained 96 % of its capacity after 30 cycles. [139] Another study  
894 found that refunctionalization of the  $\text{LiFePO}_4$  cathode using electrochemical lithiation  
895 restored its original capacity of 150–155 mAh/g. [140]

896

## 897 **5.2 Reusability of graphite from green recycling process**

898 Graphite is used as an anode material in most commercial LIBs due to its long-term  
899 cycle stability, high capacity, better electrical conductivity, and superior thermal and  
900 mechanical stability. [181] Recycling graphite from LIB leaching residue is an exciting idea  
901 towards a cost-effective closed-cycle circular economy approach. Generally, residual cathode  
902 materials, and elemental Cu, Fe, Al, and other contaminants, can be found in the leaching  
903 residue. [182] Commonly, oxidative lixiviation using acids and other solvents can be used to

904 remove impurities including Al, Cu, and Fe, whereas reductive lixiviation can be used to  
905 remove remaining cathode metals from the recycled graphite powders. [183]

906 Recently organic acid such as citric acid has been used to regenerate graphite from the  
907 spent anode. The optimal condition for impurity elimination from spent graphite was found to  
908 be 0.2 M citric acid at a pulp density of 20 g/L at 90 °C for 50 minutes. Spent graphite  
909 regenerated using citric acid had a discharge cell capacity of 330 mAh/g after 80 cycles.  
910 [184] Boric acid pre-treatment followed by a short annealing process has also been used to  
911 regenerate graphite from spent LIBs. The capacity of graphite pre-treated with boric acid and  
912 sintered at 1050 °C was 332 mAh/g, which remained unchanged after 100 cycles. [185] Our  
913 group has recycled graphite from bioleaching residue using citric acid. The recycled graphite  
914 had a discharging capacity of 320 mAh/g and is stable for more than 100 cycles. [186]. Such  
915 approaches are promising towards the direction of reuse of recycled graphite as a LIB anode.

916

### 917 **5.3 Reusability as Metal-Organic Frameworks (MOFs)**

918 The precipitation of leached metals recovered from spent LIBs into highly valuable  
919 Metal-Organic Frameworks (MOFs) opens up a new application possibility for these  
920 recovered, recycled metals.[187,188] Metal-Organic Frameworks (MOFs) are porous  
921 materials constructed from metals and organic linkers.[ 189] They are characterized by their  
922 high porosity, high thermal and chemical stability, which allows them to succeed in diverse  
923 applications such as gas separation, gas storage, or catalysis. [190] Moreover, MOFs have  
924 raised researchers' interest in their usage in electrochemical energy storage systems such as  
925 batteries. [191, 192] Developing MOF-based batteries through the recycling of LIBs will lead  
926 to a close-loop and reduce the environmental and ecological impact. Instead of separating  
927 individual metals to create a valuable, cost-effective method for making LIBs, it is also

928 advantageous to develop an alternative route for higher-value products such as MOFs that  
929 could be produced from waste LIBs in a few steps.

930 One of the most significant concerns about MOFs in practical applications is the  
931 difficulty in obtaining such materials in large quantities. Spent LIBs provide an alternative  
932 source. To optimize the synthesis of MOFs for a greener approach, it is advisable to identify  
933 the key parameters that can influence material production, such as reagents, solvents, and  
934 synthesis methods. During the formation of MOFs, transition metals (such as nickel,  
935 manganese, and cobalt) extracted through the recycling of LIBs must form strong bonds with  
936 carboxylic acid ligands such as trimesic acid (BTC) or terephthalic acid (BDC). The solvent  
937 can be replaced with a greener one in the MOFs synthesis with similar properties of  
938 dissolving metals and organic ligands, while the temperature and reaction time are two critical  
939 factors affecting the MOF synthesis process from spent LIBs.

940 MOFs are synthesized from metal ions and organic linkers using conventional  
941 methods such as hydrothermal or solvothermal processes.[193] MOF with NMC (111) can be  
942 synthesized from a battery waste leaching solution [194] by solvothermal process and used as  
943 electrode materials. [195,196] The electrochemical properties of this MOF, as well as the  
944 corresponding reduced and oxidized materials, have revealed that they have  
945 exciting properties for use in battery materials. Recently, a novel method for producing MOFs  
946 from a real waste stream was reported. [197] Typically, a hydrothermal method was used to  
947 fabricate MOFs on a large scale in the regeneration process. [193] Initially, the spent LIBs  
948 were crushed into powder, while the metals were extracted in acidic solution, followed by the  
949 addition of an organic ligand and solvent into the metal leaching solution at a low thermal  
950 process. Using this procedure, a different form of MOFs can be synthesized by changing the  
951 experimental conditions. The presence of metals such as Al and Cu in the leached solution  
952 produced MOF (MIL-96, HKUST-1) with these metals as the centres. By fine-tuning the

953 procedure, it was possible to selectively precipitate all Al and Cu in solution, producing a  
954 hybrid material with high porosity (around 700 m<sup>2</sup>.g<sup>-1</sup> for MOF MIL-96). Moreover, it has  
955 been demonstrated that another Al-MOF known as MIL-53 can be obtained by using a  
956 different precipitating agent (BDC ligand), where these porous materials can be useful for  
957 other applications such as gas storage or separation. In order to accelerate the crystallization  
958 process and fabricate uniform crystals of MOFs, many alternative synthesis routes such as  
959 microwave-assisted, electrochemical, mechanochemical, Sonochemical, and spray drying  
960 have been reported in the literature. [198-200] For example, microwave-assisted synthesis is  
961 comparable to hydrothermal or solvothermal synthesis and can achieve similar materials and  
962 yields in different batches. Microwave-assisted MOF synthesis can be an alternative green  
963 approach that controls reaction temperature and time. Indeed, this waste-to-MOFs approach  
964 for greener MOFs synthesis is of interest for obtaining high value-added products on a large  
965 scale and potentially achieving an economically viable LIB recycling process through an  
966 open-loop cycle.

967 MOFs made up of metals from connectors are unsuitable for use as electrode  
968 materials. Other battery wastes where Al and Cu have been removed (mechanically) can be of  
969 interest for forming MOFs that can be reused as new electrode materials based on Co, Ni,  
970 and/or Mn. This should be investigated in the near future to validate such a process and create  
971 a closed-loop cycle with electroactive MOF precipitation. Upscaling of MOF synthesis  
972 usually encounters difficulties due to the longer reaction times, a large amount of solvents  
973 used, the low quality of obtained materials, the difficulty in ensuring reproducibility between  
974 batches, and the cost.

#### 975 **5.4 Waste combination**

976 Green approaches in the synthetic route for MOFs are essential for using these  
977 materials in industrial applications. [201] Recently, a synthetic process has been developed for

978 both the organic linker and metal centers based on only waste sources. [202] The process  
979 utilized Polyethylene terephthalate (PET) waste bottles as a source for organic ligand and LIB  
980 waste for metal source. The release of BDC ligand in solution is caused by the  
981 depolymerization of PET waste under alkaline conditions. Combining the two waste stream  
982 flows made it possible to obtain MOF MIL-53 in large quantities from waste materials with  
983 properties similar to the MOF synthesized from commercial chemicals. The above research  
984 work paves the way for an integrated solution for solid waste utilization concerning efficient  
985 process design, low-cost materials, and highly pure and porous synthesized materials. It  
986 demonstrates how different waste streams can be combined to lay the foundation for an  
987 integrated circular economy through various waste recycling processes (for batteries and  
988 plastics).

989

## 990 **6. Conclusion and prospects**

### 991 **6.1 Bioleaching for battery recycling**

992 The factors affecting the bioleaching process of LIBs are slow kinetics, microbial  
993 tolerance against metal toxicity, acidic environment, and low solid-liquid ratio (pulp density).  
994 [64] The limitations of the bioleaching process in large-scale industrial applications are the  
995 poor adaptability of microbes and rigorous leaching conditions. However, spent LIBs are the  
996 secondary source of metals, and their content is higher than the natural ores; for example, in  
997 order to extract one ton of lithium, around 750 tons of brine salts are needed, but only 28 tons  
998 of spent LIBs are sufficient. The difficulties in the bioleaching process can be accomplished  
999 by adapting the microbes to the toxic environment using microbial consortia and the addition  
1000 of metal ions such as  $\text{Ag}^+$  and  $\text{Cu}^{2+}$  to increase the kinetics using the omics approaches to  
1001 modify the microorganisms. The microbial competencies, such as tolerance against metal  
1002 toxicity and acidic environment, as well as increasing the metabolites production, can be  
1003 achieved by genetically modifying the organism. [70, 76] The success of LIB bioleaching in a

1004 large-scale recycling process depends on the ability of microbes to tolerate toxic metals,  
1005 cultivate microbes using low-cost nutrients, and optimize process kinetics. At a high solid  
1006 content of 100 g/L (S/L), a leaching efficiency of 80–90% was obtained using the bioleaching  
1007 process recently, which is an excellent indicator for the applicability of bioleaching for  
1008 commercial recycling of spent LIBs in the coming years. [62-64] It is feasible to optimize all  
1009 conceivable parameters which affect leaching efficiency in lab-scale bioleaching experiments.  
1010 However, environmental factors such as humidity and outdoor temperature (sunlight) may  
1011 play a crucial role when scaling up the bioleaching process at an industrial scale. Optimal  
1012 humidity conditions favor and grow bacteria and transport nutrients, so it is necessary to  
1013 evaluate humidity over time vs microbial growth vs bioleaching efficiency. [203]  
1014 Temperature is another critical factor influencing microbial activity and, accordingly, metal  
1015 bioleaching. The ideal temperature for bioleaching is the one that favors metal dissolving the  
1016 most, which is also linked to bacterial activity throughout the metal extraction process. [204]  
1017 A temperature control system is necessary when performing the LIB bioleaching at the factory  
1018 scale. Conducting a life-cycle assessment is the best way for LIB bioleaching when scaling up  
1019 the process. This method compiles and assesses the inputs, outputs, and potential  
1020 environmental implications of a commercial production system. [205] By overcoming the  
1021 challenges such as slow kinetics, microbial tolerance against metal toxicity, and high solid-  
1022 liquid ratio (pulp density) in the bioleaching process, valuable metals can be recovered from  
1023 the spent LIBs in an eco-friendly and energy-efficient way.

## 1024 **6.2 Food waste enabled battery recycling**

1025       Recent discoveries on food waste-based hydrometallurgical approaches have greatly  
1026 expanded the list of available green reductants to recycle spent LIBs. Compared to the  
1027 traditional hydrometallurgical methods whose success hinges on synthetic reductants such as  
1028  $\text{H}_2\text{O}_2$ ,  $\text{NaHSO}_3$  and  $\text{NaS}_2\text{O}_3$ , the use of food waste confers a safer and low-cost route to

1029 efficiently recover the precious metals like Co, Li, Mn, and Ni from the discarded cathodes.  
1030 More importantly, the leaching efficiency for different metals is shown to reach an  
1031 appreciable range (80-100%) using these green reductants, indicating their feasibility for  
1032 replacing the conventional reducing chemicals. The mechanism of action for different kinds of  
1033 food waste and its derivatives has been extensively studied. The consensus seems to be  
1034 reached according to the data from different articles, and the theory of conversion of cellulose  
1035 and hemicellulose, two significant parts of food waste, to reducing sugars has been proposed  
1036 and tentatively verified. In addition, it is also believed that antioxidants like polyphenols also  
1037 assist with the metal extraction process.

1038         Treatment of post-processing of food waste-derived residues after metal leaching is an  
1039 open technical issue that needs to be addressed in the coming years. These residues are rich in  
1040 carbon and other valuable nutrients, such as nitrogen-containing organic molecules, which can  
1041 be recovered and efficiently used again. However, the most common procedure for post-  
1042 treatment of food waste residues is dewatering, which eliminates the moisture content,  
1043 followed by disposal in landfills, which results in significant loss of valuable ingredients. [206]  
1044 To reuse nitrogen-containing substances, scientists have begun to use microbes to stabilize the  
1045 N-based nutrients, which are then used for soil enrichment and crop growth enhancement. The  
1046 utilization of carbon compounds in food waste-derived residues, on the other hand, has  
1047 received far less attention.

1048         Future research is required in the era of the circular economy to develop a sustainable  
1049 approach to commodify these carbon-rich waste products. Turning them into high-  
1050 performance carbonic anodes is one strategy to upcycle them. [207] After all, using food  
1051 waste as a next-generation green reductant will indeed surpass currently used chemical  
1052 reductants. As the world's food waste and battery waste stockpiles are rising, an intelligent  
1053 method that can examine both forms of trash in one place is essential. Considering the real-

1054 life LIBs recycling business dealing with ton-scale battery waste, it is necessary to find a way  
1055 to translate the current findings in the laboratories to a realistic industrial recycling viable  
1056 process. Fortunately, the recent works provide detailed experimental data on the laboratory  
1057 scale and an in-depth mechanistic understanding of the food waste-based reductants approach,  
1058 which is believed to lay a solid foundation for future attempts to upscale this green process.

### 1059 **6.3 Electrochemical battery recycling**

1060 Metal recovery by electrochemical technology is selective, efficient, and eco-friendly  
1061 in nature and becoming an attractive alternative approach in developing sustainable recycling  
1062 of LIBs. Due to its ability to improve processes in different stages of hydrometallurgy, i.e.  
1063 leaching and recovery, in terms of time, product yield without adding additional chemicals, as  
1064 well as using straightforward equipment, facilitates the metal recovery towards a faster and  
1065 more efficient process while reducing the amount of secondary waste. Moreover,  
1066 electrodeposition enables the possibility to tune physicochemical properties of recovered  
1067 metal products during a deposition process, thus widening possibilities for their different  
1068 applications. However, to advance the technology towards a more practical and scalable  
1069 direction, the recovery procedures must be further improved to regenerate LIBs from the spent  
1070 mixed batteries for their second life in a straightforward approach. Among the directions to  
1071 improve are: (i) improvement of an electrochemical cell design and electrode material,  
1072 development protocols for low-cost electrolytes, (iii) improvement of an operational process  
1073 such as rotation for better ion transport.

### 1074 **6.4 Reusability of battery waste**

1075 Several pre-treatment and synthetic processes can be used to regenerate cathode  
1076 materials such as  $\text{LiNi}_x\text{Co}_y\text{Mn}_z\text{O}_2$  (NMC),  $\text{LiCoO}_2$  (LCO), and  $\text{LiFePO}_4$  (LFP) from spent  
1077 LIBs. As compared to commercial electrodes with exact stoichiometry, the regenerated  
1078 cathode materials show similar initial cell performance. Long-term performance is a deeper,

1079 in-depth studies on the electrochemical behaviour of these regenerated electrodes in new LIBs  
1080 that need to be studied. The cost of regenerating these cathode materials from spent batteries  
1081 is significantly lower than the cost of preparing them from primary resources. Though the  
1082 approach is promising, it still has some drawbacks and challenges that make it challenging to  
1083 implement regeneration strategies in practice. During the regeneration process, the impurities  
1084 Al, Cu, and Fe should be tightly controlled under the threshold level. As a result, additional  
1085 treatment is often needed to eliminate impurity elements to enhance the performance of  
1086 cathode materials. The regeneration of graphite from spent LIBs has been offered as a viable  
1087 solution for meeting the anticipated demand for battery-grade graphite. However, a number of  
1088 challenges and issues must be addressed based on available information and projected future  
1089 growth in recovering battery-grade graphite. There should be a strategy for increasing the  
1090 capacity of the graphite electrode while limiting irreversible capacity and graphite  
1091 deterioration.

1092         Although MOFs synthesis has been scaled up for industrialization, further research  
1093 needs to be done on optimizing the synthesis parameters to control MOFs' properties to obtain  
1094 a viable and marketable material. Indeed, the water-stability, quality, functionality, financial  
1095 viability, and environmental-friendly production are essential for MOF synthesis. Therefore,  
1096 the further development of the green synthesis method of MOFs is necessary for a future  
1097 sustainable environment, and the focus is on recovering metals as MOFs and their reuse in a  
1098 closed loop. This review highlights the need for a sustainable, cost-effective, and large-scale  
1099 production of MOFs. In this perspective, the new approach for MOF synthesis can be from  
1100 waste linker sources (e.g., plastic wastes) using greener solvents (e.g., water, bio-derived  
1101 compounds) under milder ambient conditions. The main challenge is to create the best system  
1102 that works in all conditions and allows metals and ligand solubility in a scalable manner.

1103 Green Recycling methods of lithium-ion batteries is a step forward in a sustainable  
1104 direction towards the circular economy, but this area is still in its infancy. Studies, as  
1105 reviewed in this report, suggest promising results employing green recycling methods for  
1106 spent LIBs; however, at this point, based on the studies performed, it is difficult to conclude  
1107 which among the green recycling process is ideal for the future. Every recycling technique has  
1108 its own set of benefits and drawbacks, as discussed and highlighted. Moving forward, detailed  
1109 economic, cost-benefit analysis studies on the green recycling process needs to be conducted  
1110 to provide the economic benefits of these processes at an industrial scale. When it comes to  
1111 the sustainability of recyclable materials, lifecycle assessment (LCA) is the framework for  
1112 examining, identifying, and evaluating the energy, material, and environmental implications  
1113 of these green recycling processes, products and/or systems across its lifespan from the cradle  
1114 to the grave. This method compiles and evaluates a commercial production system's inputs,  
1115 outputs, and potential environmental consequences. The variables of efficiency, economy, and  
1116 environment should all be examined and balanced while systematically analysing a particular  
1117 green recycling technique with LCA. A reinterpretation of the “reduce, reuse, refurbish, and  
1118 recycle” strategy as “redesign, reuse, recycle” for battery recycling is recommended based on  
1119 current practice and projected future progress in this field. [3,13]

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## 1126 **Credit author statement**

1127 The manuscript was written through the contributions of all authors. All authors have  
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1129

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1142 **Notes**

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1144 **Conflict of Interest Statement**

1145 The authors declare that they have no known Conflict of Interest or personal relationships that  
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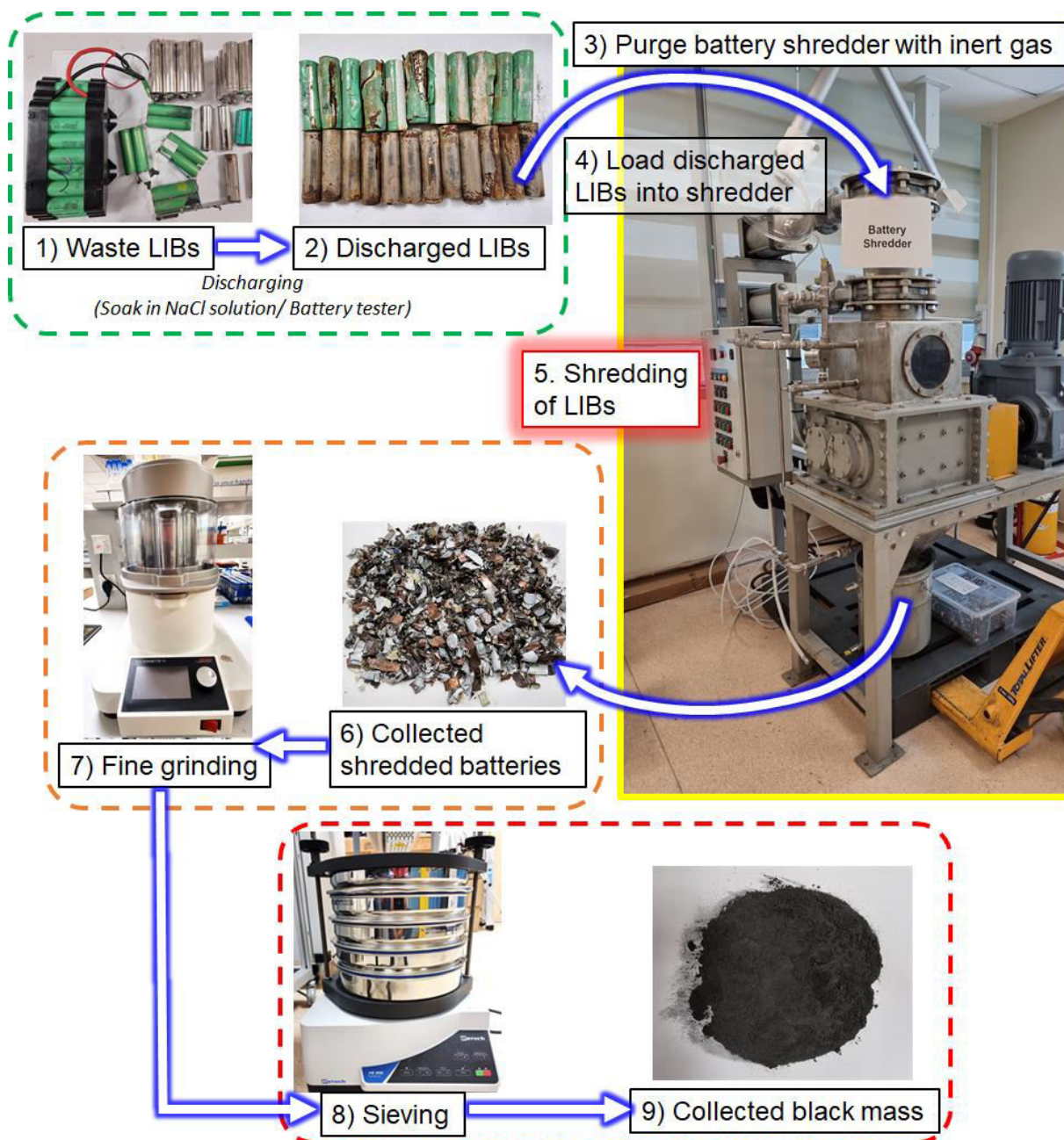
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1500 **Figures**



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Figure 1: Process flow diagram of pre-treatment.

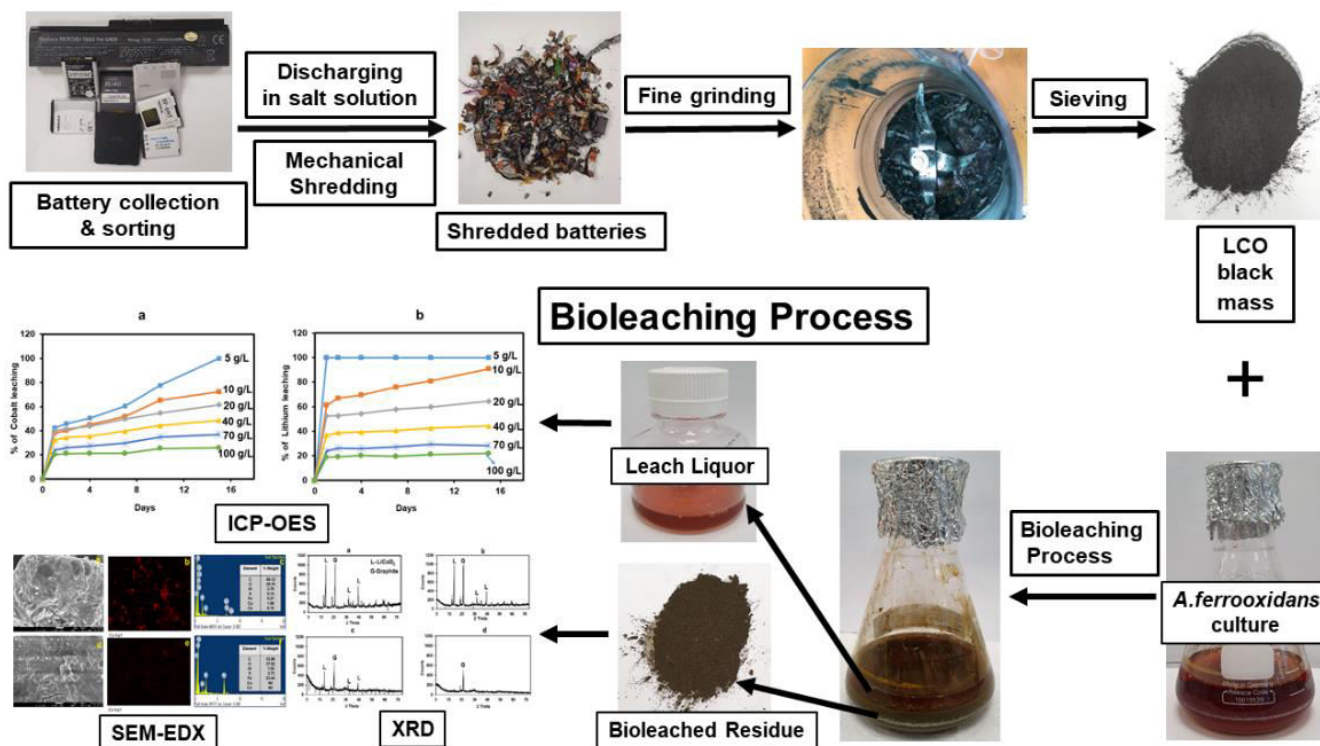
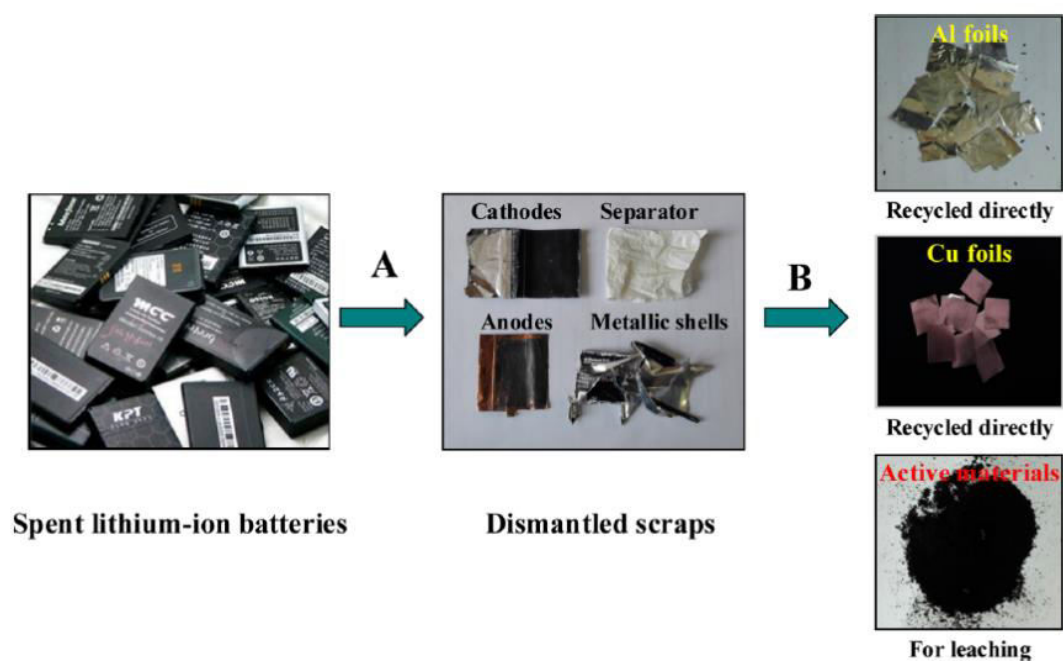


Figure 2: Typical bioleaching process , Reproduced with permission [62] Copyright 2021, Elsevier



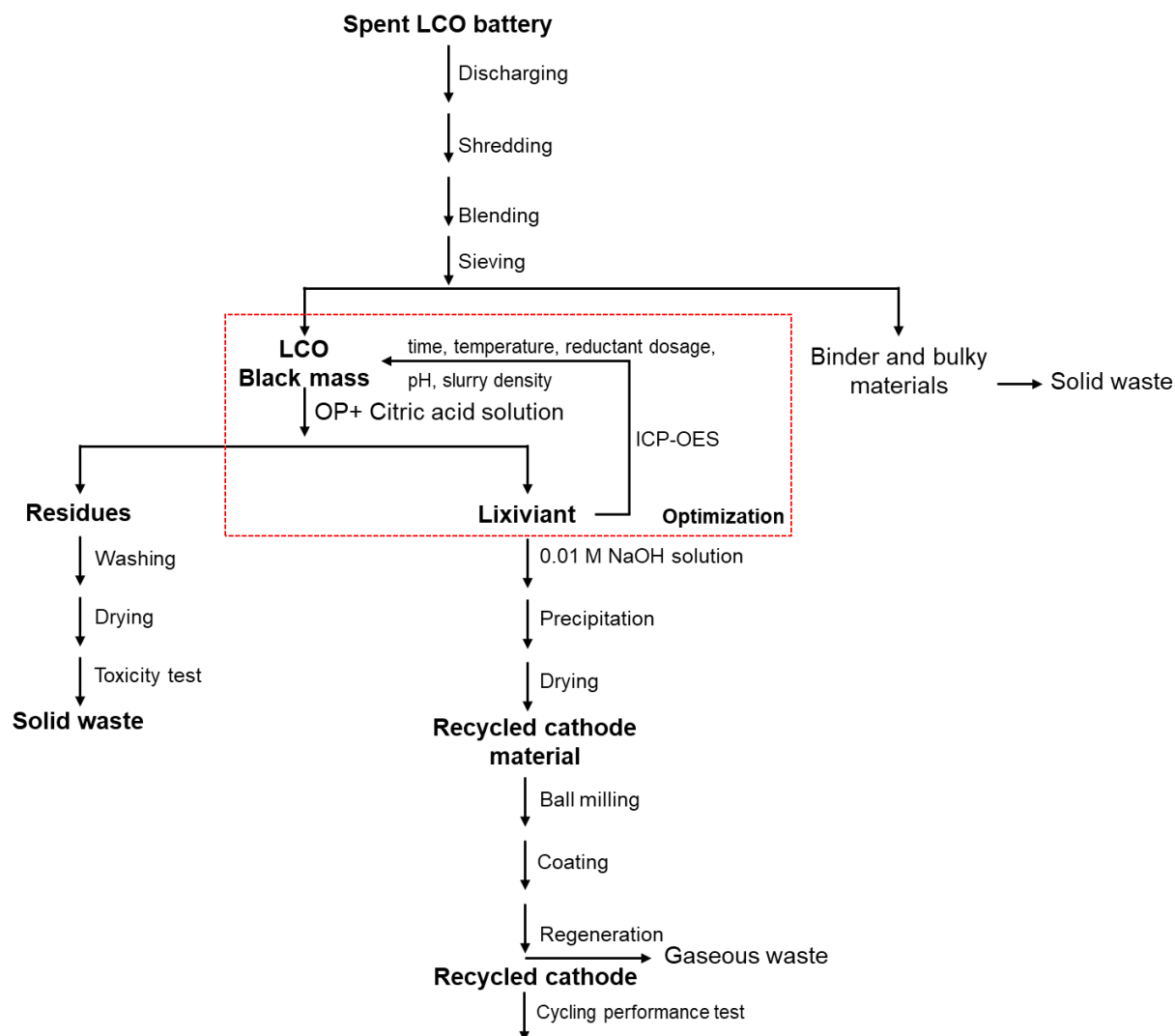
Figure 3: An illustration representing various food waste employed in the recent progress on the food-waste enabled waste for waste (W4W) approaches for recycling spent LIBs. A) Tea Leaf B) Orange peel c) Grape seed D) Macadamia shell E) Corn cop



**Figure 4: Mechanical processing of spent LIBs prior to leaching experiments.**

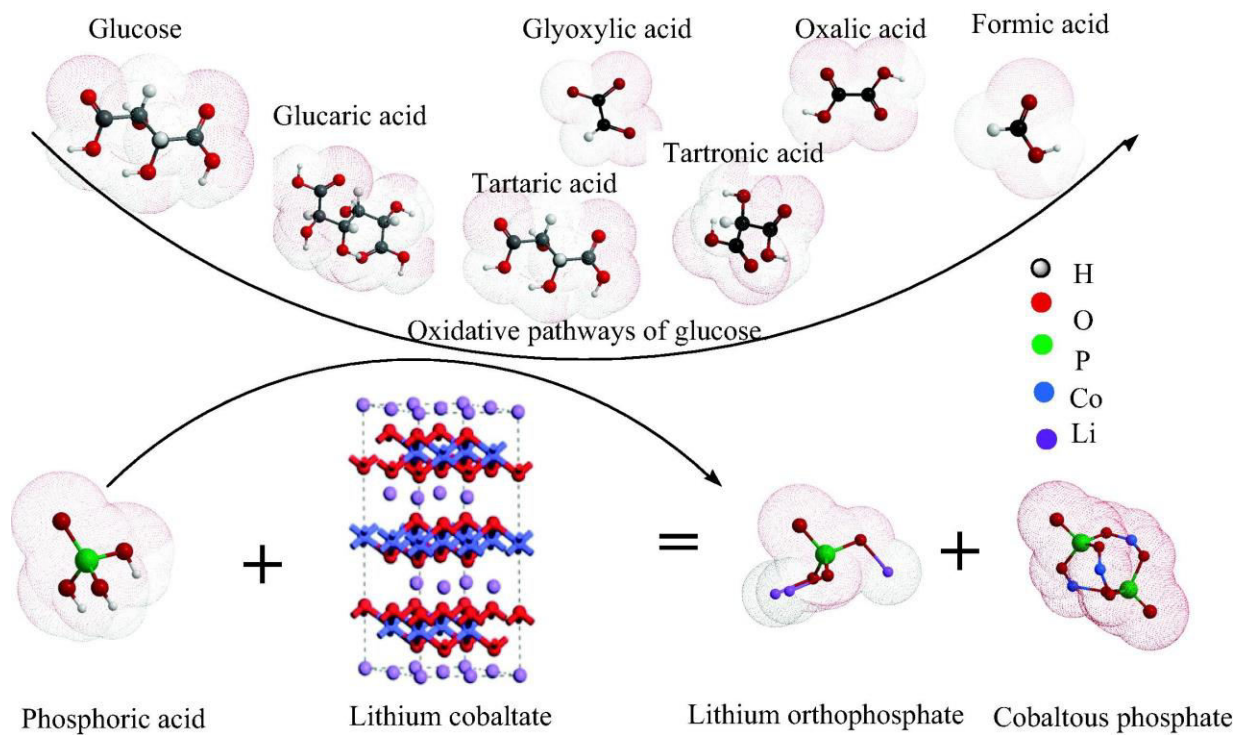
A. Manual dismantling B. Peeling of Al/Cu foils for their direct recycling

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**Figure 5: An overview of the orange peel (OP)-based green hydrometallurgical process for the recycling of spent LIBs.** Reproduced with permission [84] .

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**Figure 6: A possible leaching process of  $\text{LiCoO}_2$  material in the glucose and phosphoric acid solution.** Reproduced with permission [85] Copyright (2017), Elsevier.

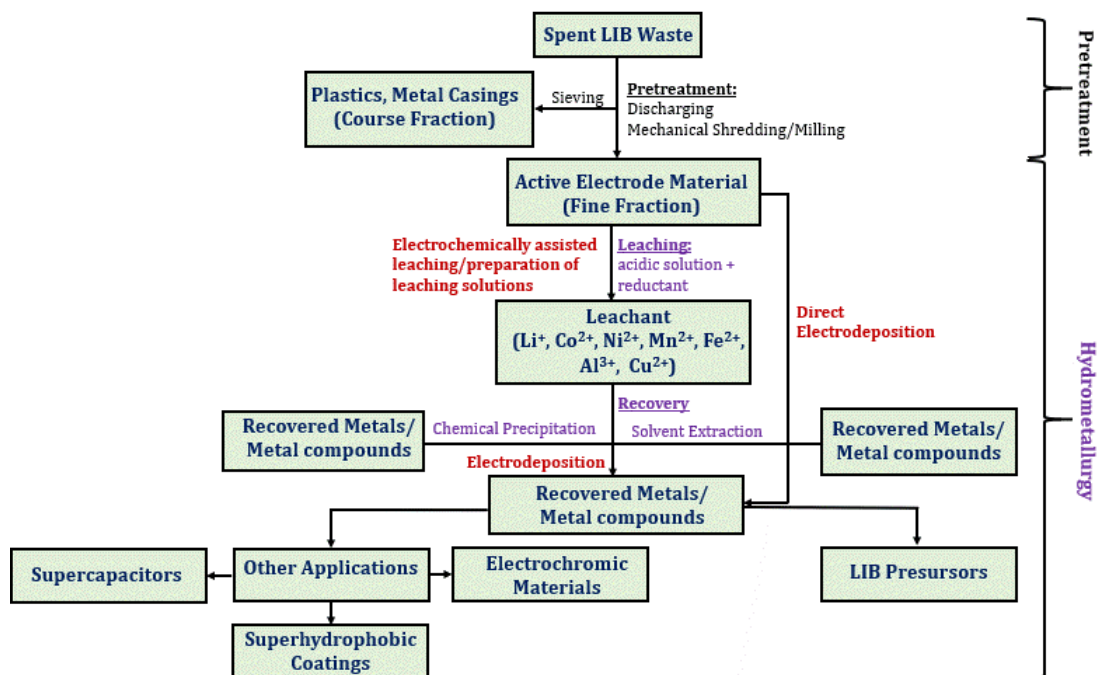
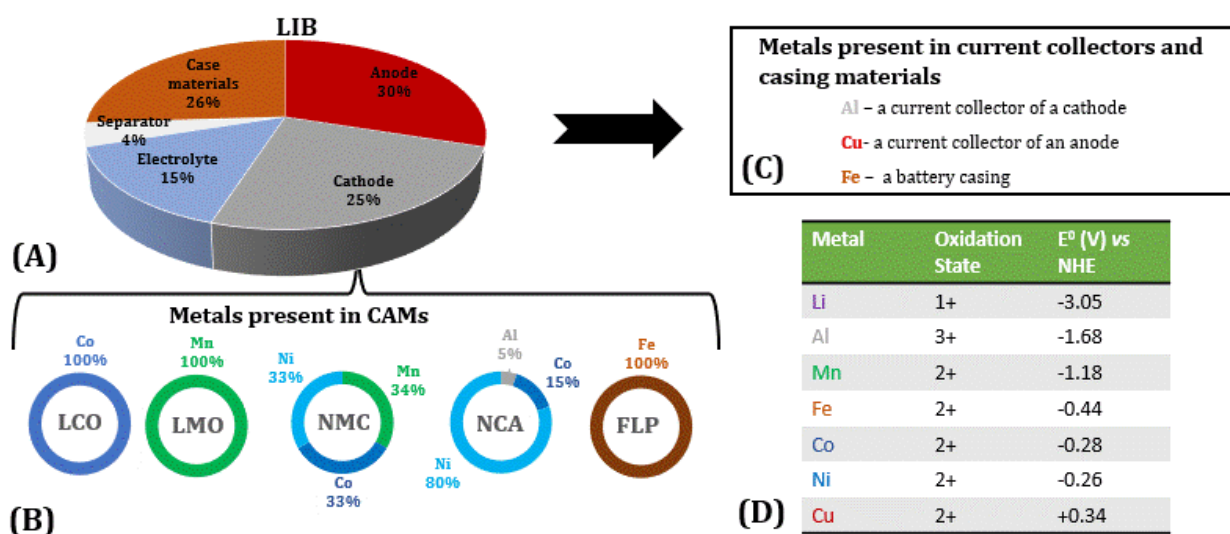


Figure 7: Flowchart of a hydrometallurgy recycling process of spent LIB waste, where the purple colour marks the commonly used processes, whereas the red colour indicates electrochemically assisted approaches.



**Figure 8:** (A) Composition of a typical LIB; (B) Metals present in different types of CAMs (Li is not shown); (C) Metals present in current collectors and casing materials; (D) Standard reduction potentials of metals present in spent LIB waste.

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## Tables

**Table 1: Battery Recycling methods' advantages and disadvantages.**

<b>Recycling Method</b>	<b>Advantages</b>	<b>Disadvantages</b>	<b>References</b>
Pyrometallurgy	Applicable to all battery types and configuration After sorting no other mechanical pre-treatment necessary High recovery of metals (e.g., Co, Ni, and Cu)	Cannot recycle/ treat Li, Al, and LFP batteries  Gas clean-up is required to avoid toxic air emissions Energy and Capital intensive	15
Hydrometallurgy	Applicable to any battery chemistry  Flexible in recovery processes to target specific metals High recovery rates and High purity can be achieved  Energy and capital efficient Retains valuable cathode structure	Battery cells must be crushed (causing safety concerns) Cathode structure defects because of Acid treatment  High volume of process efficient to be treated and recycled or disposed Not economical for lithium iron phosphate (LFP) batteries	16
Direct recycling	Practically all battery materials can be recovered, including anode, electrolyte, and foils  Suitable for LFP batteries  Energy efficient  Convenient for recycling manufacturing scraps	Complex mechanical pre-treatment and separations are required Recovered material may not perform as well as virgin material or becomes obsolete by the time it is introduced to market Mixing cathode materials could reduce the value of recycled product Regeneration processes yet to be developed Not scaled up to industrial level	17

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**Table 2: Physio-electro properties of lithium-ion batteries and types**

Types of Li-ion batteries	Cathode	Anode	Nominal Voltages	Typical operating range	Specific energy (capacity)	Charge (C-rate)	Discharge (C-rate)	Cycle life	References
Lithium Cobalt Oxide (LCo)	LiCoO <sub>2</sub> (~60% Co)	graphite	3.60V	3.0–4.2V/cell	150–200Wh/kg	0.7–1C, charges to 4.20V (most cells); 3h charge typical. Charge current above 1C shortens battery life.	1C; 2.50V cut off. Discharge current above 1C shortens battery life	500–1000, related to depth of discharge, load, temperature	22,25
Lithium Manganese Oxide (LMO)	LiMn <sub>2</sub> O <sub>4</sub>	graphite	3.70V-3.80V	3.0–4.2V/cell	100–150Wh/kg	0.7–1C typical, 3C maximum, charges to 4.20V (most cells)	1C; 10C possible with some cells, 30C pulse (5s), 2.50V cut-off	300–700 (related to depth of discharge, temperature)	22,25
Lithium Nickel Manganese Cobalt Oxide (NMC)	LiNiMnCoO <sub>2</sub>	graphite	3.60V-3.70V	3.0–4.2V/cell, or higher	150–220Wh/kg	0.7–1C, charges to 4.20V, some go to 4.30V; 3h charge typical. Charge current above 1C shortens battery life.	1C; 2C possible on some cells; 2.50V cut-off	1000–2000 (related to depth of discharge, temperature)	22,55
Lithium Iron Phosphate (LFP)	LiFePO <sub>4</sub>	graphite	3.20-3.30V	2.5–3.65V/cell	90–120Wh/kg	1C typical, charges to 3.65V; 3h charge time typical	1C, 25C on some cells; 40A pulse (2s); 2.50V cut-off (lower than 2V causes damage)	2000 and higher (related to depth of discharge, temperature)	22,25
Lithium Nickel Cobalt Aluminum Oxide (NCA)	LiNiCoAlO <sub>2</sub> (~9% Co),	graphite	3.60V	3.0–4.2V/cell	200-260Wh/kg 300Wh/kg predictable	0.7C, charges to 4.20V (most cells), 3h charge typical, fast charge possible with some cells	1C typical; 3.00V cut-off; high discharge rate shortens battery life	500 (related to depth of discharge, temp.)	22,55
Lithium Titanate (LTO)	lithium manganese oxide	Li <sub>2</sub> TiO <sub>3</sub> (titanate)	2.40V	1.8–2.85V/cell	50–80Wh/kg	1C typical; 5C maximum, charges to 2.85V	10C possible, 30C 5s pulse; 1.80V cut-off on LCO/LTO	3,000–7,000	22,55

**Table 3: Microorganisms used in the bioleaching of LIBs.**

S. No	Organism Name	Single/consortia	Nutrient Media	Temp & pH	Pulp Density w/v	Bioleaching Efficiency %	Reference
<b>Bacteria used in the bioleaching of LIBs</b>							
1.	<i>Acidithiobacillus Thiooxidans (80191)</i>	Single	Basel 317 + S power 1%	30°C / pH 3.3 & pH 2.4	0.25%	Li 22, Co 66	[44]
2.	<i>Acidithiobacillus ferrooxidans (ATCC19859)</i>	Single	9k medium+ S power + Fe(II) ion 3 g/L	30°C / pH 2.5	0.5%	Li 9, Co 65	[54]
3.	<i>Acidithiobacillus thiooxidans(isolated)</i>	Single	Basic medium + S powder 16 g/L + pyrite 16g/L	30°C / pH 1.0	1.0%	Li 85, Mn 19 Co 10, Ni 10	[73]
4.	<i>Leptospirillum ferriphilum (isolated)</i>	Single	Basic medium +S powder 16g/L + pyrite 16g/L	30°C / pH 1.0	1.0%	Li 31, Mn 42 Co 23, Ni 23	[73]
5.	<i>Acidithiobacillus thiooxidans(isolated) and Leptospirillum ferriphilum(isolated)</i>	Consortia	Basic medium + S powder 16g/L + pyrite 16g/L (1: 1 ratio)	30°C / pH 1.0	1.0%	Li 90, Mn 90 Co 96, Ni 97	[73]
6.	<i>Acidithiobacillus ferrooxidans (PTCC1647) and Acidithiobacillus Thiooxidans(PTCC 1717)</i>	Adapted mixed culture	Modified 9k medium + S powder 5 g/L+ FeSO4 36.7 g/L	32°C / pH 1.5	4.0%	Li 99.2, Co 50.4 Ni 89.4	[69]
7.	<i>Acidithiobacillus Thiooxidans(PTCC 1717)</i>	Single	9k Medium + S powder 5 g/L	30°C / pH 2.0	1.0 - 5.0%	Li 99, Co 60 Ni 20 (3% w/v)	[61]
8.	<i>Acidithiobacillus ferrooxidans (PTCC 1647)</i>	Single	9K medium + FeSO4.7H2O 44.22 g/L	30°C / pH 2.0	1.0 -10%	Li 100, Co 88, Mn 20 (4% S/L)	[56]
9.	<i>Acidithiobacillus ferrooxidans DSMZ 1927)</i>	Single	Modified 9K medium + FeSO4.7H2O 150 g/L	30°C / pH 2.0	10%	Co 94, Li 60	[62]
10.	<i>Acidithiobacillus ferrooxidans DSMZ 1927)</i>	Single	Modified 9K medium + FeSO4.7H2O 150 g/L	30°C / pH 2.0	10%	Ni 90, Mn 92, Co 82, Li 89	[63]
<b>Fungi used in the bioleaching of LIBs</b>							
11.	<i>Aspergillus Niger (Isolated)</i>	Single	Sucrose medium	30°C / 2.4	0.25	Li 100, Co 82	[44]
12.	<i>Aspergillus Niger (PTCC 5010)</i>	Single/ adapted	Sucrose medium	30°C / 2.5	1.0	Li 100, Co 38 Cu 94, Mn 72 Ni 45	[48]
13.	<i>Aspergillus Niger (PTCC 5210)</i>	Single	Sucrose medium	30°C / 3.0	2.0	Li 100, Co 55, Cu 100, Mn 77, Ni 37	[47]
14.	<i>Aspergillus Niger (PTCC 5210)</i>	Single	Sucrose medium	30°C / 1.0	1.0	Li 95, Co 45 Cu 100, Mn 70, Ni 38	[49]

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**Table 4: A summary of several recent publications on the development of green hydrometallurgical processes**

Acid	Reductant	Reaction steps	Results	Reference
Succinic acid	H <sub>2</sub> O <sub>2</sub>	1.5 M succinic acid; 4 vol% H <sub>2</sub> O <sub>2</sub> ; 15 g/L S/L ratio; 70 °C; 40 min	100% Co and 96% Li were leached out	[99]
Malic acid	H <sub>2</sub> O <sub>2</sub>	1.5 M malic acid; 2 vol% H <sub>2</sub> O <sub>2</sub> ; 20 g/L LCO; 90 °C; 40 min	90% Co and 100% Li were leached out	[100]
Citric acid	H <sub>2</sub> O <sub>2</sub>	2M citric acid; 2 vol% H <sub>2</sub> O <sub>2</sub> ; 33g/L S/L ratio; 80 °C; 90 min	97% Ni, 95% Co, 94% Mn, and 99% Li were leached out	[101]
Tartaric acid	H <sub>2</sub> O <sub>2</sub>	2 M tartaric acid; 4 vol% H <sub>2</sub> O <sub>2</sub> ; 17 g/L pulp density; 70 °C; 30 min	99.31% Mn, 99.07% Li, 98.64% Co, and 99.31% Ni were leached out	[102]
Formic acid	H <sub>2</sub> O <sub>2</sub>	10:1 molar ratio of formic acid and LCO; 6 vol% H <sub>2</sub> O <sub>2</sub> 20 g/L S/L ratio; 60 °C; 20 min	~ 99% Co and Li were leached out	[103]
Acetic acid	H <sub>2</sub> O <sub>2</sub>	2M acetic acid; 2.5 vol% H <sub>2</sub> O <sub>2</sub> ; 30g/L S/L ratio; 25 °C	~ 70% Co and Li were leached out	[104]
Ascorbic acid	-	1.25 M ascorbic acid; 25 g/L S/L ratio; 70 °C, 20 min	94.8% Co and 98.5% Li were leached out	[105]
Lactic acid	H <sub>2</sub> O <sub>2</sub>	1.5 M lactic acid; 0.5 vol% H <sub>2</sub> O <sub>2</sub> ; 20 g/L S/L ratio; 70 °C; 20 min	97.7 Li, 98.2 Ni, 98.9 Co, and 98.4 Mn were leached out	[106]
Oxalic acid	H <sub>2</sub> O <sub>2</sub>	1 M oxalic acid; 15 vol% H <sub>2</sub> O <sub>2</sub> ; 50 g/L S/L ratio; 80 °C; 60 min	~ 96% Co and Li were leached out	[107]
Aspartic acid	H <sub>2</sub> O <sub>2</sub>	1.5 M aspartic acid; 4 vol% H <sub>2</sub> O <sub>2</sub> ; 10 g/L S/L ratio; 90 °C; 120 min;	60% Co and Li were leached out	[108]
Sulfuric acid	NaHSO <sub>3</sub>	1 M H <sub>2</sub> SO <sub>4</sub> ; 0.075 M NaHSO <sub>3</sub> ; 50 g/L S/L ratio; 95 °C; 240 min	93.4% Li, 66.2% Co, 96.3% Ni and 50.2% Mn were leached out	[81-82]
Sulfuric acid	Na <sub>2</sub> S <sub>2</sub> O <sub>3</sub>	3 M H <sub>2</sub> SO <sub>4</sub> ; 0.25 M Na <sub>2</sub> S <sub>2</sub> O <sub>3</sub> ; 1/15 S/L ratio; 90 °C; 180 min	99.95% Co, 99.71% Li were leached out	[109]

**Table 5: Electrochemically-assisted leaching studies of metals from spent LIB waste.**

Year	LIB Type	Leaching Procedure	Leaching Rate	Reference
<b>Electrochemically-assisted leaching</b>				
2010	Mixed LIBs	Galvanostatic leaching at 400 A/m <sup>2</sup> in 2 M H <sub>2</sub> SO <sub>4</sub> for 3h. Pb anode and SS cathode.	99 % of Co and Mn	[116]
2019	LMO	Galvanostatic leaching (at 400 A/m <sup>2</sup> ) of 75 g/l of CAM in the mixture of 1 M H <sub>2</sub> SO <sub>4</sub> and 1M MnSO <sub>4</sub> (90 °C for 20 h). Ru-plated Ti anode and graphite cathode.	99 % of Li and 92 % of Mn	[132]
<b>Leaching in electrochemically generated leaching solution</b>				
2018	Mixed LIBs	Leaching solution generation: graphite rod or Ti mesh electrodes. Electrolysis of 0.5 M NaCl at 4 and 8 V for 24 h.  A single stage leaching: pulp density of 10 % (w/v) at 80 °C and room temperature with 200 rpm shaking for 2 h.  Multistage leaching: 10 % (w/v) at 80 °C and room temperature with 200 rpm shaking for 1 h. Leaching again with a fresh anolyte solution after centrifugation.	Multistage leaching :  <10 % for Co and Cu, 31 % Li, 59 % Ni, 28 % Mn	[117]
2020	LCO	0.1 M HCl anolyte and 0.1 M HNO <sub>3</sub> catholyte separated by a cation exchange membrane. Ru-plated Ti anode and SS cathode. Electrodialysis at 10 A/m <sup>2</sup> for 70 h at 25 °C.	56 % of Li and 25 % of Co	[118]

**Table 6: Summary of research on metal recovery from spent LIBs by electrochemical methods.**

LIB Type	Electrochemical Recovery Procedure	Products/ Recovery Rate	Research Scope/ Application	Reference.
<b>Recovery from H<sub>2</sub>SO<sub>4</sub> Leachate</b>				
NCA	Galvanostatic Ni deposition (Al cathode, Pb-8 Sb anode): 250 A/m <sup>2</sup> , pH 3-3.2 at 50 °C; Potentiostatic Ni deposition (Al cathode, Ti anode): -1.2 to -1.5 vs SCE at RT.	Ni=87 % Co and Li not recovered.	N/A	[134]
Mixed LIBs	Galvanostatic Co deposition (Al cathode, Pb-8 Sb anode): 250 A/m <sup>2</sup> , pH 4-6 at 25-50 °C; Galvanostatic Ni deposition (SS cathode, Pb-8 Sb anode): 250 A/m <sup>2</sup> , pH 3.2 at 25-50 °C; Potentiostatic Co deposition (Al cathode, SS anode): -0.9 V vs SCE, pH 4-6, 30 °C; Potentiostatic Ni deposition (Al cathode, Ti anode): -1.5 vs SCE at RT.	Co=100 % Ni=87 % Li discarded as Li <sub>2</sub> SO <sub>4</sub> solution	N/A	[135]
LCO	Ag/AgCl <sub>sat</sub> RE, Pt CE and Pt WE electrodes. Potentiostatic deposition: at -0.2, -0.3, and -0.4 V for 30 s. Potentiodynamic deposition: +0.1 ÷ +0.8 V, 20 mV/s. Electrolyte: pH adjustment to 2.0 or 4.5 by using KOH, then buffering with 0.10 M H <sub>3</sub> BO <sub>3</sub> and 0.5 M K <sub>2</sub> SO <sub>4</sub> . Co <sup>2+</sup> conc. 0.001 M.	Cu	Evaluation of Cu electrodeposition mechanism by QCM and electrochemical methods.	[119]
LCO	Ag/AgCl <sub>sat</sub> RE, Pt CE, Al, Pt and vitreous carbon WE electrodes. Potentiostatic deposition: Co at -1 V and Cu at -0.3 V for 50 and 100 s. Electrolyte: pH adjustment to 2.7 or 5.4 by using NaOH, then buffering with 0.10 M H <sub>3</sub> BO <sub>3</sub> . Co <sup>2+</sup> and Cu <sup>2+</sup> conc. equal to 0.001 M and 0.1 M.	Co and Cu multilayers	Evaluation of pH effect on metal layer growth, morphology, and crystalline structure. Co-Cu multilayers exhibit giant magnetoresistance.	[119]
LCO	Ag/AgCl <sub>sat</sub> RE, Pt CE, ferritic SS 430 WE electrodes. Potentiodynamic deposition: -0.5 ÷ -1 V, 20 mV/s. Potentiostatic deposition: -0.8, -0.9, -1.2, -1.5, -2 V. Electrolyte: pH adjustment to 3, Co <sup>2+</sup> conc. 3.1 M.	Co=96 %	Coating on SOFC interconnects.	[145]
Mixed LIBs	Galvanostatic deposition at 200 A/m <sup>2</sup> in the leaching solution. Pb anode and SS cathode.	Co=96 % Cu=97 % Mn=99 %	Combined electro-leaching and electrodeposition system functioning at a zero liquid discharge tested at pilot scale.	[115]
Mixed LIBs	Galvanostatic deposition of Co was carried out at 200 A/m <sup>2</sup> , pH 4, 60 °C for 4 h.	Co= 92 % Other metals discarded as waste.	N/A	[133]
LCO	Pt ring anode and St-12 plain carbon steel plate cathode. Electrodeposition: Current control mode at 200 A/m <sup>2</sup> for 600 s; Pulsed current mode (1500 cycles) consisting of 400 ms deposition time at 200 A/m <sup>2</sup> and 400 ms with no current. Electrolyte: leachate with or without 0.5 M boric acid.	LiCo(CO) <sub>4</sub>	Corrosion resistive superhydrophobic coating.	[124]
LCO	Precipitation of Co(OH) <sub>2</sub> at pH 6.5 and calcination at 500 °C for 10 h to obtain Co <sub>3</sub> O <sub>4</sub> . Potentiostatic electroreduction (2.2 V for 3h) of Co <sub>3</sub> O <sub>4</sub> to Co using Ni10Cu11Fe alloy as an anode, and the Co <sub>3</sub> O <sub>4</sub> as a cathode. Electrolyte: molten Na <sub>2</sub> CO <sub>3</sub> -K <sub>2</sub> CO <sub>3</sub> . Precipitation of LiCO <sub>3</sub> at pH 10.3 (with addition of Na <sub>2</sub> CO <sub>3</sub> ) when increasing pH with NaOH.	Co (99 %) and Li <sub>2</sub> CO <sub>3</sub> (99 %)	Combined hydrometallurgical and pyro-electrochemical approach for a high recovery yield of Li and Co.	[137]

LCO	Co precipitation by liquid-liquid extraction, stripping, and galvanostatic deposition using Pb anode and SS cathode from Co solution (9 g/l) at 50-300 A/m <sup>2</sup> .	Co=80 % Li not recovered.	N/A	[136]
LMO	MnO <sub>2</sub> electrodeposition during electrochemical leaching (Table 5). LiCO <sub>3</sub> chemical extraction by Na <sub>2</sub> CO <sub>3</sub> .	MnO <sub>2</sub> and Li <sub>2</sub> CO <sub>3</sub>	MnO <sub>2</sub> for synthesis of catalyst, ionic sieve, or a CAM for LMO regeneration.	[132]

**Recovery from HCl Leachate**

LCO	Ag/AgCl <sub>sat</sub> RE, Pt CE and Al WE electrodes. Potentiodynamic deposition: -0.7÷-1.5 V vs Ag/AgCl <sub>sat</sub> , 10 mV/s. Potentiostatic deposition: at -0.8, -0.9, -1.0, -1.1, and -1.2 V. Electrolyte: leaching solution with pH adjustment.	Co=96.9 % at pH 5.4.	Evaluation of electrodeposition dependence on pH.	[142]
LCO	Ag/AgCl <sub>sat</sub> RE, Pt CE and Pt WE electrodes. Potentiodynamic deposition: 0÷-1.0 V vs Ag/AgCl <sub>sat</sub> , 20 mV/s. Potentiostatic deposition: at -0.9 or -1.0 V. Electrolyte: leaching solution with pH adjusted to 2.7 or 5.4, respectively.	Co=100% at pH 5.4	Investigation of Co electrodeposition mechanism in different pH solutions by simultaneous electrochemical-QCM technique.	[143]
LCO	Ag/AgCl <sub>sat</sub> RE, Pt CE and Al WE electrodes. Potentiostatic deposition was performed at -1.0 V, applying charge density (via adjusting the deposition duration) of 10, 50 and 100 C/cm <sup>2</sup> . Electrolyte: leaching solution with pH adjusted to 2.7 or 5.4, respectively,	Co=100% at pH 5.4	Evaluation of charge density and solution pH impact on the electrodeposition efficiency as well as morphology, and crystalline structure of the Co electrodeposits.	[120]
LCO	Ag/AgCl <sub>sat</sub> RE, Pt CE and Pt WE electrodes. Potentiostatic deposition: at -1.0 V, applying charge density of 5 C/cm <sup>2</sup> .	Co	Studies of supercapacitive behaviour of the recovered Co.	[144]
NMC	SCE RE, Pt sheet CE and Ni foam WE. Potentiodynamic deposition: -1.2÷-0.2 V vs SCE, 5 mV/s, 5 cycles. Electrolyte: leaching solution with pH adjusted to 6-7.	Li-Ni-Mn-Co hydroxides	Supercapacitor	[122]

**Recovery from HNO<sub>3</sub> Leachate**

LCO	Electroreduction of Co <sup>2+</sup> ions forming Co(OH) <sub>2</sub> (s) layer on Ti electrode by applying linear sweep voltammetry (LSV, 0÷-1.5V vs Ag/AgCl at 10 mV/s). Thermal dehydration at 400 °C converting Co(OH) <sub>2</sub> to Co <sub>3</sub> O <sub>4</sub> .	Co <sub>3</sub> O <sub>4</sub> (Li not recycled)	Electrochromic compound	[125]
LCO	The pH 11 adjusted by adding fresh 4 M LiOH solution. Electrodeposition parameters: 10 A/m <sup>2</sup> ; Ni anode; Pt cathode; T = 100 °C; time 20 h.	LCO	Refurbished LCO	[139]

**Recovery from Organic Acid Leachate**

LCO and LPF	F-doped tin oxide used as WE and CE, SCE RE. Potentiodynamic deposition of Fe film from the spent LPF cathode: -1.1 ÷ -0.5 V vs the SCE, 100 mV/s. Fe film conversion to hematite (Fe <sub>2</sub> O <sub>3</sub> ) in air at 770 °C. Further, the Co phosphate (CoPi)-based catalyst photoelectrochemical deposition on the Fe <sub>2</sub> O <sub>3</sub> films by using CAM from the spent LCO.	Fe <sub>2</sub> O <sub>3</sub> /CoPi	Fe <sub>2</sub> O <sub>3</sub> /CoPi photoanodes for water oxidation	[149]
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**Direct Recovery**

LCO	Galvanostatic electrodeposition on Pt at 0.001÷10 A/m <sup>2</sup> (40-100 °C). Electrolyte: CAM dispersed in 4 M KOH and NaOH mixture.	LCO	Refurbished LCO	[138]
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LCO	CAM pellet as a cathode and graphite rod anode. Potentiostatic electrodeposition at 1.0, 1.2, 1.5, and 1.8 V. Electrolyte: molten salt $\text{Na}_2\text{CO}_3\text{-K}_2\text{CO}_3$ .	CoO or Co (99 %), $\text{Li}_2\text{CO}_3$ (85 %)	CoO and $\text{Li}_2\text{CO}_3$ used as precursors to resynthesize LCO	[121]
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